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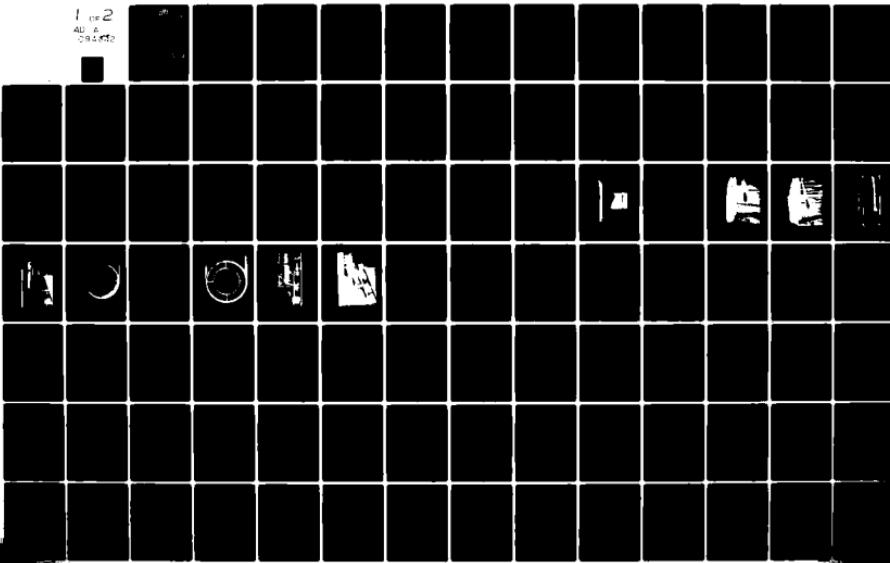
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**DAVID W. TAYLOR NAVAL SHIP
RESEARCH AND DEVELOPMENT CENTER**



Bethesda, Maryland 20084

DTNSRDC/SPD-0833-06

ANALYSIS OF WAKE SURVEY EXPERIMENTAL DATA FOR MODEL 5365 REPRESENTING THE
R/V ATHENA WITH AND WITHOUT THE BASS DYNAMOMETER BOAT

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REPRESENTING THE R/V ATHENA WITH AND WITHOUT THE
BASS DYNAMOMETER BOAT.

by

Rae B. Hurwitz and L. Bruce/Crook

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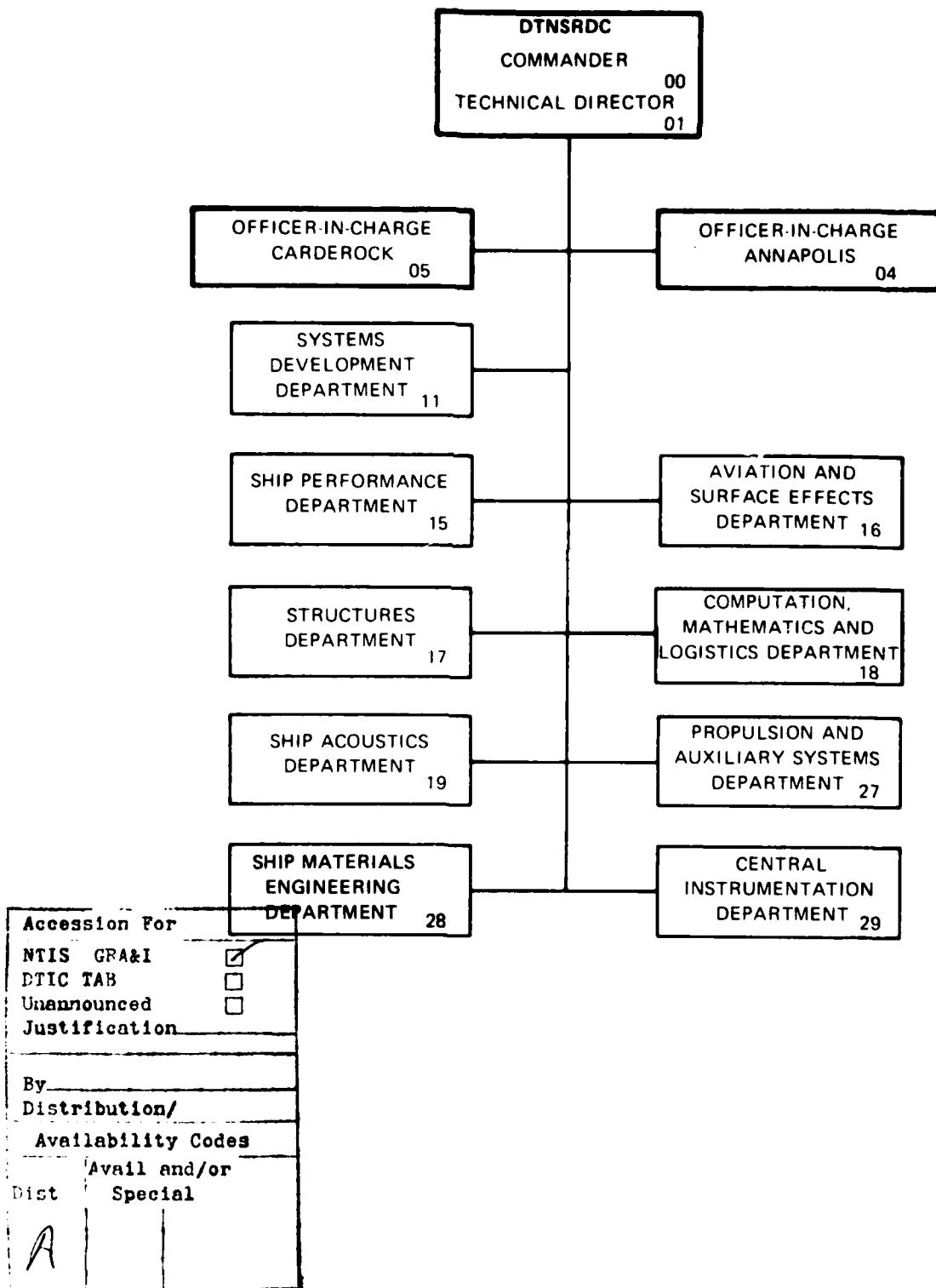
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distribution experiments, in which the model was removed and the pitot rake was mounted upstream of the Bass Boat. The effect of an operating port propeller on the mean starboard wake distribution and the harmonic content of the wake was small. The presence of the Bass Boat behind the ATHENA model, however, affects both the mean values and the harmonic content of the wake. Finally, one idealized mean wake distribution was shown to be weakly dependent on speed, and the harmonic content of wakes at two different speeds differed by less than three percent.

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TABLE OF CONTENTS

	Page
LIST OF FIGURES.....	iv
LIST OF TABLES.....	ix
NOTATION.....	xiii
ABSTRACT.....	1
ADMINISTRATIVE INFORMATION.....	1
INTRODUCTION.....	2
EXPERIMENTAL PROCEDURE.....	3
ACCURACY ASSESSMENT.....	7
PRESENTATION AND DISCUSSION OF RESULTS.....	7
CONCLUSIONS.....	14
REFERENCES.....	16
 APPENDIX A - VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS FOR EXPERIMENTS 3 AND 9	 31
 APPENDIX B - VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS FOR EXPERIMENT 10.....	 61
 APPENDIX C - VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS FOR EXPERIMENT 11.....	 77
 APPENDIX D - VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS FOR EXPERIMENT 12.....	 93
 APPENDIX E - VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS FOR EXPERIMENT 13.....	 109
 APPENDIX F - VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS FOR EXPERIMENT 14.....	 125
 APPENDIX G - VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS FOR EXPERIMENT 15.....	 141
 APPENDIX H - VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS FOR EXPERIMENT 16.....	 157

LIST OF FIGURES

	Page
1 - Rake Arrangement Sketch Showing Five Spherical Head Pitot Tubes with Five Holes Each	17
2 - Rake Arrangement Photographs Showing Installation in Starboard Shaft of Model 5365 During Experiments 3 and 9 Without Port Propeller	18
3 - Sketch Illustrating Location of Wake Survey Experimental Radii on Model 5365 Afterbody Sections Representing the R/V ATHENA	19
4 - Rake Arrangement Photograph Showing Closeup Profile View of Installation in Starboard Shaft of Model 5365 Without Port Propeller	20
5 - Rake Arrangement Photograph Showing Closeup Quartering View of Installation in the Starboard Shaft of Model 5365 Without Port Propeller	21
6 - Rake Arrangement Photograph Showing Installation in Bass Dynamometer Boat, Model 5271, Mounted Behind Starboard Shaft of Model 5365 With and Without Port Propeller as During Experiments 11 and 12	22
7 - Rake Arrangement Photograph Showing Bass Dynamometer Boat Mounted for 20 Degree (0.349 radian) Inclined Idealized Flow Wake Experiment 13	23
8 - Wake Screen Photograph Showing Downstream View at Spherical Head Pitot Tubes Used for Idealized Flow Experiment 14	24
9 - Schematic of Wake Screen Wire Sections and Sizes Used for Idealized Flow Experiment 14	25
10 - Wake Screen Photograph Showing Upstream View Into the Flow for Idealized Flow Experiment 14	26
11 - Bass Dynamometer Boat Mounted Behind the Wake Screen Photograph Showing Arrangement of Pitot Tubes for Idealized Flow Experiment 14	27
12 - Bass Dynamometer Boat Mounted for 10 Degree (0.174 radian) Inclined Idealized Flow Wake Photograph Showing Spacer Block Used for Experiments 15 and 16	28
A-1 ~ Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiments 3 and 9	32

LIST OF FIGURES (Continued)

	Page
A-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiments 3 and 9	33
A-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiments 3 and 9	34
A-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiments 3 and 9	35
A-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 3	36
A-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 3	37
A-7 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 9	38
A-8 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 9	39
A-9 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 9	40
A-10 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 9	41
A-11 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 9	42
A-12 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 9	43
B-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 10	62
B-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 10	63

LIST OF FIGURES (Continued)

	Page
B-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 10	64
B-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 10	65
B-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 10	66
B-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 10	67
C-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 11	78
C-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 11	79
C-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 11	80
C-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 11	81
C-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 11	82
C-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 11	83
D-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 12	94
D-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 12	95
D-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 12	96

LIST OF FIGURES (Continued)

	Page
D-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 12	97
D-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 12	98
D-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 12	99
E-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 13	110
E-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 13	111
E-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 13	112
E-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 13	113
E-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 13	114
E-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 13	115
F-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 14	126
F-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 14	127
F-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 14	128
F-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 14	129

LIST OF FIGURES (Continued)

	Page
F-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 14	130
F-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 14	131
G-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 15	142
G-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 15	143
G-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 15	144
G-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 15	145
G-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 15	146
G-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 15	147
H-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 16	158
H-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 16	159
H-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 16	160
H-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 16	161
H-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 16	162
H-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 16	163

LIST OF TABLES

	Page
1 - Ship and Model Characteristics, R/V ATHENA Represented by Model 5365	29
2 - Experimental Program	30
A-1 - Input Data for Harmonic Analysis for R/V ATHENA, Model 5365, Experiment 3	44
A-2 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 3	45
A-3 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 3	46
A-4 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 3	47
A-5 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 3	49
A-6 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 3	50
A-7 - Input Data for Harmonic Analysis for R/V ATHENA, Model 5365, Experiment 9	52
A-8 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 9	53
A-9 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 9	54
A-10 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 9	55
A-11 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 9	57
A-12 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 9	58
B-1 - Input Data for Harmonic Analysis for R/V ATHENA, Model 5365, Experiment 10	68
B-2 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 10	69

LIST OF TABLES (Continued)

	Page
B-3 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 10	70
B-4 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 10	71
B-5 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 10	73
B-6 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 10	74
C-1 - Input Data for Harmonic Analysis for R/V ATHENA, Model 5365, Experiment 11	84
C-2 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 11	85
C-3 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 11	86
C-4 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 11	87
C-5 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 11	89
C-6 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 11	90
D-1 - Input Data for Harmonic Analysis for R/V ATHENA, Model 5365, Experiment 12	100
D-2 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 12	101
D-3 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 12	102
D-4 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 12	103
D-5 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 12	105
D-6 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 12	106

LIST OF TABLES (Continued)

Page

E-1 - Input Data for Harmonic Analysis for R/V ATHENA with Bass Dynamometer Boat, Experiment 13	116
E-2 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 13	117
E-3 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 13	118
E-4 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 13	119
E-5 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 13	121
E-6 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 13	122
F-1 - Input Data for Harmonic Analysis for R/V ATHENA with Bass Dynamometer Boat, Experiment 14	132
F-2 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 14	133
F-3 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 14	134
F-4 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 14	135
F-5 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 14	137
F-6 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 14	138
G-1 - Input Data for Harmonic Analysis for R/V ATHENA with Bass Dynamometer Boat, Experiment 15	148
G-2 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 15	149
G-3 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 15	150

LIST OF TABLES (Continued)

	Page
G-4 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 15	151
G-5 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 15	153
G-6 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 15	154
H-1 - Input Data for Harmonic Analysis for R/V ATHENA with Bass Dynamometer Boat, Experiment 16	164
H-2 - Listing of the Mean Velocity Component Ratios, the Mean Advance Angles and Other Derived Quantities at the Experimental and Interpolated Radii for Experiment 16	165
H-3 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Experimental Radii for Experiment 16	166
H-4 - Harmonic Analyses of Longitudinal Velocity Component Ratios at the Interpolated Radii for Experiment 16	167
H-5 - Harmonic Analyses of Tangential Velocity Component Ratios at the Experimental Radii for Experiment 16	169
H-6 - Harmonic Analyses of Tangential Velocity Component Ratios at the Interpolated Radii for Experiment 16	170

NOTATION

<u>CONVENTIONAL SYMBOL</u>	<u>SYMBOL APPEARING ON PLOTS</u>	<u>DEFINITION</u>
A_N	COS COEF	The cosine coefficient of the N^{th} harmonic*
B_N	SIN COEF	The sine coefficient of the N^{th} harmonic*
D	---	Propeller diameter
J_V	---	Apparent advance coefficient $J_V = \frac{V}{nD}$ (dimensionless)
N	N	Harmonic number
n	---	Propeller revolutions
r/R or x	Radius or RAD.	Distance (r) from the propeller axis expressed as a ratio of the propeller radius (R)
V	V	Actual model or ship velocity
$v_b(x, \theta)$	---	Resultant inflow velocity to blade for a given point
$\bar{v}_b(x)$	---	Mean resultant inflow velocity to blade for a given radius
$v_r(x, \theta)$	VR	Radial component of the fluid velocity for a given point (positive toward the shaft centerline)
$\bar{v}_r(x)$	---	Mean radial velocity component for a given radius
$v_r(x, \theta)/V$	VR/V	Radial velocity component ratio for a given point
$\bar{v}_r(x)/V$	VRBAR	Mean radial velocity component ratio for a given radius
$v_t(x, \theta)$	VT	Tangential component of the fluid velocity for a given point (positive in a counterclockwise direction looking forward)

*See footnote on the following page

NOTATION (Continued)

$\bar{v}_t(x)$	---	Mean tangential velocity component for a given radius
$v_t(x, \theta)/v$	VT/V	Tangential velocity component ratio for a given point
$\bar{v}_t(x)/v$	VTBAR	Mean tangential velocity component ratio for a given radius
$(\tilde{v}_t(x)/v)_N$	AMPLITUDE	Amplitude (B_N for single screw symmetric; C_N otherwise) of Nth harmonic of the tangential velocity component ratio for a given radius*
$v_x(x, \theta)$	VX	Longitudinal (normal to the plane of survey) component of the fluid velocity for a given point (positive in the astern direction)
$\bar{v}_x(x)$	---	Mean longitudinal velocity component for a given radius
$v_x(x, \theta)/v$	VX/V	Longitudinal velocity component ratio for a given point
$\bar{v}_x(x)/v$	VXBAR	Mean longitudinal velocity component ratio for a given radius
$(\tilde{v}_x(x)/v)_N$	AMPLITUDE	Amplitude (A_N for single screw symmetric; C_N otherwise) of Nth harmonic of the longitudinal velocity component ratio for a given radius*
ϕ_N	PHASE ANGLE	Phase Angle of Nth harmonic*

*The harmonic amplitudes of any circumferential velocity distribution $f(\theta)$ are the coefficients of the Fourier Series:

$$\begin{aligned} f(\theta) &= A_0 + \sum_{N=1}^{\infty} A_N \cos(N\theta) + \sum_{N=1}^{\infty} B_N \sin(N\theta) \\ &= A_0 + \sum_{N=1}^{\infty} C_N \sin(N\theta + \phi_N) \end{aligned}$$

NOTATION (Continued)

$1-w(x)$

$1-WX$

Volumetric mean velocity ratio
from the hub to a given radius

$$1-w(r/R) = \frac{\int_{r_{\text{hub}}/R}^{r/R} (\bar{v}_{x_c}(x)/V) \cdot x \cdot dx}{(r/R)^2 - (r_{\text{hub}}/R)^2}$$

where $\bar{v}_{x_c}(x)/V = \rho \int_0^{\pi} \left[\frac{v_{x_c}(x, \theta)/V}{2 \pi V} \right] d\theta$

and $v_{x_c}(x, \theta)/V = (v_x(x, \theta)/V) - (v_t(x, \theta)/V) \tan(\hat{\beta}(x, \theta))$

$1-w_v(x)$

$1-WVX$

Volumetric mean velocity ratio from
the hub to a given radius (without the
tangential velocity correction)

$$1-w(r/R) = \frac{\int_{r_{\text{hub}}/R}^{r/R} (\bar{v}_x(x)/V) \cdot x \cdot dx}{(r/R)^2 - (r_{\text{hub}}/R)^2}$$

$\beta(x, \theta)$

Advance angle in degrees for a given
point

$\bar{\beta}(x)$

BBAR

Mean advance angle in degrees for a
given radius

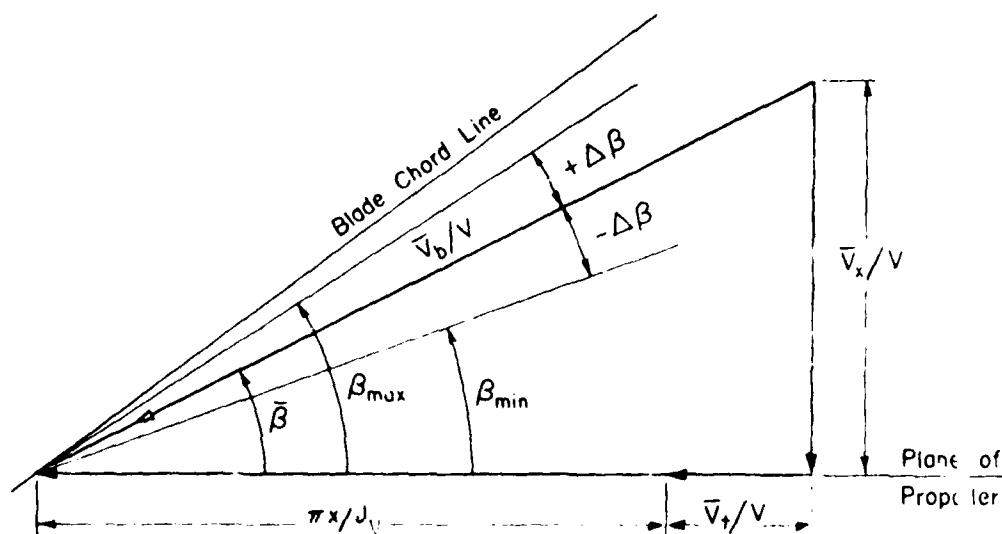
$+\Delta \beta$

BPOS

Variation of the maximum advance angle
from the mean for a given radius

NOTATION (Continued)

$-\Delta\beta$	BNEG	Variation of the minimum advance angle from the mean for a given radius
θ	Angle in Degrees	Position angle (angular coordinate) in degrees



VELOCITY DIAGRAM OF BETA ANGLES

ENGLISH/SI EQUIVALENTS

ENGLISH

SI

1 inch	25.400 millimeters [0.0254 m (meters)]
1 foot	0.3048 m (meters)
1 foot per second	0.3048 m/sec (meters per second)
1 knot	0.5144 m/sec (meters per second)
1 pound (force)	4,4480 N (Newtons)
1 degree (angle)	0.01745 rad (radians)
1 horsepower	0.7457 kW (kilowatts)
1 long ton	1.016 metric tons or 1016 kilograms
1 inch water (60°F)	248.8 pa (pascals)

ABSTRACT

This report describes a series of model experiments conducted as part of the overall project of the David Taylor Naval Ship R&D Center (DTNSRDC) to adapt controllable pitch propellers to the needs of high speed combatant ships. The first set of experiments was conducted on a model of the R/V ATHENA, with and without the port propeller operating. The second set of experiments repeated the first, except that the Bass Dynamometer Boat was mounted aft of the model. The third set was a series of idealized wake distribution experiments, in which the model was removed and the pitot rake was mounted upstream of the Bass Boat. The effect of an operating port propeller on the mean starboard wake distribution was small. The presence of the Bass Boat behind the ATHENA model, however, affects both the mean values and the harmonic content of the wake. Finally, one idealized mean wake distribution was shown to be weakly dependent on speed, and the harmonic content of wakes at two different speeds differed by less than three percent.

ADMINISTRATIVE INFORMATION

The experimental program was initiated and funded by the Naval Sea Systems Command (NAVSEA 05R) under Task Area S0379001. This work was performed at the David Taylor Naval Ship R&D Center (DTNSRDC) under work unit number 1524-641. The preliminary data analysis was performed by Chi Associates, Inc. (CAI) under contract to DTNSRDC.

INTRODUCTION

As part of its overall project to adapt controllable pitch propellers to the needs of high speed combatant ships, the David Taylor Naval Ship Research and Development Center (DTNSRDC) conducted a full-scale wake survey aboard the R/V ATHENA in September 1977 as reported by Day et al¹. The specific goal of this project was to obtain propeller disk velocity component ratios in the wake of a full-scale ship. In addition, propeller blade loading experiments have been completed for the R/V ATHENA.

Subsequent to the full-scale wake trials, a series of wake surveys were conducted on a model of the R/V ATHENA. These experiments were designed to evaluate the model wake at one propeller location, both with and without the other propeller operating. In addition, wake survey experiments were conducted with and without the Bass Dynamometer Boat mounted aft of the model. The Bass Dynamometer Boat was used in the blade loading experiments to drive the propeller and dynamometry systems from behind the model. The wake information was necessary to account for the effect of the Bass Boat on the flow into the propeller in the analysis of the blade loading experiments. Several idealized wake distributions were measured, and will be used for blade loading calculations for a propeller operating in an idealized wake. An idealized wake is the breaking down of a wake field into a purely longitudinally dominated wake by a wake screen or a purely tangentially dominated wake by inclining the flow angle. The blade loading calculations for the R/V ATHENA will be compared with experimental force measurements on a model propeller to help determine the validity of the load calculation method and will be reported later.

¹ References are listed on page 16.

EXPERIMENTAL PROCEDURE

The experiments described in this report measured the propeller disk velocity components under a variety of operating conditions. In the first set of experiments (Experiments 3, 9 and 10), wake measurements were obtained from the starboard propeller plane of the model with, and without the port propeller operating. In the second set (Experiments 11 and 12), measurements were taken with the model followed by the Bass Dynamometer Boat, with and without the port propeller operating. The third set of experiments (Experiments 13 through 16) consisted of idealized wake surveys. The ATHENA model was removed, and a pitot tube rake was mounted ahead of the Bass Dynamometer Boat. These experiments were run behind a screen which provided an idealized wake distribution.

DTNSRDC Model 5365, representing the R/V ATHENA (PG-94), was constructed to a linear ratio of 8.250, in accordance with model specifications of the Naval Sea Systems Command (NAVSEA 05R). Model and ship characteristics are presented in Table 1. The model was fitted with shafts and struts, a centerline skeg, and stabilizer fins. Model rudders were not included. DTNSRDC pitot tube rake number 7 was mounted in the model through the starboard shafting. Differential pressure gauges were used to measure the velocities in the plane of the propeller at four radial locations. A sketch of the pitot rake on the model is shown in Figure 1. The rake as fitted to Model 5365, including the five-hole spherical pitot tubes, is shown in Figure 2.

The DTNSRDC Bass Dynamometer Boat (Model 5271) was employed in all but the first three experiments. It was mounted in the same location in which it had previously been run to study unsteady propeller blade

forces behind a model, and was later mounted behind the pitot rake and wake screen.

The experimental program, as it pertains to this report, is described in Table 2. The experiments being discussed are 3 and 9 through 16. All the other experiments (1, 2, and 4 through 8) are discussed in another report by Hurwitz and Crook². Experiment 3 was a conventional wake survey experiment which measured the Model 5365 starboard wake without the port propeller operating in the initial setup. Experiment 9 repeated this test to verify that the model conditions were essentially unchanged in the second setup from the original. For Experiment 10, with the port propeller operating, the model conditions from Experiments 3 and 9 were duplicated.

Experiments 11 and 12 were again conventional wake surveys, with the pitot tube rake mounted from inside the starboard shaft; but the Bass Dynamometer Boat was attached downstream of the ATHENA model. Experiment 11 was conducted without the port propeller, and Experiment 12 with the port propeller operating. A sketch of the experimental radii taken with the pitot tube arrangement behind the hull sections is shown in Figure 3. Figures 4 and 5 are profile and quartering photographs of the pitot tube rake and the ATHENA model. Figure 6 shows the experimental setup during Experiments 11 and 12.

Experiments 13 through 16 were conducted to create idealized wakes. Data from these wake surveys were required to perform calculations of unsteady blade loads for comparison with experimental results. Experiment 13 modeled an uniform flow with the rake inclined at 20 degrees (0.349 radian), as shown in Figure 7. Experiment 14 was performed to measure the flow behind a one-cycle wake screen with the bass dynamometer boat

and rake both at zero degree inclination. Figures 8 through 10 show the wake screen used, and Figures 11 and 12 show the experimental setups. Finally, Experiments 15 and 16 were uniform flow surveys at ten degrees (0.175 radian) inclination of the bass dynamometer boat and rake at model speeds corresponding to full-scale speeds of 17.2 and 8.6 knots (8.8 and 4.4 m/s), respectively. Also the single cycle wake screen was removed during Experiments 15 and 16.

The full-scale propeller disk was 6 feet (1.83 meters) in diameter. The radii at which measurements were made, expressed as ratios of the propeller radius (r/R), were 0.456, 0.633, 0.781, and 0.963. The plane in which the velocity measurements were taken was the starboard propeller plane located 146.2 feet (44.56 meters) aft of the forward perpendicular. The ATHENA displacement was 263 tons (267 metric tons), and the model trim was locked at a speed corresponding to a 20 knot (10.3 meter/second) ship speed, with the pitot rake in the zero degree position.

The wake measurement system consisted of a pitot tube rake and four differential pressure gages. The rake has five 5-hole spherical pitot tubes mounted in a common housing. Measurements were not made using the innermost pitot tube because of the flow interference between the pitot tube and the propeller hub. Figure 1 shows the arrangement of the rake and the pitot tubes. A description of the use and the calibration of 5-hole tubes is given by Hadler and Cheng.³

The carriage computer integrated the four pressure signals from each pitot tube, the model speed, and the angular position of the rake, over a 5-second period. Digital voltmeters and frequency counters monitored the computer values. The computer collected the pressure data for each of the

four pitot tubes. The rake was then rotated to a new angle, and the procedure was repeated until data were obtained throughout the entire rotation of the rake in the propeller disc.

Velocity component ratios were computed from the pressure data using established computer programs. The circumferential distributions of the longitudinal, tangential, and radial velocity component ratios were plotted for each radial location. Plots of the data were generated by a Control Data Corporation (CDC) Computer using a CALCOMP Plotter. Data were checked for random errors and agreement with previous experiments. Interpolation of the velocity component ratios in the radial and circumferential directions was made. This process yielded interpolated data every 2.5 degrees (0.044 radians) for four experimental radii, and for additional selected radii (interpolated radii). The mean longitudinal, tangential, and radial velocity component ratios; the volumetric mean wake; and the mean and extreme values of the advance angles were computed and are presented in this report. The advance angles were calculated using an advance coefficient, J_V , of 0.739. Explanation of this terminology and a diagram showing the relationship among the velocity vectors, the advance coefficient, and the advance angles are presented in the "Notation" section of this report.

Harmonic analyses of the circumferential distributions of the longitudinal and tangential velocity component ratios were computed for the experimental data. The harmonic content was determined by Fourier series analysis. The results of the harmonic analyses are presented as amplitudes and phase angles of a sine series.

ACCURACY ASSESSMENT

The instrumentation accuracy and the repeatability of wake survey experiments have been discussed in detail by Hadler and Cheng,³ and Day⁴.

The mean velocity component ratios and the harmonic amplitudes of these ratios all repeat within one percent of the model velocity. The accuracy of the entire velocity survey measurement system was also determined to be one percent of the model velocity, except in flow regions where steep velocity gradients occur, such as behind a shaft strut. In these high gradient regions, the accuracy was shown to be much less. These error bounds were derived for wake surveys calculated at model speeds of at least four knots, with the accuracy decreasing at lower speeds.

All data comparisons which follow will be referenced to the model velocity. Since the accuracy is on the order of one percent of the model velocity, higher order harmonics, whose amplitudes tend to be less than one percent of model velocity, cannot be considered to be as accurate as the mean values and lower order harmonics. The small higher order harmonics do not make a significant contribution to the reproduction of the velocity component ratios, though they do contribute to moments and forces calculated from the wake harmonics.

PRESENTATION AND DISCUSSION OF RESULTS

EXPERIMENTS 3, 9, AND 10 - EFFECT OF OPERATING PORT PROPELLER ON CONVENTIONAL WAKE SURVEYS

Experiments 3, 9, and 10 were conventional wake surveys of the starboard propeller plane of the R/V ATHENA (Model 5365). Experiment 3 was conducted without the port propeller operating, Experiment 9 was a check of

Experiment 3, and Experiment 10 was identical to Experiment 3, except that the port propeller was operating.

A listing of the input data for Experiment 3 (without the port propeller operating) is presented in Table A-1, of Appendix A. The circumferential distribution of the longitudinal, tangential, and radial velocity component ratios from Experiment 3 are shown in graphical form for each pitot tube radius in Figures A-1 through A-4. Included in these figures are the data from Experiment 9, which agree with the data for Experiment 3. The mean longitudinal (VXBAR), tangential (VTBAR), and radial (VRBAR) velocity component ratios, and the volumetric mean wake (1-WX) are presented in Table A-2. These quantities, except the radial mean, are presented graphically in Figure A-5.

The calculated mean values of the advance angle (BBAR), and the extreme variations (BPOS and BNNEG) are shown in Figure A-6 and Table A-2. Tables A-3 through A-6 present the harmonic analyses of the circumferential distributions of the longitudinal and tangential velocity component ratios at the experimental and interpolated radii.

The results are presented in a similar form for Experiment 10 (with the port propeller operating). The circumferential distributions of the velocity component ratios are presented in Appendix B as Figures B-1 through B-4, the input data are listed in Table B-1, and mean values are presented in Figures B-5 and B-6, and Table B-2. The results of the harmonic analyses are presented in Tables B-3 through B-6.

When the results from Experiments 3 and 10 are compared, only small differences are seen. The mean values for the input radii of longitudinal,

tangential, and radial velocity listed in Tables A-2 and B-2 agree in most cases to within one percent of the freestream velocity. The circumferential mean values from Experiment 3 are not consistently higher or lower than those from Experiment 10.

The results of the harmonic analyses compare just as favorably. For example, at the input radii, the amplitudes of all harmonics of the longitudinal, tangential, and radial velocity component ratios differ by less than one percent of freestream. The phase angles, however, are different at several radii. The good agreement of the data, all within experimental accuracy, for Experiments 3 and 10, indicates only a small effect on the starboard wake is realized when the port propeller is operating.

EXPERIMENTS 11 AND 12 - EFFECT OF OPERATING PORT PROPELLER IN FRONT OF BASS DYNAMOMETER BOAT MOUNTED DOWNSTREAM

Experiments 11 and 12 were conventional wake surveys on the starboard propeller plane of the R/V ATHENA (Model 5365), with the Bass Dynamometer Boat (Model 5271) mounted downstream. This setup physically modeled the unsteady blade force experiments mentioned previously. Experiment 11 was conducted without the port propeller operating, and Experiment 12 was identical to Experiment 11, except that the port propeller was operating.

The circumferential distribution of the longitudinal, tangential, and radial velocity component ratios for Experiment 11 are shown graphically for each pitot tube radius in Appendix C as Figures C-1 through C-4. A listing of the input data is presented in Table C-1. The mean longitudinal, tangential, and radial velocity component ratios and the volumetric mean wake are presented in Figure C-5 and Table C-2.

The calculated mean and extreme values of the advance angles are also shown in Table C-2 and in Figure C-6. Tables C-3 through C-6 present the results of harmonic analyses of the circumferential distributions of the longitudinal and tangential velocity component ratios at the experimental and interpolated radii.

The results are presented in a similar form for Experiment 12. The circumferential distributions of the velocity component ratios are presented in Figures D-1 through D-4, the input data is listed in Table D-1, and the mean values are presented in Figures D-5 and D-6, and in Table D-2. The harmonic analyses are presented in Tables D-3 through D-6.

When the results from Experiments 11 and 12 are compared, only small differences are seen. The mean values of the longitudinal, tangential, and radial velocity component ratios for the input radii all agree to within one percent of freestream. At each radius, the longitudinal mean velocity component ratio is slightly higher with the port propeller operating (Experiment 12). However, the values are so nearly the same that no conclusions can be drawn regarding the trend.

The results of the harmonic analyses also compare favorably. For example, at the input radii, the amplitudes of the first harmonic of the longitudinal velocity component ratios differ less than one percent of freestream. The phase angles, however, are different for several of the radii. The harmonics of the tangential velocity component ratios also show good agreement, with the differences being very small compared to freestream with good phase angle agreement. These results further verify the earlier conclusions that with the port propeller operating only a small effect on the starboard wake distribution is realized.

EXPERIMENTS 9 AND 11 - EFFECT OF BASS DYNAMOMETER BOAT MOUNTED DOWNSTREAM

The results already presented from Experiments 9 and 11 can be compared to determine the effect of the Bass Dynamometer Boat on the ATHENA model wake. The differences are very significant. The mean values of the longitudinal velocity component ratios in Tables A-2 and C-2 showed differences of 10 to 20 percent of the model velocity. The longitudinal velocity component ratios were always smaller with the Bass Dynamometer Boat behind the ATHENA model, as expected. The tangential and radial mean ratios also changed, though no consistent trend was evident.

The harmonics of the longitudinal velocity component ratios showed some differences. For example, the amplitude of the first harmonic is slightly less when the Bass Boat is present; however, the fifth harmonic shows the opposite trend, that is, slightly higher when the Bass Boat is present. The tangential harmonics differ only slightly. For example, the amplitudes of the first harmonic taken with the Bass Boat differed by about 2 percent of freestream when compared to the amplitudes of the first harmonic without the Bass Boat.

EXPERIMENT 13 - IDEALIZED WAKE SURVEY AT LARGE INFLOW ANGLE

Experiment 13 was an idealized wake survey conducted with the Bass Dynamometer Boat downstream of only the pitot tube rake, that is, no ATHENA model was present for this experiment or single cycle wake screen. The rake inclination to the direction of travel was 20 degrees (0.349 radians).

The circumferential distribution of the longitudinal, tangential, and radial component ratios for Experiment 13 are shown graphically for each pitot tube radius in Figures E-1 through E-4. A listing of the input data

is presented in Table E-1. The mean longitudinal, tangential, and radial velocity component ratios and the volumetric mean wake are presented in Table E-2 and Figure E-5.

The calculated mean and extreme values of the advance angles are shown in Figure E-6 and Table E-2. Tables E-2 through E-6 present the results of harmonic analyses of the circumferential distributions of the longitudinal and tangential velocity component ratios.

The mean values presented in Table E-2 are not uniform for all radii, though all differences are less than three percent of model velocity. The circumferential mean values of velocity components for this experiment indicate that the Bass Dynamometer Boat not only retards the flow, but also has a small effect on the radial distribution of the flow.

EXPERIMENT 14 - IDEALIZED WAKE SURVEY WITHOUT ANY INFLOW ANGLE BEHIND A WAKE SCREEN

Experiment 14 was an idealized wake survey conducted with the Bass Dynamometer Boat mounted at zero degree inclination downstream of a one-cycle wake screen. The results are presented in a form similar to Experiment 13. The circumferential velocity component distributions are presented in Figures F-1 through F-4, the input data are listed in Table F-1, and the mean values are presented in Figures F-5 and F-6 and Table F-2. The results of harmonic analyses are presented in Tables F-3 through F-6.

The circumferential distributions shown in Figures F-1 through F-4 indicate that the wake screen did indeed produce a one-cycle wake with a peak-to-peak variation to longitudinal velocity component ratio of about 0.3. Table F-2 indicates that the mean longitudinal velocity component

ratio is about 0.63. The longitudinal harmonics presented in Table F-3 indicate that even though the wake has only one cycle the higher harmonics are still significant.

EXPERIMENTS 15 AND 16 - EFFECT OF SPEED ON IDEALIZED WAKE SURVEY

Experiments 15 and 16 were idealized wake surveys conducted with only the Bass Dynamometer Boat downstream of the pitot tube rake. There was no single cycle wake screen during these experiments. The rake inclination to the direction of travel was ten degrees for both experiments. Experiment 16 was identical to Experiment 15, except that the towing speed of Experiment 16 was one-half that of Experiment 15.

The circumferential distribution of the longitudinal, tangential, and radial velocity component ratios for Experiment 15 are shown in Figures G-1 through G-4. A listing of the input data is presented in Table G-1. The mean longitudinal, tangential, and radial velocity component ratios and the volumetric mean wake are presented in Table G-2 and Figure G-5.

The calculated mean and extreme values of the advance angles are shown in Figure G-6 and Table G-2. Tables G-3 through G-6 present the results of harmonic analyses of the circumferential distributions of the longitudinal and tangential velocity component ratios at the experimental and interpolated radii.

The results are presented in similar form for Experiment 16. The circumferential velocity component distributions are presented in Figures H-1 through H-4, the input data are listed in Table H-1, and the mean values are presented in Figures H-5 and H-6 and in Table H-2. The results of harmonic analyses are presented in Tables H-3 through H-6.

When the results from Experiments 15 and 16 are compared, only small differences are noted. The differences between mean values presented in Tables G-2 and H-2 are not significant with a maximum difference of about one percent of model velocity in the longitudinal mean, and a maximum difference in the tangential and radial means of less than one percent. The harmonics do not compare as favorably as the mean values, although the amplitudes of the first harmonic of the tangential velocity component ratios at the input radii differ by less than three percent of model velocity. The amplitudes of the first harmonic for the longitudinal ratios are in better agreement with the maximum difference being less than one percent of model velocity. These small differences indicate this idealized wake is only weakly dependent on speed.

CONCLUSIONS

- (1) The effect due to the port propeller operating on the starboard mean wake distribution is small. This effect was illustrated twice and established no noticeable trends in the mean velocity component ratios.
- (2) The Bass Dynamometer Boat mounted aft of the R/V ATHENA very significantly affects the mean longitudinal velocity component ratios. These mean longitudinal velocity component ratios with and without the Bass Dynamometer Boat differ by 10 to 20 percent. The results of the harmonic analyses show smaller trends. The radial distribution of the flow is also slightly influenced.
- (3) The Bass Dynamometer Boat affects each radius differently due to the bass dynamometer blunt bow causing greater flow obstruction when at a 20 degree inclination.

(4) When a single cycle wake screen is mounted upstream of the Bass Dynamometer Boat, both at zero inclined angle, the wake screen affects the peak to peak fluctuations in the longitudinal velocity component ratios. These peak to peak fluctuation ranges are half the total mean longitudinal velocity component ratio values. The single cycle wake screen affects the higher harmonics significantly.

(5) The idealized flow wake surveys show a weak dependence upon velocity when the Bass Dynamometer Boat and rake are mounted at a ten degree angle of inclination to the free surface without any single cycle wake screen present.

REFERENCES

1. Day, W. G., Jr., A. M. Reed, R. B. Hurwitz, "Full-Scale Propeller Disk Wake Survey and Boundary Layer Velocity Profile Measurements on the 154-Foot Ship R/V ATHENA," DTNSRDC Ship Performance Department Report DTNSRDC/SPD-0833-01 (Sep 1980).
2. Hurwitz, R. B. and L. B. Crook, "Analysis of Wake Survey Experimental Data for Model 5365 Representing the R/V ATHENA in the DTNSRDC Towing Tank," DTNSRDC Ship Performance Department Report DTNSRDC/SPD-0833-04 (Oct 1980).
3. Hadler, J. B. and H. M. Cheng, "Analysis of Experimental Wake Data in Way of Propeller Plane of Single- and Twin- Screw Ship Models," Trans. Soc. Naval Arch. and Mar. Eng., Vol. 73, pp. 287-414 (1965).
4. Day, W. G., Jr., "Effect of Speed on the Wake in Way of the Propeller Plane for the DD 963 Class Destroyer Represented by Model 5265-1B," NSRDC Ship Performance Department Report SPD-311-37 (Jun 1975).

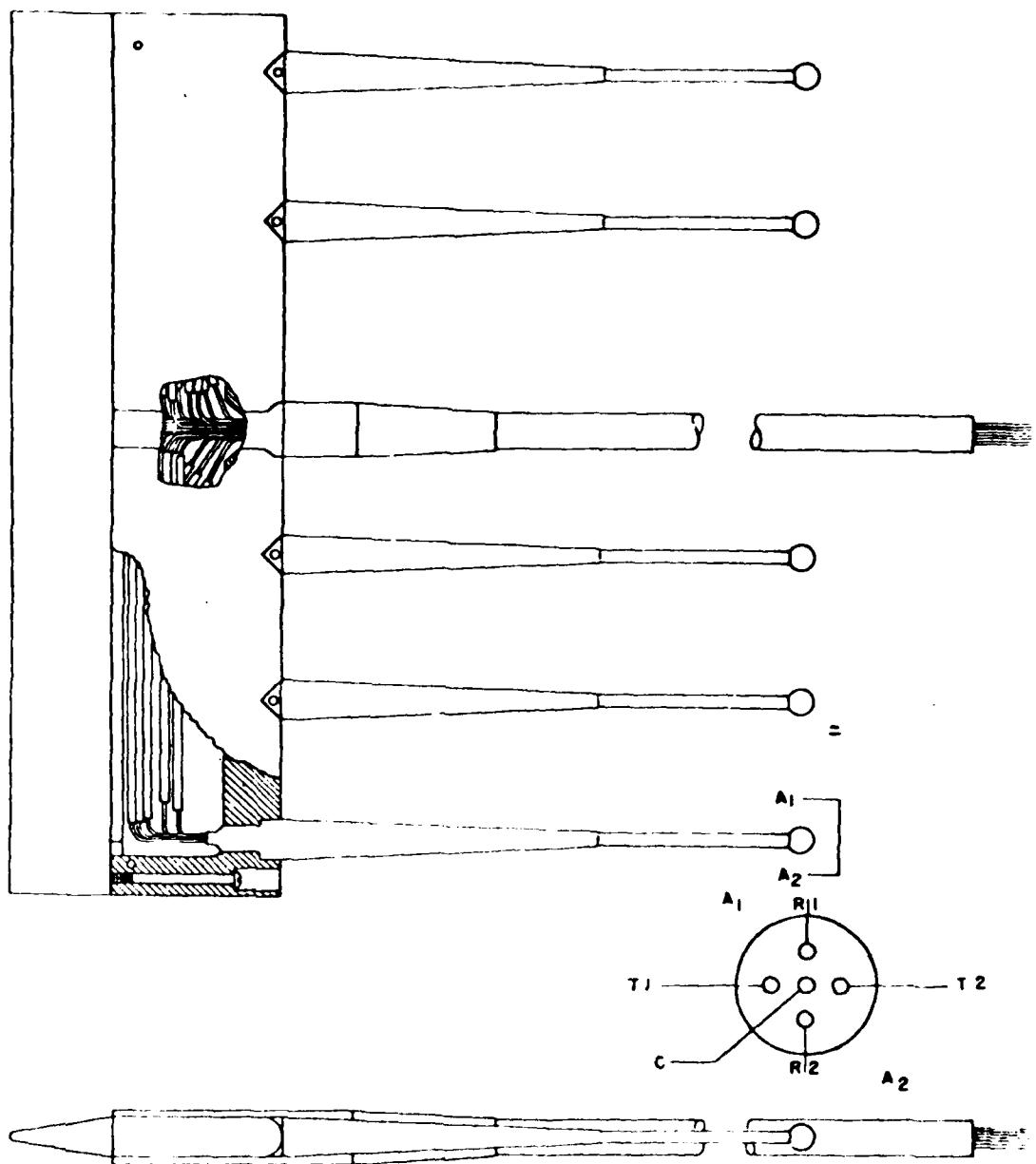
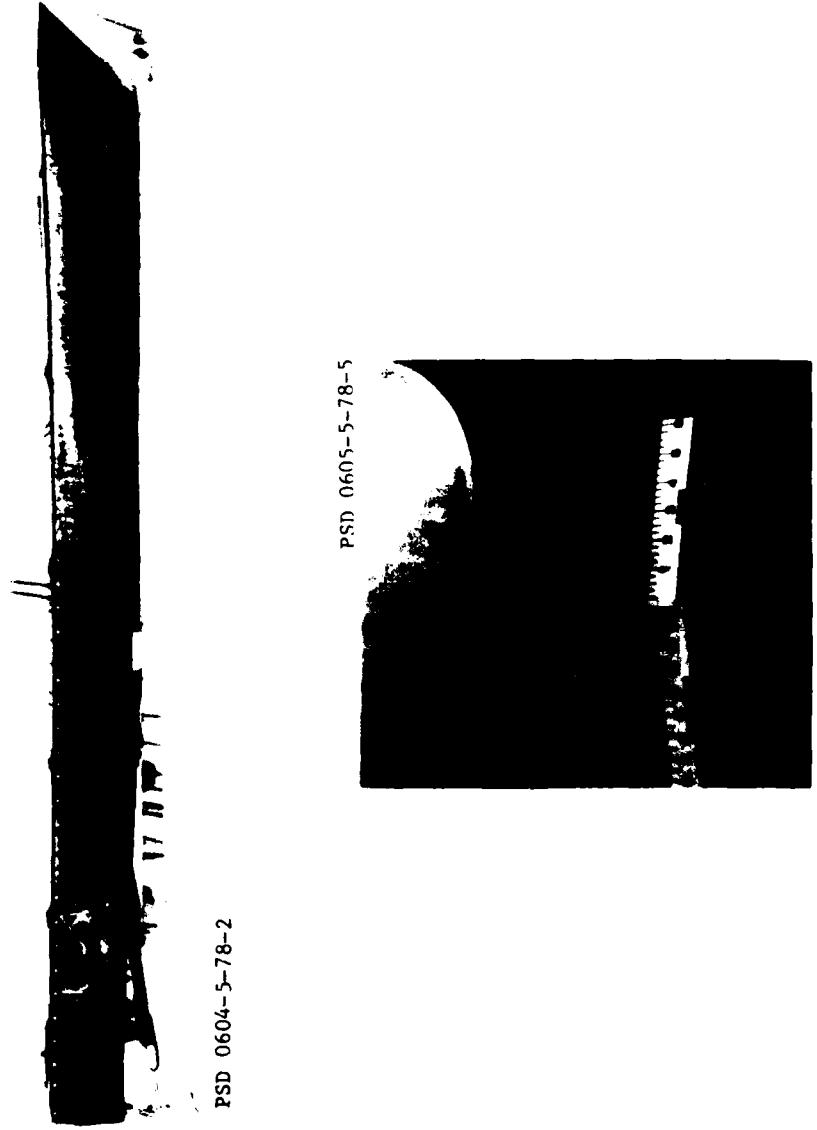


Figure 1 - Rake Arrangement Sketch Showing Five Spherical Head Pitot Tubes with Five Holes Each

Figure 2 - Rake Arrangement Photographs Showing Installation in Starboard Shaft of Model 5365 During Experiments 3 and 9 Without Port Propeller



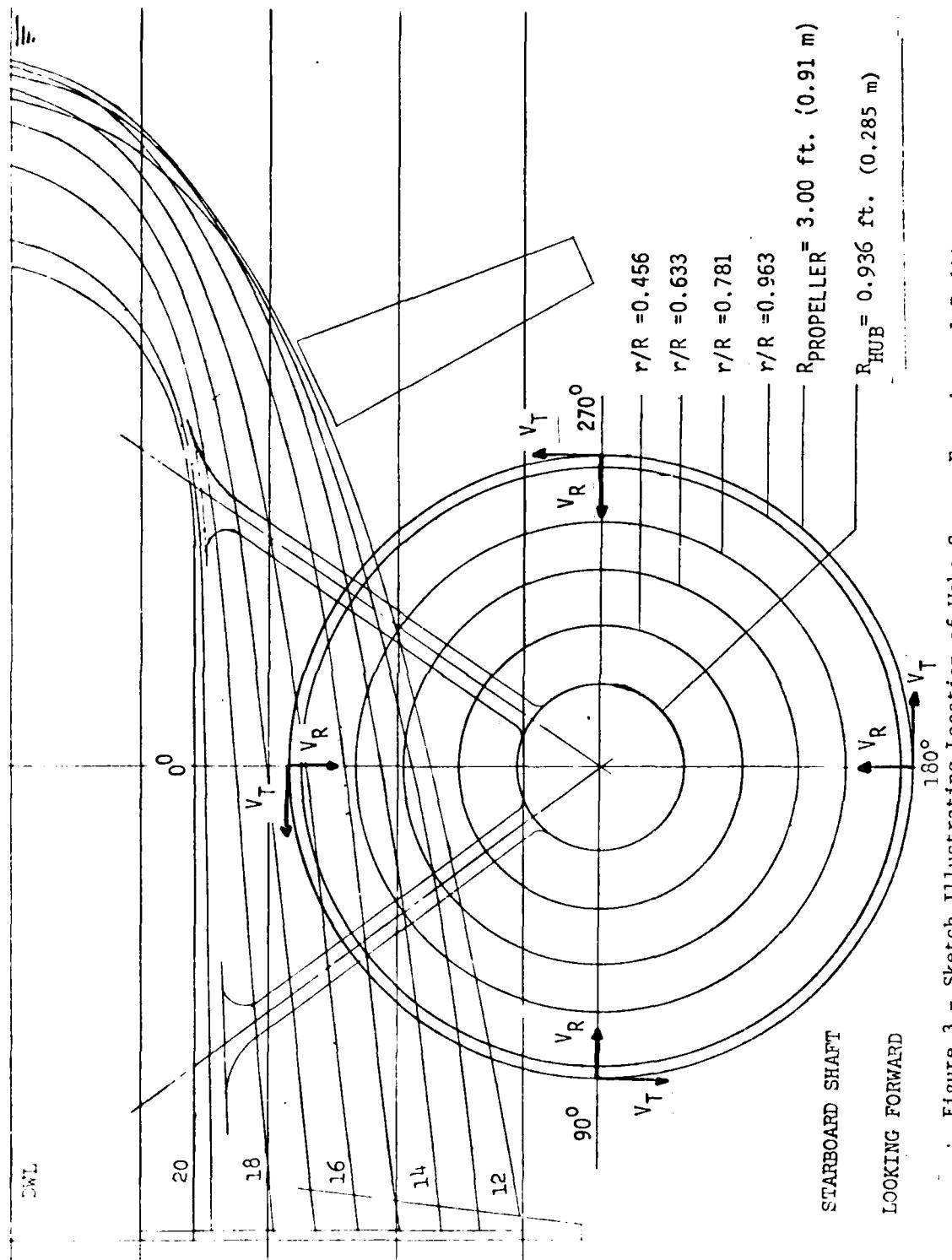


Figure 3 - Sketch Illustrating Location of Wake Survey Experimental Radii on Model 5365 Afterbody Sections Representing the R/V ATHENA

PSD 0604-5-78-9

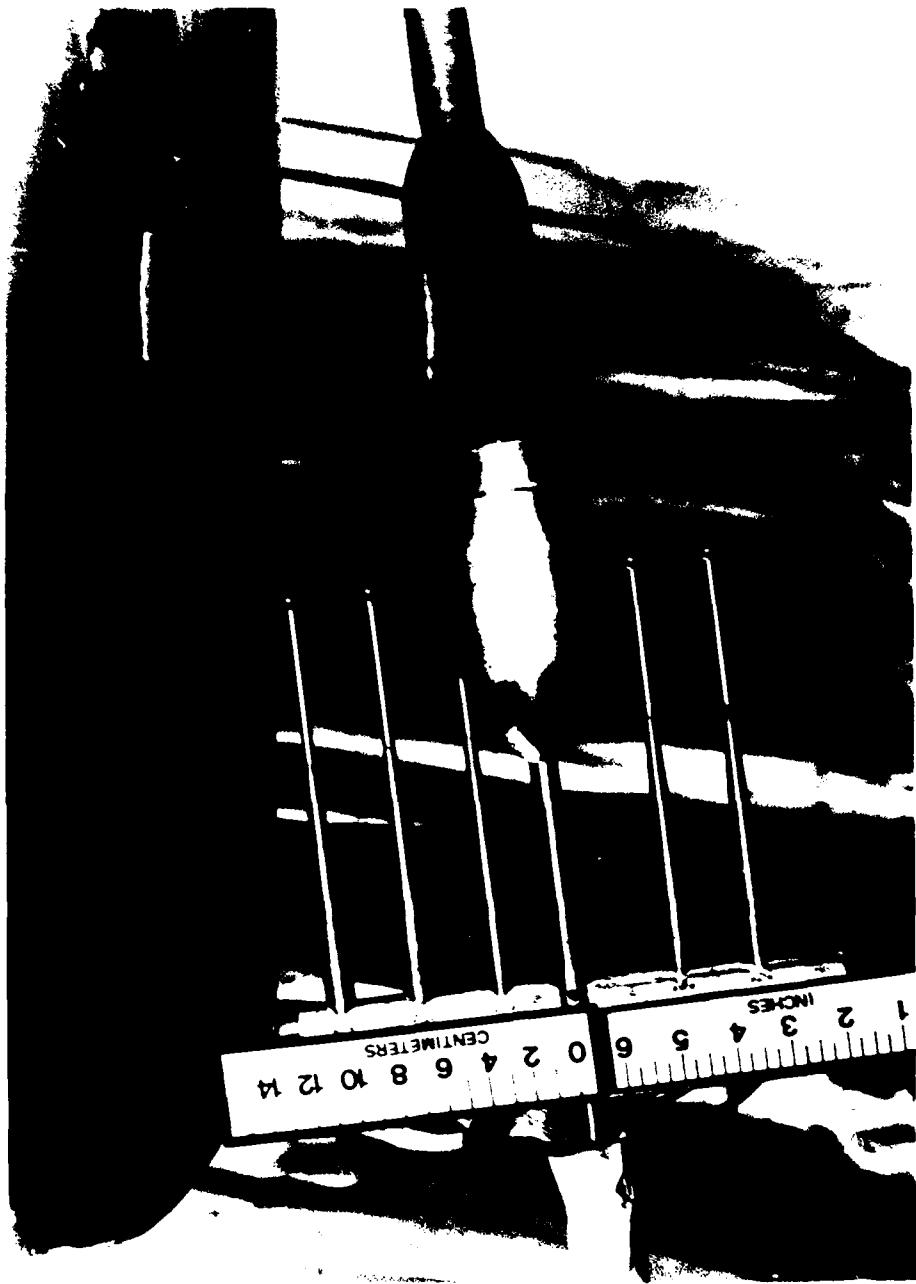


Figure 4 - Rake Arrangement Photograph Showing Closeup Profile View of Installation in
Starboard Shaft of Model 5365 Without Port Propeller



FIGURE 3 - Propeller Arrangement Photograph Showing Closeup Quartering View of Installation in the Starboard Shaft of Model 5365 Without Port Propeller

Figure 6 - Photo Arrangement Photograph Showing Installation in Bass Dynamometer Boat, Model 5271, Mounted Behind Starboard Shaft of Model 5365 With and Without Port Propeller as During Experiments 11 and 12

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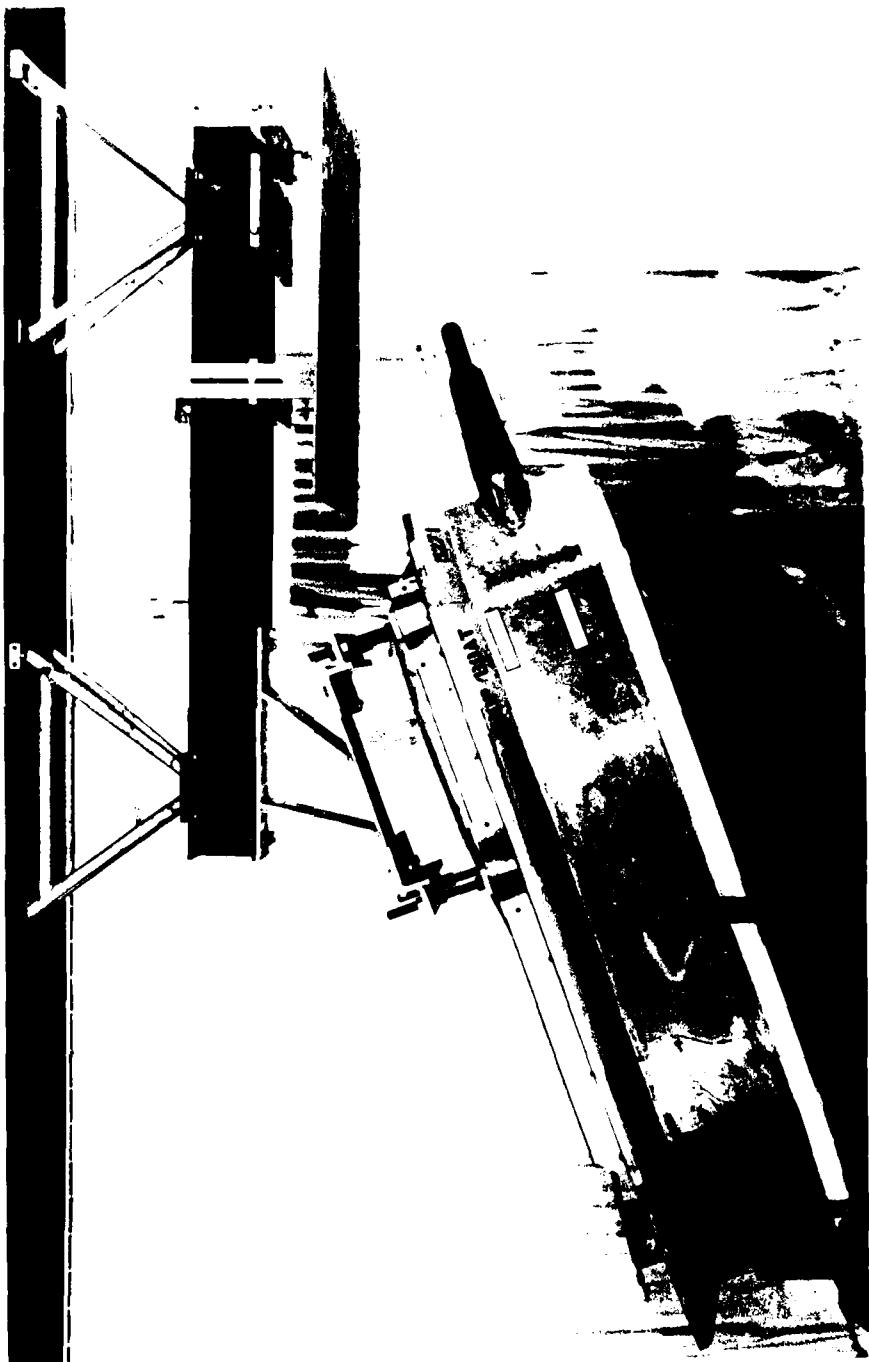


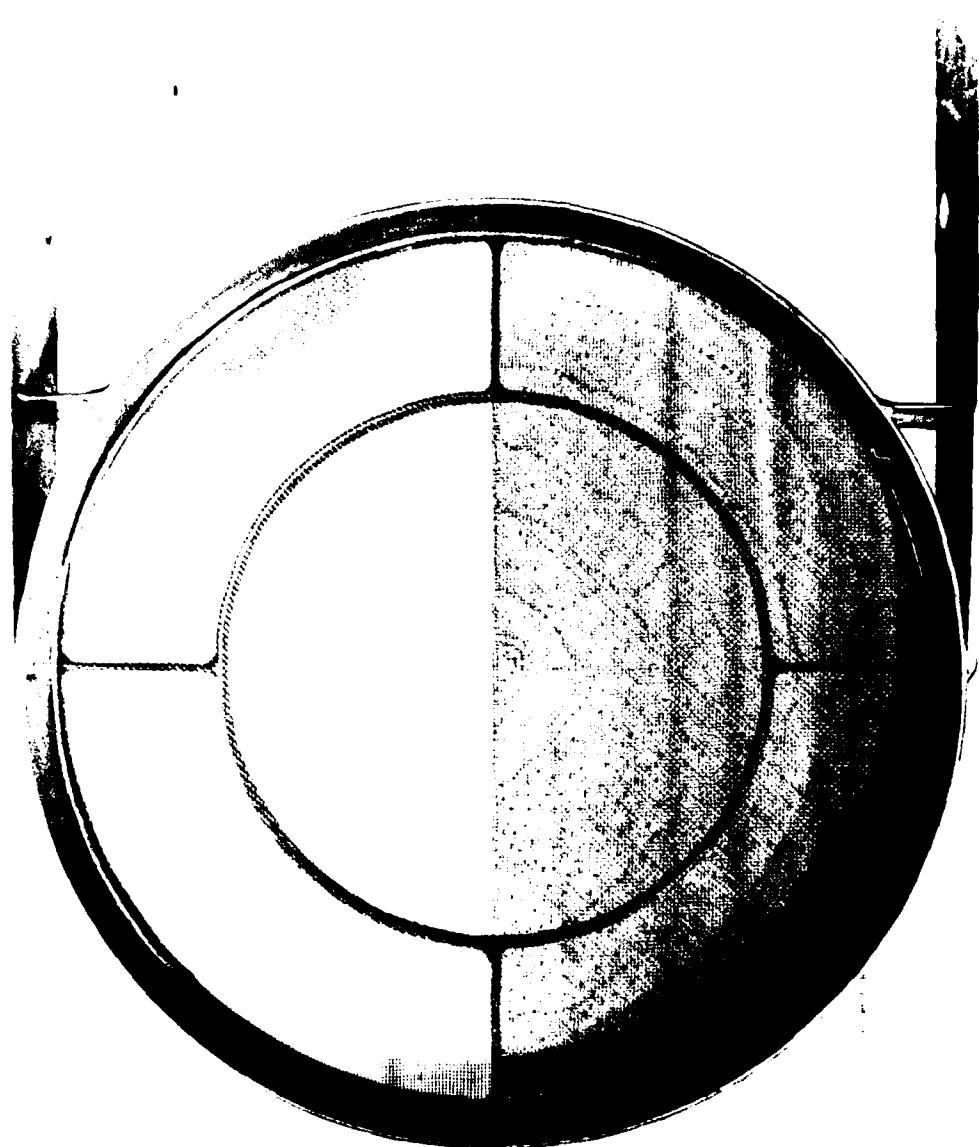
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PSD 0606-5-78-3

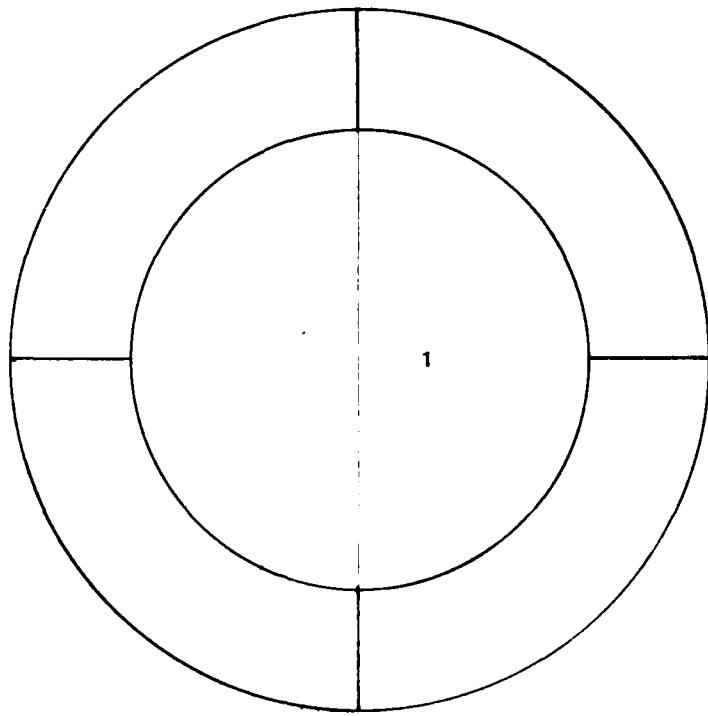
Figure 7 - Rake Arrangement Photograph Showing Bass Dynamometer Boat Mounted for 20 Degree (0.349 radian) Inclined Idealized Flow Wake Experiment 13





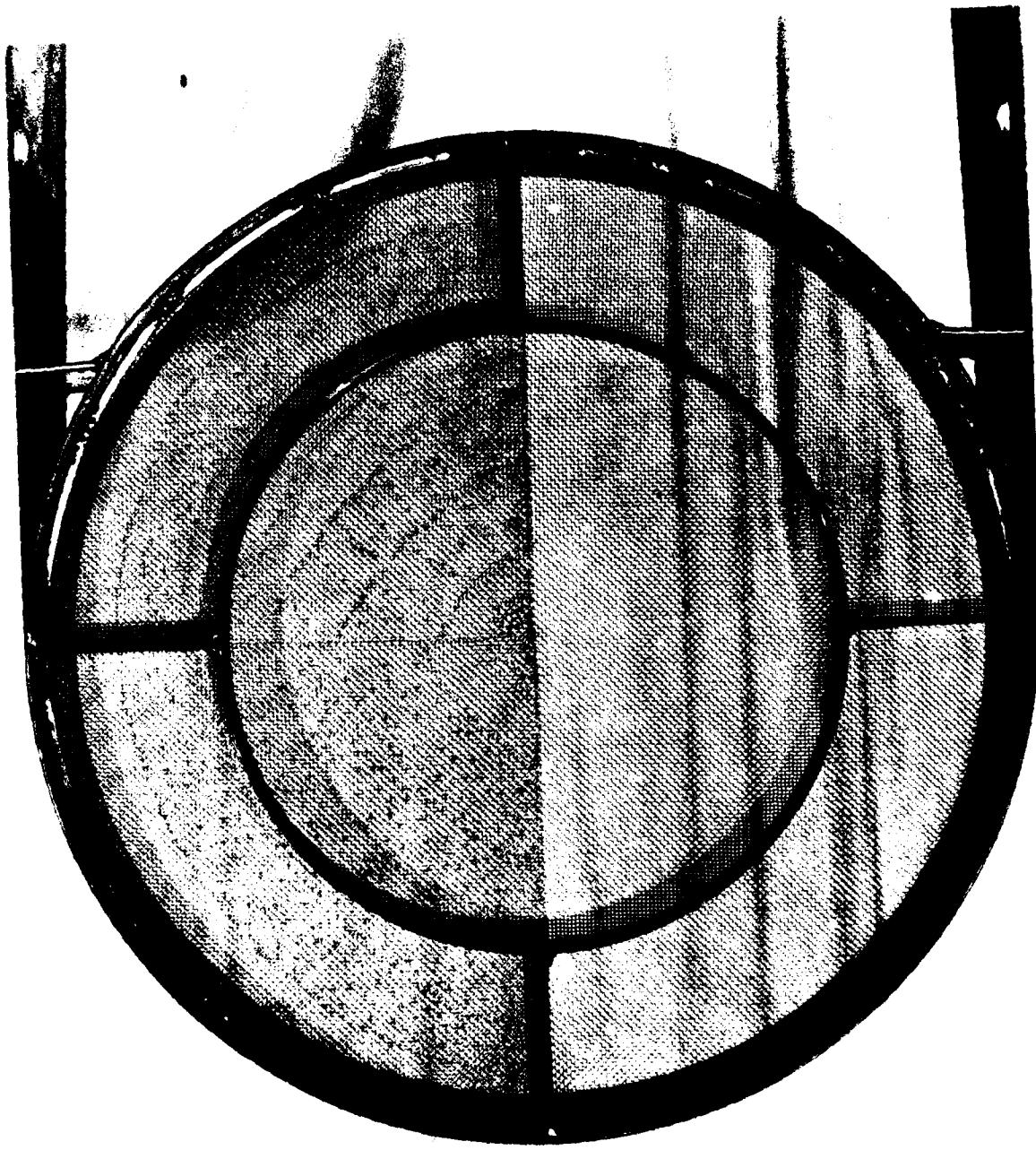
PSD 0607-5-78-1

Figure 8 - Wake Screen Photograph Showing Downstream View at Spherical Head Pitot Tubes Used for Idealized Flow Experiment 14



REGION	SCREEN SIZE	
	WIRES PER INCH	DIAMETER (inches)
SUPPORT (ALL)	16	0.009
1	20	0.011

Figure 9 - Schematic of Wake Screen Wire Sections and Sizes Used for Idealized Flow Experiment 14



PSD 0604-5-78-11

Figure 10 - Wake Screen Phototgraph Showing Upstream View Into the Flow for Idealized Flow Experiment 14

PSD 0606-5-78-7

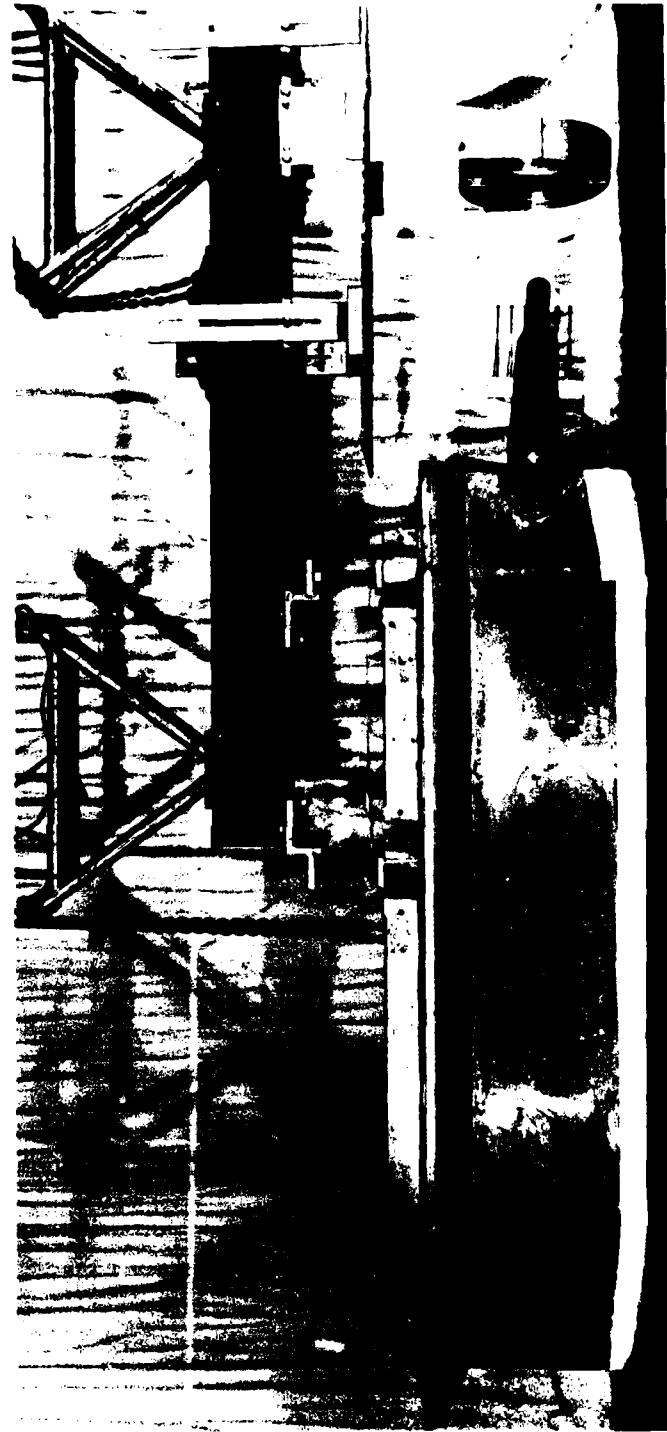


Figure 11 - Bass Dynamometer Boat Mounted Behind the Wake Screen Photograph Showing Arrangement of Pitot Tubes for Idealized Flow Experiment 14

PSD 0606-5-78-7



Figure 12 - Bass Dynamometer Boat Mounted for 10 Degree (0.174 radian) Inclined Idealized Flow Wake Photograph Showing Spacer Block Used for Experiments 15 and 16

TABLE I
Ship and Model Characteristics
R/V ATHENA Represented by Model 5365

	<u>Ship</u>	<u>Model</u>
Length Between Perpendiculars	154.0 ft (46.9m)	18.6 ft (5.7m)
Length Overall	164.5 ft (50.1m)	19.9 ft (6.1m)
Maximum Beam	24.0 ft (7.3 m)	2.9 ft (0.9m)
Displacement	263 tons (267.3 tonnes)	1020 lbs (462.6 kg)
Wetted Surface	3413 ft ² (317.1 m ²)	50.15 ft ² (4.659 m ²)
Draft	5.63 ft (1.72 m)	0.682 ft (0.208 m)
Trim by Stern	0.59 ft (0.18 m)	0.071 ft (0.022 m)
Propeller Diameter	6.0 ft (1.8 m)	8.73 in (22.2 cm)
Linear Scale Ratio	8.25	1.0

Propulsion: Twin screw, controllable pitch, 4 blades each

Appendages: Twin stabilizers, main shafts and V-struts, twin rudders,
centerline skeg

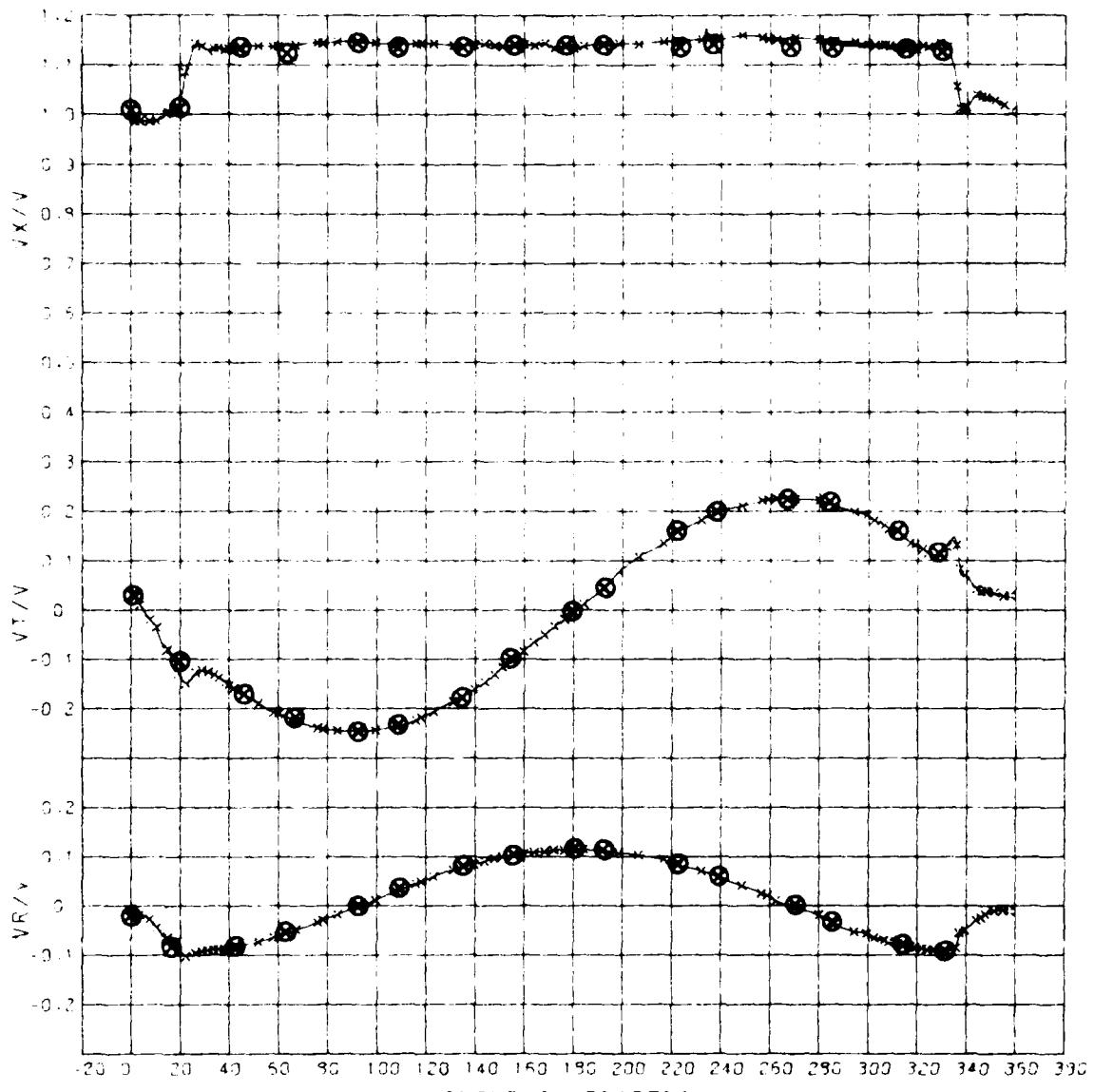
APPENDIX A
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENTS 3 AND 9

Table 2
EXPERIMENTAL PROGRAM

Experiment Number	Equivalent Ship Speed in Knots (m/s)	Shaft Inclination	Athena Model	Dynamometer Boat	Wake Screen	Port Propeller Operating
3,9	20.0 (10.3)	*	yes	no	no	no
10	20.0 (10.3)	*	yes	no	no	yes
11	20.0 (10.3)	*	yes	yes	no	no
12	20.0 (10.3)	*	yes	yes	no	yes
13	11.5 (5.9)	20°	no	yes	no	no
14	12.9 (6.6)	0°	no	yes	yes	no
15	17.2 (8.8)	10°	no	yes	no	no
16	8.6 (4.4)	10°	no	yes	no	no

* Model trim set at equivalent ship speed twenty knots (10.3 meters/second)

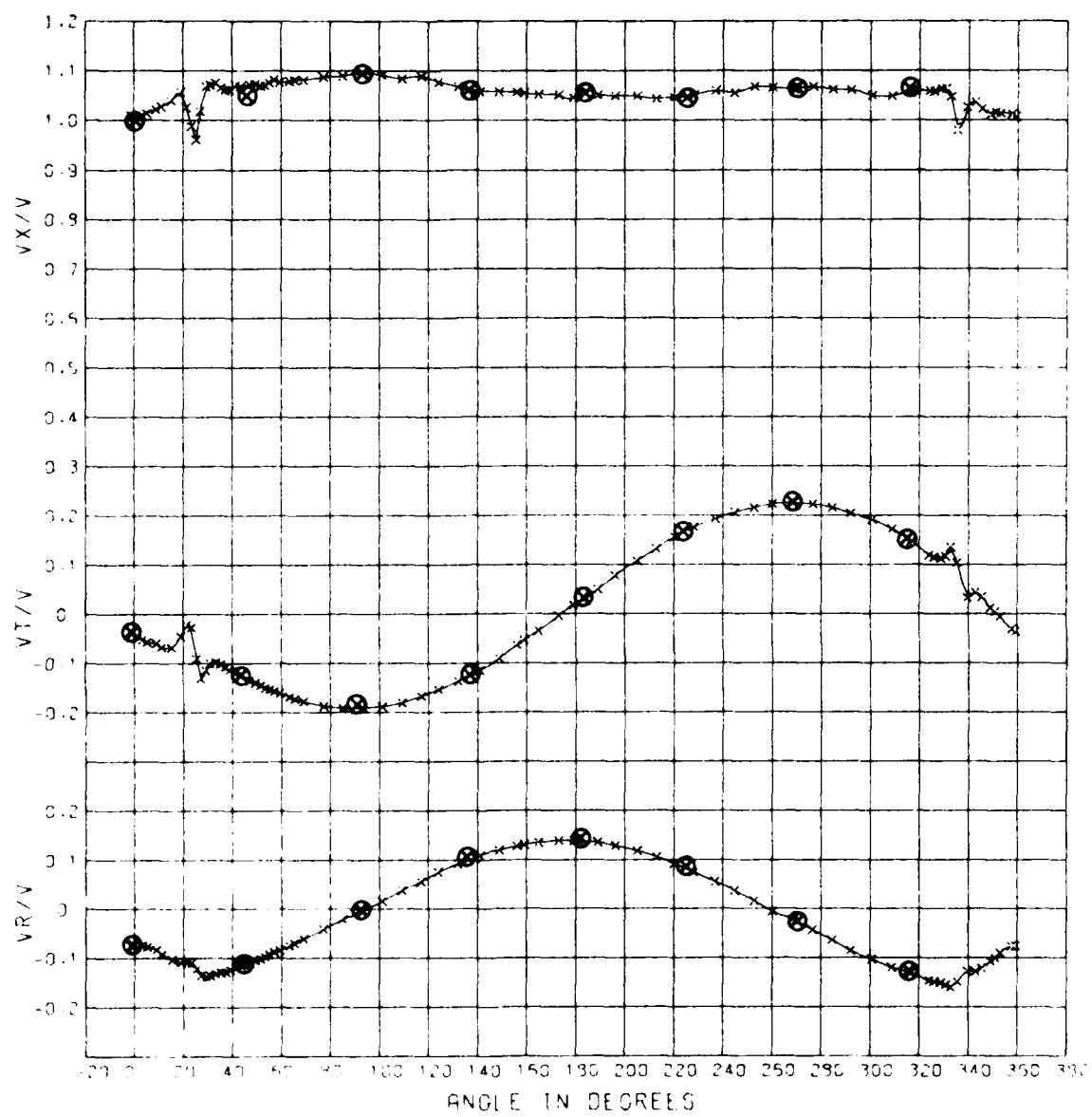
APPENDIX A
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENTS 3 AND 9



VELOCITY COMPONENT RATIOS FOR MODEL S365 CORRELATION WITH R/V ATHENA 3
 0.456 RAD.

Figure A-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiments 3 and 9

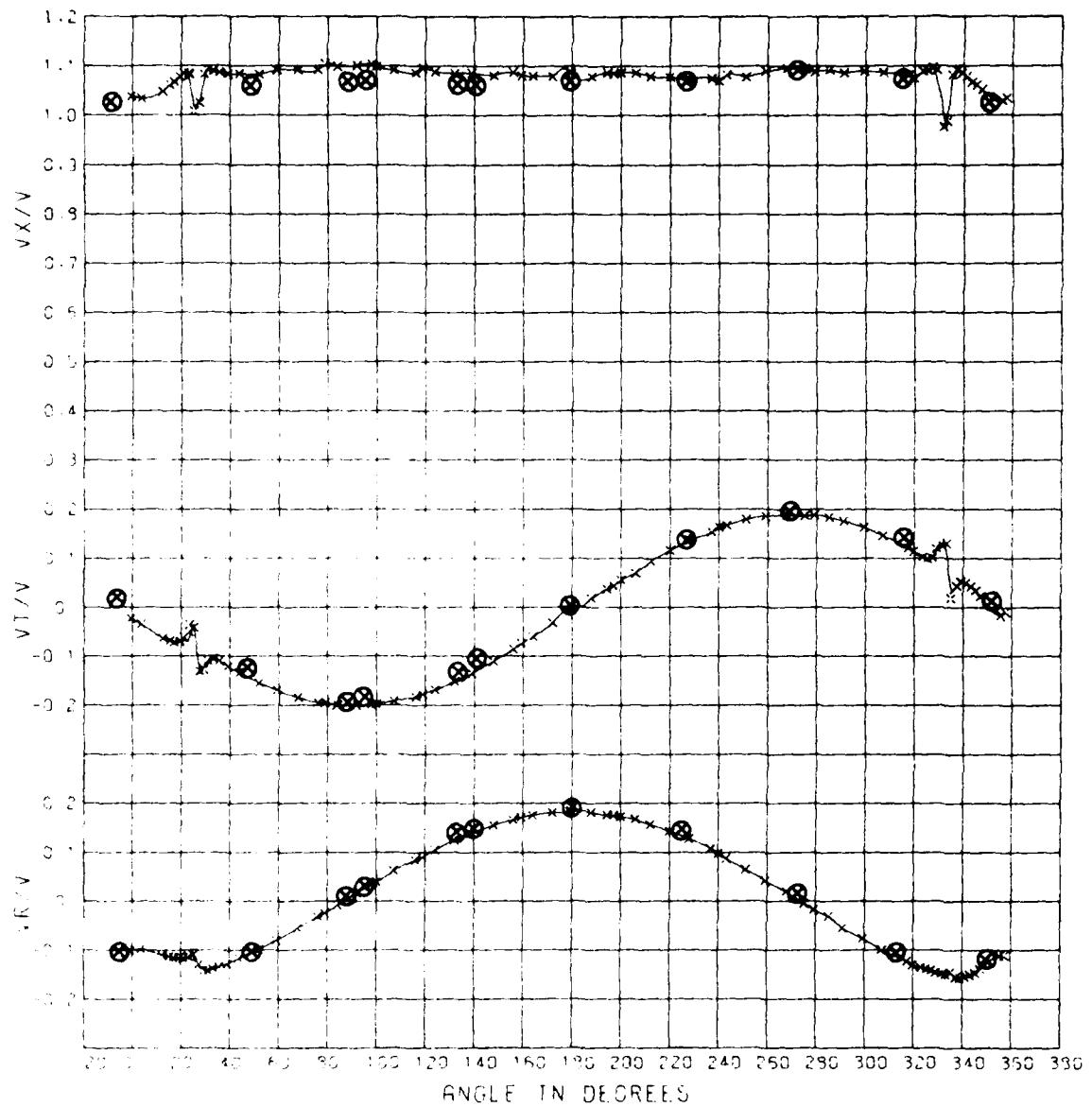
\times : Experiment 3
 \circledast : Experiment 9



VELOCITY COMPONENT RATIOS FOR MODEL 5365 CORRELATION WITH R/V ATHENA 3
0.633 RAD.

Figure A-2 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.633
for Experiments 3 and 9

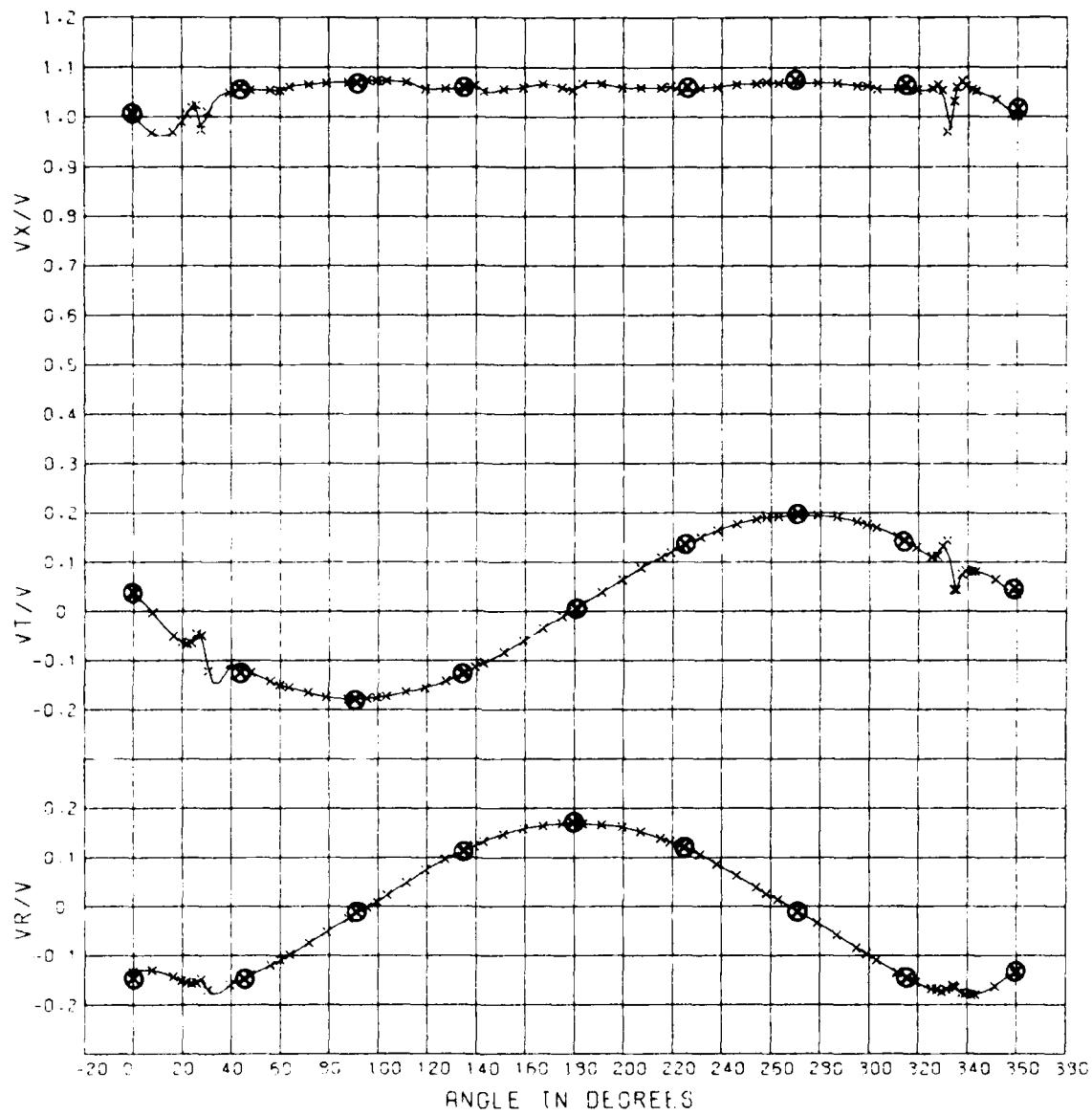
- \times : Experiment 3
- \bullet : Experiment 9



VELOCITY COMPONENT RATIOS FOR MODEL 5365 CORRELATION WITH R/V ATHENA 3
0.781 RAD.

Figure A-3 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.781
for Experiments 3 and 9

x : Experiment 3
⊗ : Experiment 9



VELOCITY COMPONENT RATIOS FOR MODEL 5365 CORRELATION WITH R/V ATHENA 3
0.963 RAD.

Figure A-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiments 3 and 9

x : Experiment 3
 ● : Experiment 9

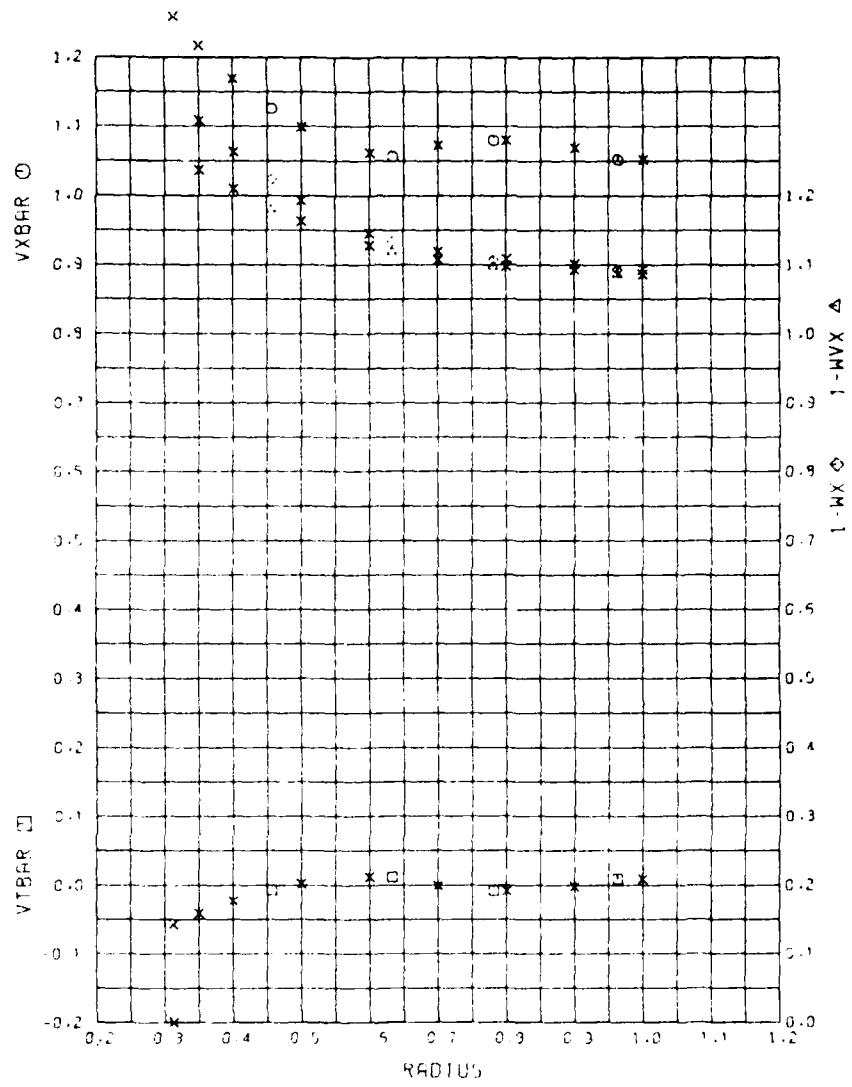


Figure A-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 3

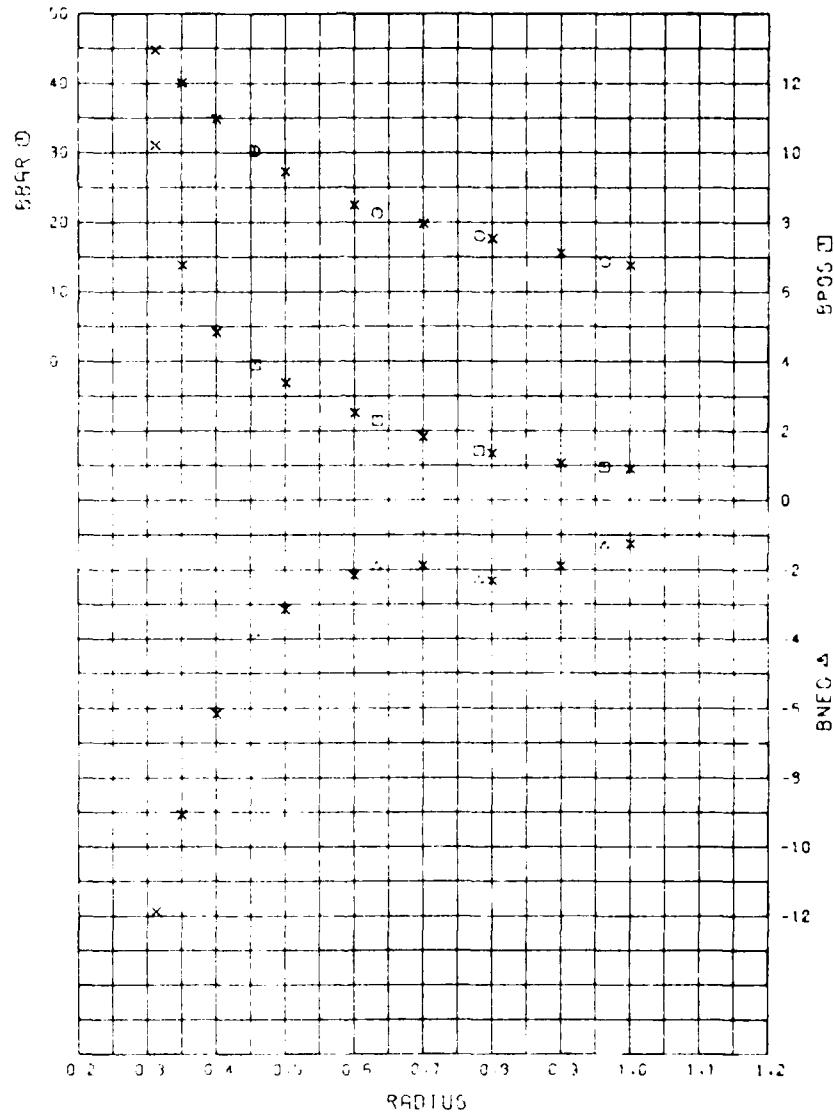


Figure A-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 3

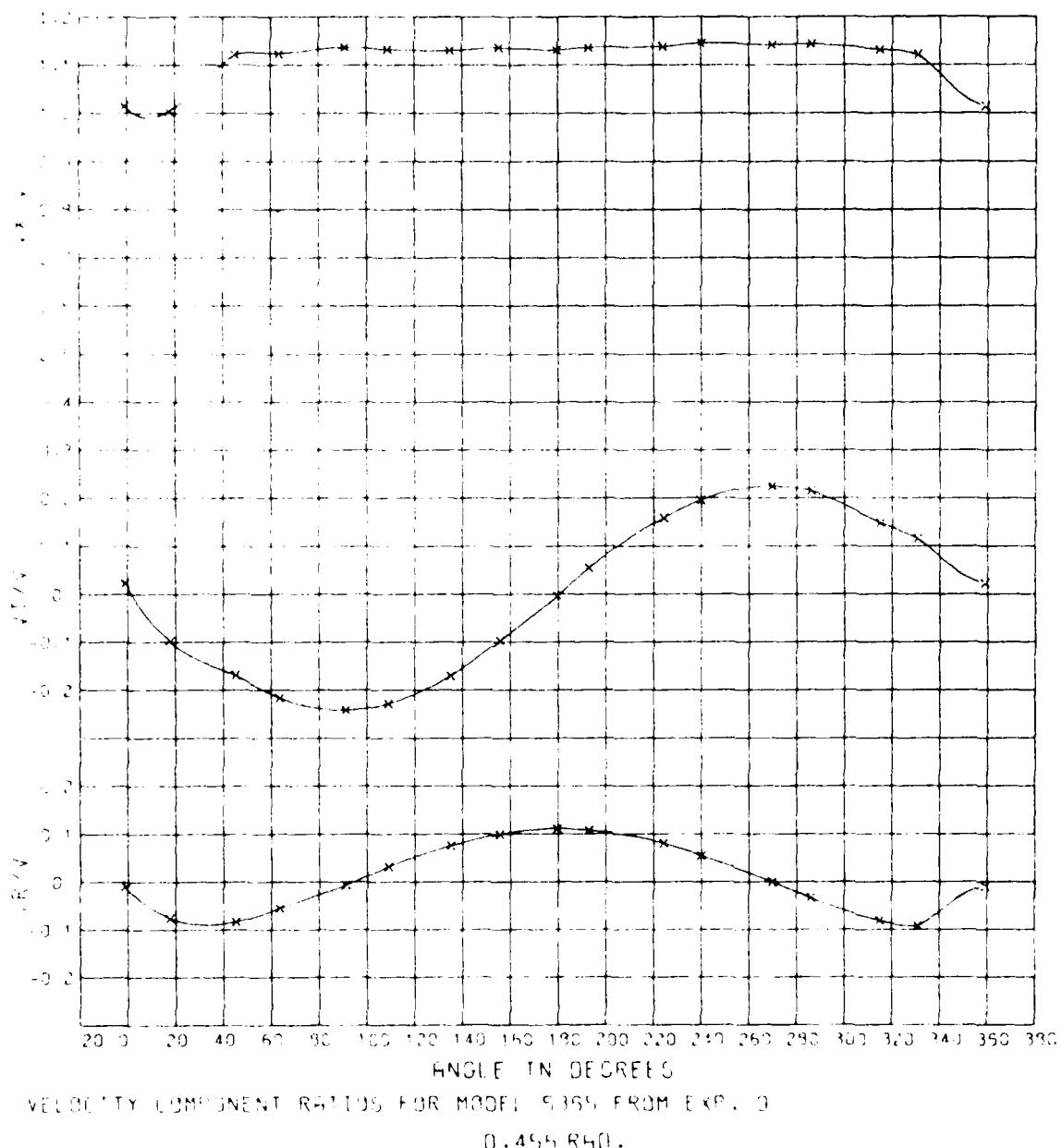
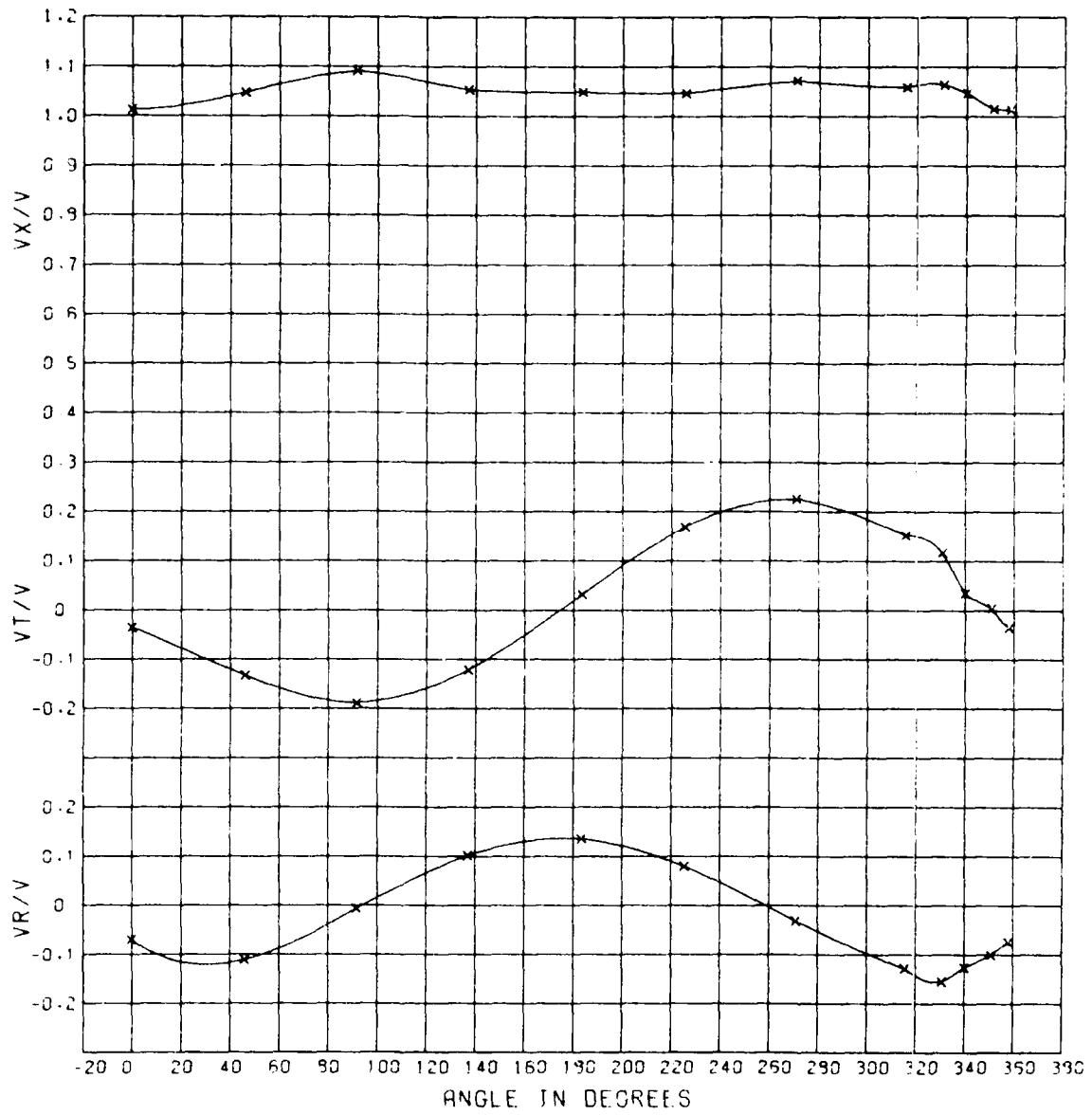


Figure A-7 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 9



VELOCITY COMPONENT RATIOS FOR MODEL 5365 FROM EXP. 9
0.633 RAD.

Figure A-8 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 9

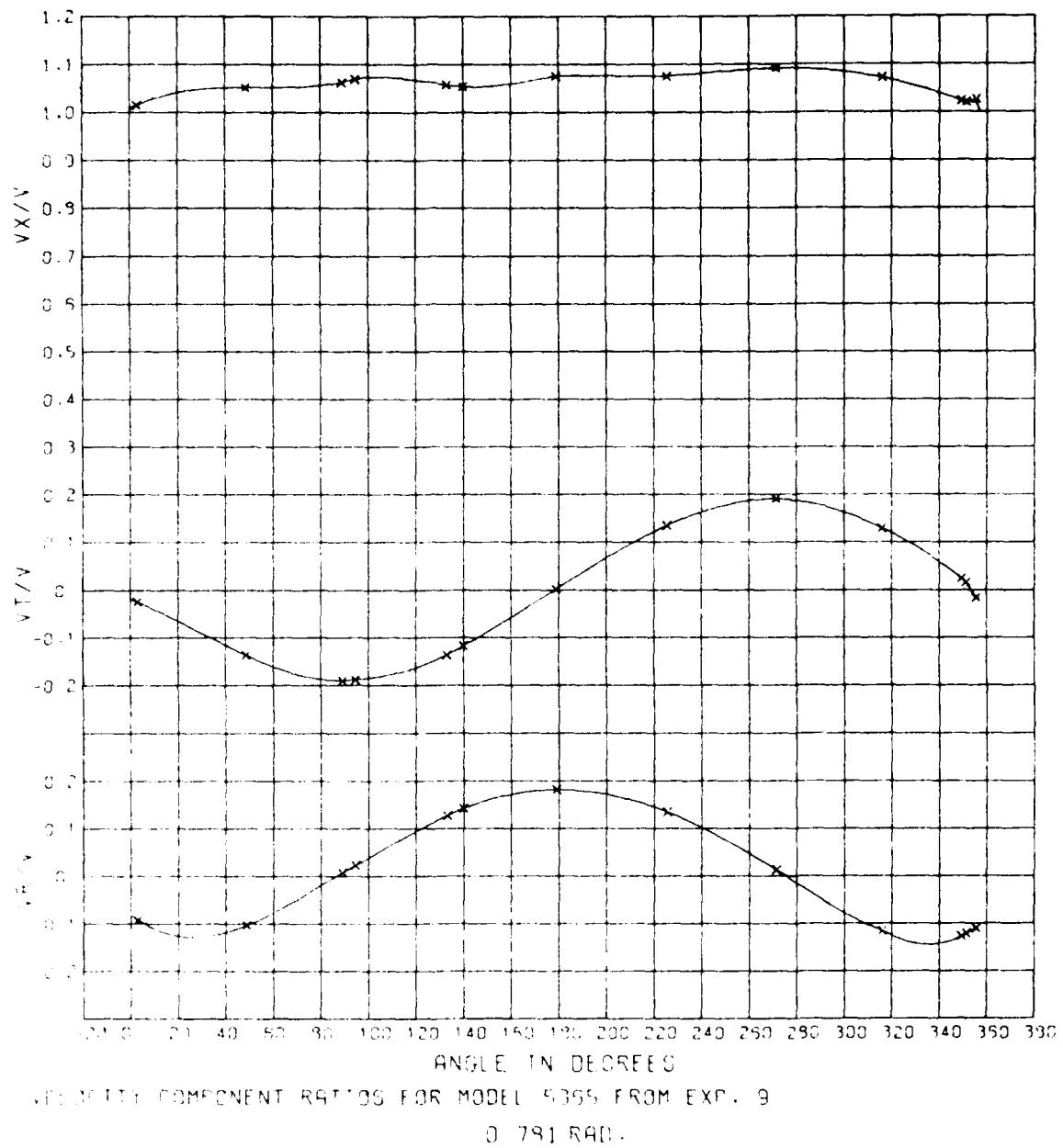


Figure A-9 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 9

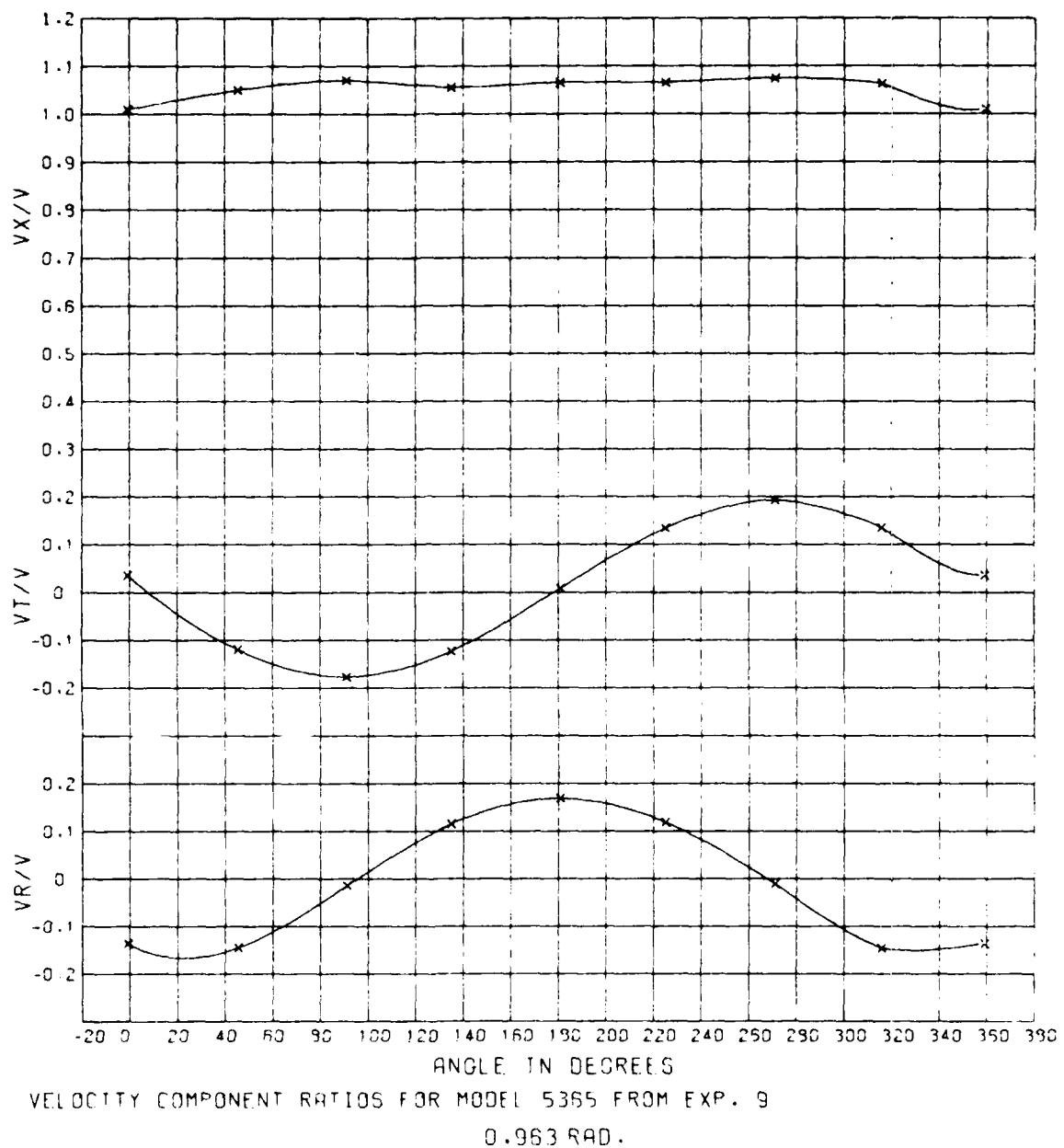


Figure A-10 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 9

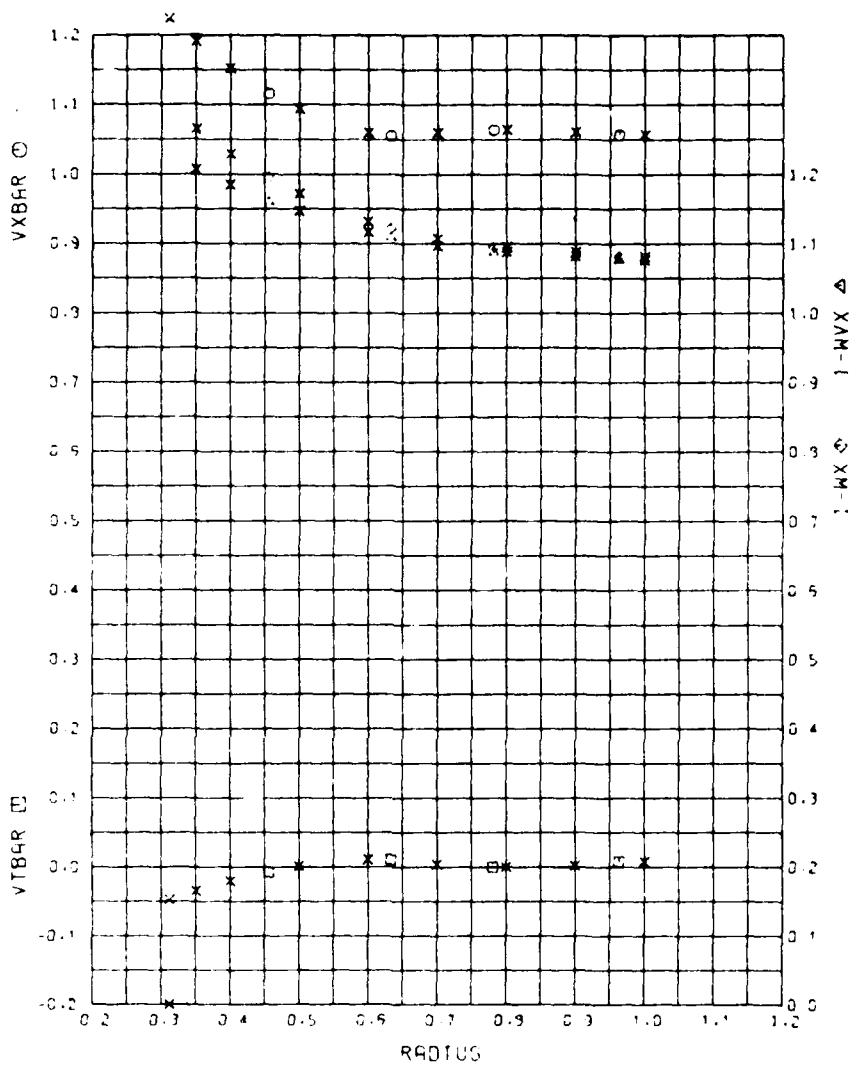


Figure A-11 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 9

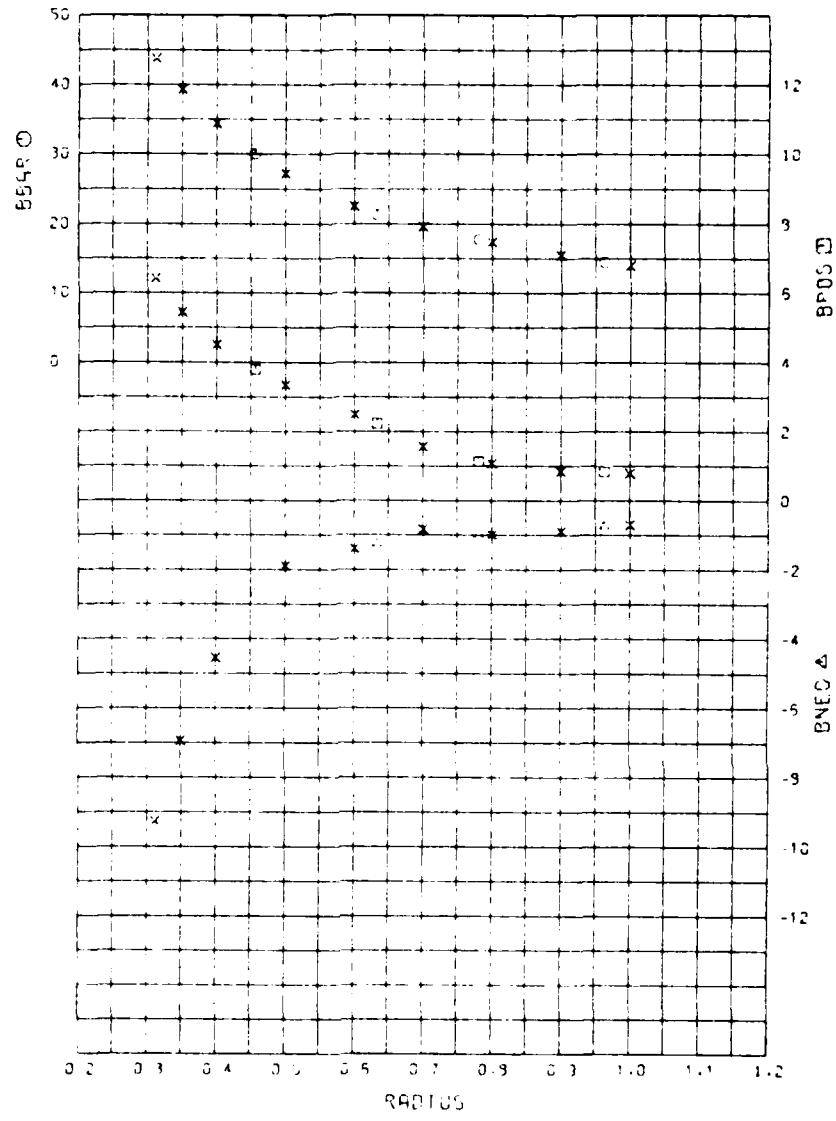


Figure A-12 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 9

TABLE A-1

INPUT DATA FOR HARMONIC ANALYSIS FOR R/V ATHENA,
MODEL 5365, EXPERIMENT 3

ANGLE Y	RADIUS X	V/V									
-1.2	.999	.997	-1.0	.999	.995	-0.8	.999	.993	-0.6	.999	.991
-1.1	.999	.996	-0.9	.999	.994	-0.7	.999	.992	-0.5	.999	.990
-1.0	.999	.995	-0.8	.999	.993	-0.6	.999	.991	-0.4	.999	.989
-0.9	.999	.994	-0.7	.999	.992	-0.5	.999	.990	-0.3	.999	.988
-0.8	.999	.993	-0.6	.999	.991	-0.4	.999	.989	-0.2	.999	.987
-0.7	.999	.992	-0.5	.999	.990	-0.3	.999	.988	-0.1	.999	.986
-0.6	.999	.991	-0.4	.999	.989	0.0	.999	.987	0.2	.999	.985
-0.5	.999	.990	-0.3	.999	.988	0.4	.999	.986	0.6	.999	.984
-0.4	.999	.989	-0.2	.999	.987	0.8	.999	.985	0.9	.999	.983
-0.3	.999	.988	-0.1	.999	.986	1.0	.999	.984	1.1	.999	.982
-0.2	.999	.987	0.0	.999	.985	1.2	.999	.983	1.3	.999	.981
-0.1	.999	.986	0.2	.999	.984	1.4	.999	.982	1.5	.999	.979
0.0	.999	.985	0.4	.999	.983	1.6	.999	.981	1.7	.999	.977
0.1	.999	.984	0.6	.999	.982	1.8	.999	.980	1.9	.999	.975
0.2	.999	.983	0.8	.999	.981	2.0	.999	.979	2.1	.999	.973
0.3	.999	.982	1.0	.999	.980	2.2	.999	.978	2.3	.999	.969
0.4	.999	.981	1.2	.999	.979	2.4	.999	.976	2.5	.999	.960
0.5	.999	.980	1.4	.999	.978	2.6	.999	.974	2.7	.999	.951
0.6	.999	.979	1.6	.999	.977	2.8	.999	.972	2.9	.999	.933
0.7	.999	.978	1.8	.999	.976	3.0	.999	.970	3.1	.999	.914
0.8	.999	.977	2.0	.999	.975	3.2	.999	.968	3.3	.999	.895
0.9	.999	.976	2.2	.999	.974	3.4	.999	.966	3.5	.999	.876
1.0	.999	.975	2.4	.999	.973	3.6	.999	.964	3.7	.999	.857
1.1	.999	.974	2.6	.999	.972	3.8	.999	.962	3.9	.999	.838
1.2	.999	.973	2.8	.999	.971	4.0	.999	.960	4.1	.999	.819
1.3	.999	.972	3.0	.999	.970	4.2	.999	.958	4.3	.999	.799
1.4	.999	.971	3.2	.999	.969	4.4	.999	.956	4.5	.999	.779
1.5	.999	.970	3.4	.999	.968	4.6	.999	.954	4.7	.999	.759
1.6	.999	.969	3.6	.999	.967	4.8	.999	.952	4.9	.999	.739
1.7	.999	.968	3.8	.999	.966	5.0	.999	.950	5.1	.999	.719
1.8	.999	.967	4.0	.999	.965	5.2	.999	.948	5.3	.999	.699
1.9	.999	.966	4.2	.999	.964	5.4	.999	.946	5.5	.999	.679
2.0	.999	.965	4.4	.999	.963	5.6	.999	.944	5.7	.999	.659
2.1	.999	.964	4.6	.999	.962	5.8	.999	.942	5.9	.999	.639
2.2	.999	.963	4.8	.999	.961	6.0	.999	.940	6.1	.999	.619
2.3	.999	.962	5.0	.999	.960	6.2	.999	.938	6.3	.999	.599
2.4	.999	.961	5.2	.999	.959	6.4	.999	.936	6.5	.999	.579
2.5	.999	.960	5.4	.999	.958	6.6	.999	.934	6.7	.999	.559
2.6	.999	.959	5.6	.999	.957	6.8	.999	.932	6.9	.999	.539
2.7	.999	.958	5.8	.999	.956	7.0	.999	.930	7.1	.999	.519
2.8	.999	.957	6.0	.999	.955	7.2	.999	.928	7.3	.999	.499
2.9	.999	.956	6.2	.999	.954	7.4	.999	.926	7.5	.999	.479
3.0	.999	.955	6.4	.999	.953	7.6	.999	.924	7.7	.999	.459
3.1	.999	.954	6.6	.999	.952	7.8	.999	.922	7.9	.999	.439
3.2	.999	.953	6.8	.999	.951	8.0	.999	.920	8.1	.999	.419
3.3	.999	.952	7.0	.999	.950	8.2	.999	.918	8.3	.999	.399
3.4	.999	.951	7.2	.999	.949	8.4	.999	.916	8.5	.999	.379
3.5	.999	.950	7.4	.999	.948	8.6	.999	.914	8.7	.999	.359
3.6	.999	.949	7.6	.999	.947	8.8	.999	.912	8.9	.999	.339
3.7	.999	.948	7.8	.999	.946	9.0	.999	.910	9.1	.999	.319
3.8	.999	.947	8.0	.999	.945	9.2	.999	.908	9.3	.999	.299
3.9	.999	.946	8.2	.999	.944	9.4	.999	.906	9.5	.999	.279
4.0	.999	.945	8.4	.999	.943	9.6	.999	.904	9.7	.999	.259
4.1	.999	.944	8.6	.999	.942	9.8	.999	.902	9.9	.999	.239
4.2	.999	.943	8.8	.999	.941	10.0	.999	.900	10.1	.999	.219
4.3	.999	.942	9.0	.999	.940	10.2	.999	.898	10.3	.999	.199
4.4	.999	.941	9.2	.999	.939	10.4	.999	.896	10.5	.999	.179
4.5	.999	.940	9.4	.999	.938	10.6	.999	.894	10.7	.999	.159
4.6	.999	.939	9.6	.999	.937	10.8	.999	.892	10.9	.999	.139
4.7	.999	.938	9.8	.999	.936	11.0	.999	.890	11.1	.999	.119
4.8	.999	.937	10.0	.999	.935	11.2	.999	.888	11.3	.999	.099
4.9	.999	.936	10.2	.999	.934	11.4	.999	.886	11.5	.999	.079
5.0	.999	.935	10.4	.999	.933	11.6	.999	.884	11.7	.999	.059
5.1	.999	.934	10.6	.999	.932	11.8	.999	.882	11.9	.999	.039
5.2	.999	.933	10.8	.999	.931	12.0	.999	.880	12.1	.999	.019
5.3	.999	.932	11.0	.999	.930	12.2	.999	.878	12.3	.999	.000
5.4	.999	.931	11.2	.999	.929	12.4	.999	.876	12.5	.999	.180
5.5	.999	.930	11.4	.999	.928	12.6	.999	.874	12.7	.999	.360
5.6	.999	.929	11.6	.999	.927	12.8	.999	.872	12.9	.999	.540
5.7	.999	.928	11.8	.999	.926	13.0	.999	.870	13.1	.999	.720
5.8	.999	.927	12.0	.999	.925	13.2	.999	.868	13.3	.999	.900
5.9	.999	.926	12.2	.999	.924	13.4	.999	.866	13.5	.999	.080
6.0	.999	.925	12.4	.999	.923	13.6	.999	.864	13.7	.999	.260
6.1	.999	.924	12.6	.999	.922	13.8	.999	.862	13.9	.999	.440
6.2	.999	.923	12.8	.999	.921	14.0	.999	.860	14.1	.999	.620
6.3	.999	.922	13.0	.999	.920	14.2	.999	.858	14.3	.999	.800
6.4	.999	.921	13.2	.999	.919	14.4	.999	.856	14.5	.999	.980
6.5	.999	.920	13.4	.999	.918	14.6	.999	.854	14.7	.999	.160
6.6	.999	.919	13.6	.999	.917	14.8	.999	.852	14.9	.999	.340
6.7	.999	.918	13.8	.999	.916	15.0	.999	.850	15.1	.999	.520
6.8	.999	.917	14.0	.999	.915	15.2	.999	.848	15.3	.999	.700
6.9	.999	.916	14.2	.999	.914	15.4	.999	.846	15.5	.999	.880
7.0	.999	.915	14.4	.999	.913	15.6	.999	.844	15.7	.999	.060
7.1	.999	.914	14.6	.999	.912	15.8	.999	.842	15.9	.999	.240
7.2	.999	.913	14.8	.999	.911	16.0	.999	.840	16.1	.999	.420
7.3	.999	.912	15.0	.999	.910	16.2	.999	.838	16.3	.999	.600
7.4	.999	.911	15.2	.999	.909	16.4	.999	.836	16.5	.999	.780
7.5	.999	.910	15.4	.999	.908	16.6	.999	.834	16.7	.999	.960
7.6	.999	.909	15.6	.999	.907	16.8	.999	.832	16.9	.999	.140
7.7	.999	.908	15.8	.999	.906	17.0	.999	.830	17.1	.999	.320
7.8	.999	.907	16.0	.999	.905	17.2	.999	.828	17.3	.999	.500
7.9	.999	.906	16.2	.999	.904	17.4	.999	.826	17.5	.999	.680
8.0	.999	.905	16.4	.999	.903	17.6	.999	.824	17.7	.999	.860
8.1	.999	.904	16.6	.999	.902	17.8	.999	.822	17.9	.999	.040
8.2	.999	.903	16.8	.999	.901	18.0	.999	.820	18.1	.999	.220
8.3	.999	.902	17.0	.999	.900	18.2	.999	.818	18.3	.999	.400
8.4	.999	.901	17.2	.999	.899	18.4	.999	.816	18.5	.999	.580
8.5	.999	.900	17.4	.999	.898	18.6	.999	.814	18.7	.999	.760
8.6	.999	.899	17.6	.999	.897	18.8	.999	.812	18.9	.999	.940
8.7	.999	.898	17.8	.999	.896	19.0	.999	.810	19.1	.999	.120
8.8	.999	.897	18.0	.999	.895	19.2	.999	.808	19.3	.999	.300
8.9	.999	.896	18.2	.999	.894	19.4	.999	.806	19.5	.999	.480
9.0	.999	.895	18.4	.999	.893	19.6	.999	.804	19.7	.999	.660
9.1	.999	.894	18.6	.999	.892	19.8	.999	.802	19.9	.999	.840
9.2	.999	.893	18.8	.999	.891	20.0	.999	.800	20.1	.999	.020
9.3	.999	.892	19.0	.999	.890	20.2	.999	.798	20.3	.999	.200
9.4	.9										

TABLE A-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 3

VELOCITY COMPONENT RATIOS FOR MODEL 5305 CORRELATION WITH R/V ATHENA 3
(ROPELLER DIAMETER 6.00 FEET
JA = .739)

RADIUS :	.456	.613	.781	.963	.312	.350	.402	.450	.500	.550	.600	.650	.700	.800	.900	1.000
V _{MAX} :	1.126	1.07	1.030	1.052	1.253	1.217	1.169	1.133	1.062	1.073	1.080	1.069	1.069	1.052		
J ² A :	- .007	.512	-.008	.009	- .057	- .041	- .023	.002	.012	- .001	- .008	- .002	- .009			
V _{MIN} :	- .003	- .008	.015	- .008	.056	.041	.023	- .000	- .009	.007	.015	.006	- .008			
I-W ₄ :	- 1.180	1.119	1.097	1.086	0.600	1.237	1.216	1.183	1.128	1.107	1.098	1.093	1.086			
I-W ₆ :	- 1.224	1.135	1.107	1.093	0.900	1.368	1.253	1.168	1.146	1.119	1.108	1.101	1.093			
B _{MAX} :	36.23	21.26	18.05	14.38	44.74	40.05	34.87	28.44	22.51	19.82	17.65	15.61	13.87			
B ₂₀ :	3.91	2.29	1.42	.95	10.21	6.77	4.53	3.32	2.52	1.82	1.35	1.06	.90			
THETA :	90.00	92.50	95.00	95.00	22.50	22.50	85.00	9.50	92.50	95.00	95.00	95.00	95.00			
LNEG :	- 1.83	- 1.91	- 2.31	- 1.31	- 11.67	- 9.67	- 6.17	- 4.1	- 2.17	- 1.88	- 2.32	- 1.90	- 1.26			
THETA :	0.00	335.00	332.50	0.00	0.00	33.40	335.00	332.50	332.50	332.50	332.50	332.50	332.50			

45

UXBAR IS MEAN LONGITUDINAL VELOCITY.
 VTBAR IS CIRCUMFERENTIAL MEAN TANGENTIAL VELOCITY.
 VTBAR IS ARCWISE MEAN RADIAL VELOCITY.
 I-W₄ IS VOLUMETRIC MEAN WAKE VELOCITY WITHOUT TANGENTIAL CORRECTION.
 I-W₆ IS VOLUMETRIC MEAN WAKE VELOCITY WITH TANGENTIAL CORRECTION.
 BBAR IS MEAN ANGLE OF ADVANCE.
 BFO₀ IS VARIATION BETWEEN THE MAXIMUM AND MEAN ADVANCE ANGLES.
 d_{MEG} IS VARIATION BETWEEN THE MINIMUM AND MEAN ADVANCE ANGLES.
 THETA IS ANGLE IN DEGREES AT WHICH CORRESPONDING BPOS OR BNUG OCCUR.

TABLE A-3 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL
RADII FOR EXPERIMENT 3

VELOCITY COMPONENT RATIOS FOR MODEL SIZES CORRELATION WITH Q/V ANTENA 3 PROPELLER DIAMETER 6.00 FEET JA = .734									
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .456									
AMPLITUDE =	.0367	.0358	.0244	.0192	.0143	.0099	.0050	.0026	
PHASE ANGLE =	204.2	273.4	271.3	267.3	269.3	263.6	244.1	195.5	
RADIUS = .633									
AMPLITUDE =	.0150	.0224	.0098	.0052	.0034	.0013	.0010	.0027	
PHASE ANGLE =	323.3	268.9	215.5	211.1	212.2	222.6	13.3	31.2	
RADIUS = .781									
AMPLITUDE =	.0103	.0147	.0133	.0025	.0024	.0040	.0007	.0012	
PHASE ANGLE =	209.9	254.1	218.3	358.2	253.3	278.6	205.2	183.8	
RADIUS = .963									
AMPLITUDE =	.0187	.0193	.0152	.0067	.0063	.0070	.0058	.0038	
PHASE ANGLE =	261.6	254.1	234.9	191.4	213.7	193.4	175.5	174.1	
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .456									
AMPLITUDE =	.0041	.0058	.0018	.0057	.0054	.0030	.0069	.0019	
PHASE ANGLE =	130.7	130.5	116.4	124.6	126.8	154.0	179.1	296.1	
RADIUS = .633									
AMPLITUDE =	.0034	.0021	.0012	.0028	.0033	.0032	.0031	.0034	
PHASE ANGLE =	73.2	40.2	118.1	248.0	279.1	261.3	212.6	271.8	
RADIUS = .781									
AMPLITUDE =	.0007	.0027	.0019	.0016	.0043	.0027	.0029	.0003	
PHASE ANGLE =	217.1	254.2	235.2	213.3	296.3	274.4	319.3	240.7	
RADIUS = .963									
AMPLITUDE =	.0027	.0026	.0012	.0026	.0020	.0017	.0010	.0014	
PHASE ANGLE =	165.9	169.4	170.8	260.4	205.3	298.0	133.4	43.5	

TABLE A-4 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 3

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	1	2	3	4	5	6	7	8	
RADIUS = .312									
AMPLITUDE = .0160	.0499	.0145	.0142	.0218	.0155	.0131			
PHASE ANGLE = 215.6	275.9	214.9	214.6	272.6	262.5	215.2	201.9		
RADIUS = .350									
AMPLITUDE = .0730	.0459	.0141	.0176	.0224	.0123	.0122	.0134		
PHASE ANGLE = 216.7	275.3	214.1	214.0	271.4	262.6	216.5	201.4		
RADIUS = .400									
AMPLITUDE = .0537	.0409	.0143	.0261	.0193	.0153	.0095	.0063		
PHASE ANGLE = 254.3	274.5	213.6	213.3	270.5	262.9	239.1	200.1		
RADIUS = .500									
AMPLITUDE = .0269	.0320	.0172	.0136	.0110	.0065	.0029	.0035		
PHASE ANGLE = 216.0	272.4	213.5	213.4	264.0	254.9	252.4	151.0		
RADIUS = .600									
AMPLITUDE = .0167	.0246	.00842	.00749	.0018	.0019	.0009	.0025		
PHASE ANGLE = 313.7	269.9	213.7	213.2	263.4	277.8	346.3	31.6		
RADIUS = .700									
AMPLITUDE = .0116	.0177	.00040	.00276	.00339	.00332	.0006	.0008		
PHASE ANGLE = 312.2	267.7	211.3	211.6	268.6	291.2	348.1	41.7		
RADIUS = .800									
AMPLITUDE = .0106	.0144	.0045	.0023	.0029	.0040	.0010	.0015		
PHASE ANGLE = 214.5	262.9	216.6	303.6	251.8	272.5	195.9	185.4		
RADIUS = .900									
AMPLITUDE = .0145	.0159	.0112	.0029	.0051	.0046	.0036	.0033		
PHASE ANGLE = 205.7	256.7	234.5	213.3	220.8	223.6	179.6	180.9		
RADIUS = 1.000									
AMPLITUDE = .0167	.0193	.0142	.0070	.0083	.0070	.0059	.0038		
PHASE ANGLE = 211.0	254.1	234.9	211.4	213.7	193.4	175.5	174.1		

TABLE A-4 (Continued)

VELOCITY COMPONENT RATIOS FOR MODEL 3365 CORRELATION WITH R/V ATHENA 3									
PROPELLER DIAMETER = 6.00 FEET JA = .739									
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .312									
AMPLITUDE = .0109		.0157	.0134	.0156	.0185	.0107	.0082	.0044	
PHASE ANGLE = 132.6		159.9	130.7	128.5	116.5	122.3	71.5	65.5	
RADIUS = .350									
AMPLITUDE = .0078		.0125	.0113	.0126	.0145	.0082	.0055	.0026	
PHASE ANGLE = 173.7		154.2	130.7	128.4	117.9	126.0	75.7	73.8	
RADIUS = .400									
AMPLITUDE = .0057		.0069	.0041	.0091	.0098	.0054	.0025	.0012	
PHASE ANGLE = 166.6		145.5	130.7	128.5	120.5	134.1	88.2	.9	
RADIUS = .500									
AMPLITUDE = .0040		.0042	.0052	.0035	.0027	.0020	.0021	.0028	
PHASE ANGLE = 10.0		113.0	121.5	129.8	140.7	188.2	226.7	262.9	
RADIUS = .600									
AMPLITUDE = .0037		.0024	.0021	.0052	.0025	.0028	.0033	.0035	
PHASE ANGLE = 79.3		58.5	137.5	218.2	270.4	254.0	247.3	273.4	
RADIUS = .700									
AMPLITUDE = .0011		.0012	.0009	.0012	.0034	.0030	.0030	.0017	
PHASE ANGLE = 53.6		290.5	266.4	289.2	292.8	267.2	288.6	265.6	
RADIUS = .800									
AMPLITUDE = .00069		.00029	.0020	.0017	.0036	.0026	.0027	.0001	
PHASE ANGLE = 255.3		250.0	284.9	281.3	295.9	276.1	324.1	172.1	
RADIUS = .900									
AMPLITUDE = .0017		.0026	.0014	.0022	.0020	.0021	.0012	.0010	
PHASE ANGLE = 201.1		217.8	214.6	208.9	270.9	287.4	349.4	64.1	
RADIUS = .000									
AMPLITUDE = .0027		.0026	.0012	.0026	.0020	.0017	.0010	.0014	
PHASE ANGLE = 165.9		169.4	146.8	260.4	205.3	298.0	133.4	43.5	

TABLE A-3 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 3

WIGLEY'S COMPONENT RATIOS TO MODEL 5365 CORRELATION WITH R/V ANTENNA 3
PROPELLER DIAMETER 6.00 FEET
UA = .739

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (V1/V)

HARMONIC	1	2	3	4	5	6	7	8
RADIUS = .456								
AMPLITUDE = .2359	.0054	.0027	.0030	.0036	.0034	.0031		
PHASE ANGLE = 160.6	66.7	131.0	150.6	141.6	146.5	106.7		
RADIUS = .633								
AMPLITUDE = .2069	.0088	.0072	.0059	.0047	.0041	.0037	.0026	
PHASE ANGLE = 163.6	289.5	210.4	219.2	279.7	272.4	232.2	282.0	
RADIUS = .781								
AMPLITUDE = .1932	.0037	.0012	.0027	.0031	.0020	.0022	.0013	
PHASE ANGLE = 160.5	283.4	210.2	213.2	279.0	256.9	294.7	312.0	
RADIUS = .963								
AMPLITUDE = .1668	.0031	.0026	.0042	.0044	.0044	.0027	.0012	
PHASE ANGLE = 178.5	154.7	127.2	125.1	106.3	104.2	89.7	62.6	

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (V1/V)

HARMONIC	9	10	11	12	13	14	15	16
RADIUS = .456								
AMPLITUDE = .0050	.0045	.0012	.0051	.0042	.0026	.0012	.0010	
PHASE ANGLE = 62.1	43.5	43.2	43.6	43.0	61.2	60.2	164.8	
RADIUS = .633								
AMPLITUDE = .0625	.0024	.0008	.0008	.0016	.0030	.0030	.0034	
PHASE ANGLE = 247.0	287.0	210.2	211.6	167.1	13.9	163.1	156.5	
RADIUS = .781								
AMPLITUDE = .0019	.0008	.0002	.0003	.0013	.0018	.0014	.0015	
PHASE ANGLE = 330.4	31.0	48.6	17.4.8	135.3	158.7	147.6	168.7	
RADIUS = .963								
AMPLITUDE = .0002	.0008	.0014	.0023	.0025	.0022	.0016	.0014	
PHASE ANGLE = 212.2	210.4	191.3	172.3	153.9	124.6	46.0		

TABLE A-6 - HARMONIC ANALYSIS OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 3

VELOCITY COMPONENT RATIOS FOR MODEL 5305 CORRELATION WITH R/V ATHENA 3 PROPELLER DIAMETER 6.20 FEET JA = .739									
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT.V)									
	1	2	3	4	5	6	7	8	9
RADIUS = .312									
AMPLITUDE =	.2717	.0308	.0212	.0196	.0165	.0161	.0137		
PHASE ANGLE =	174.5	92.2	111.5	114.0	124.1	122.3	108.9	88.8	
RADIUS = .450									
AMPLITUDE =	.2610	.0226	.0154	.0157	.0149	.0124	.0121	.0104	
PHASE ANGLE =	176.3	90.2	112.8	126.2	125.6	124.5	108.7	88.5	
RADIUS = .400									
AMPLITUDE =	.2483	.0134	.0077	.0045	.0077	.0076	.0066		
PHASE ANGLE =	178.5	85.2	115.9	111.5	129.8	129.9	108.2	87.5	
RADIUS = .500									
AMPLITUDE =	.2273	.0027	.0013	.0021	.0020	.0019	.0008	.0010	
PHASE ANGLE =	181.9	254.3	262.7	262.5	177.9	192.1	97.2	69.3	
RADIUS = .600									
AMPLITUDE =	.2117	.0080	.0046	.0051	.0040	.0037	.0031	.0021	
PHASE ANGLE =	163.6	292.5	275.6	276.5	275.2	268.4	292.6	283.0	
RADIUS = .700									
AMPLITUDE =	.1997	.0065	.0061	.0047	.0047	.0034	.0033	.0020	
PHASE ANGLE =	162.1	289.0	261.0	275.1	279.3	268.0	291.7	292.5	
RADIUS = .800									
AMPLITUDE =	.1920	.0031	.0047	.0023	.0029	.0015	.0019	.0012	
PHASE ANGLE =	160.2	260.6	247.1	256.8	278.3	250.4	296.8	316.9	
RADIUS = .900									
AMPLITUDE =	.1378	.0014	.0002	.0019	.0010	.0019	.0008	.0008	
PHASE ANGLE =	178.3	191.9	260.3	178.6	117.2	117.5	60.7	24.0	
RADIUS = 1.000									
AMPLITUDE =	.1868	.0031	.0026	.0040	.0044	.0044	.0027	.0012	
PHASE ANGLE =	175.5	154.7	127.2	125.1	106.3	104.2	89.7	62.6	

TABLE A-6 (Continued)

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
VELOCITY COMPONENT RATIOS FOR MODEL 5365 CORRELATION WITH R.V. ATHENA 3 PROPELLER DIAMETER = 5.00 FEET JA = .739									
RADIUS = .312	9	10	11	12	13	14	15	16	
AMPLITUDE = .0163	.0162	.0160	.0154	.0136	.0096	.0074	.0047		
PHASE ANGLE = 73.7	62.7	55.3	49.3	33.5	30.8	6.5	328.1		
RADIUS = .350									
AMPLITUDE = .0132	.0124	.0143	.0122	.0107	.0073	.0057	.0029		
PHASE ANGLE = 72.4	60.4	49.7	49.3	34.6	35.0	11.6	326.4		
RADIUS = .400									
AMPLITUDE = .0069	.0082	.0101	.0095	.0073	.0047	.0031	.0009		
PHASE ANGLE = 19.5	55.4	48.5	49.3	37.1	44.6	20.3	315.5		
RADIUS = .500									
AMPLITUDE = .0027	.0025	.0037	.0030	.0024	.0020	.0013	.0009		
PHASE ANGLE = 46.4	20.5	62.5	60.4	54.5	106.1	129.8	152.0		
RADIUS = .600									
AMPLITUDE = .0020	.0022	.0005	.0001	.0028	.0024	.0033			
PHASE ANGLE = 306.2	295.7	323.2	184.6	153.7	158.7	161.4	156.2		
RADIUS = .700									
AMPLITUDE = .0022	.0011	.0003	.0004	.0013	.0023	.0021	.0025		
PHASE ANGLE = 314.3	321.7	324.7	154.9	146.1	162.1	159.0	164.1		
RADIUS = .800									
AMPLITUDE = .0018	.0009	.0002	.0006	.0013	.0018	.0013	.0013		
PHASE ANGLE = 333.5	10.8	65.7	135.2	136.4	157.8	144.2	168.0		
RADIUS = .900									
AMPLITUDE = .0010	.0004	.0006	.0013	.0017	.0019	.0013	.0005		
PHASE ANGLE = 346.4	94.4	160.3	176.1	157.3	154.4	127.1	84.8		
RADIUS = 1.000									
AMPLITUDE = .0002	.0008	.0014	.0023	.0025	.0022	.0016	.0014		
PHASE ANGLE = 211.6	212.2	206.4	191.5	172.3	153.9	124.0	46.0		

TABLE A-7

INPUT DATA FOR HARMONIC ANALYSIS FOR R/V ATHENA,
MODEL 5365, EXPERIMENT 9

INPUT DATA

	RADIUS = .456		RADIUS = .781					
ANGLE	VX/V	VT/V	VR/V	ANGLE	VX/V	VT/V	VR/V	
-1.0	1.014	.023	-.010	2.9	1.015	-.025	-.092	
17.6	1.003	~.098	-.076	48.7	1.052	~.137	~.104	
45.2	1.122	~.168	-.084	89.1	1.063	~.190	.007	
63.6	1.121	~.217	-.053	94.6	1.070	~.188	.023	
63.6	1.124	~.216	-.058	133.2	1.058	~.136	.127	
91.1	1.137	~.241	-.007	140.0	1.054	~.117	.142	
109.0	1.132	~.228	.031	174.0	1.075	.002	.182	
135.0	1.129	~.170	.076	179.0	1.076	.002	.182	
155.6	1.136	~.097	.099	225.5	1.075	.134	.135	
179.7	1.131	~.003	.111	271.4	1.092	.191	.013	
193.0	1.136	.055	.108	316.0	1.072	.128	-.116	
224.2	1.138	.159	.081	349.3	1.024	.025	~.127	
240.0	1.145	.196	.055	351.3	1.020	.016	~.121	
269.6	1.137	.225	.002	355.6	1.027	~.017	~.111	
269.7	1.145	.224	~.002	362.9	1.015	~.025	~.092	
286.1	1.143	.215	~.034					
315.0	1.131	.148	~.081					
331.0	1.121	.116	~.093					
359.0	1.014	.023	~.010	ANGLE	VX/V	VT/V	VR/V	
361.0	1.014	.023	~.010		-.5	1.011	.036	
					-1.0	1.009	.036	
	RADIUS = .633				45.5	1.050	~.120	~.145
ANGLE	VX/V	VT/V	VR/V		91.2	1.071	~.177	~.014
~.3	1.013	~.035	~.070		136.1	1.056	~.124	.115
46.0	1.048	~.133	~.111		180.9	1.066	.009	.169
91.7	1.091	~.189	~.007		225.1	1.066	.133	.118
137.0	1.053	~.122	.102		271.0	1.074	.193	~.011
137.0	1.056	~.121	.101		316.0	1.063	.135	~.146
183.4	1.049	.032	.136		359.0	1.009	.036	~.137
225.5	1.047	.168	.080		359.5	1.011	.036	~.135
274.0	1.071	.225	~.032		360.5	1.011	.036	~.135
315.7	1.058	.152	~.129					
330.8	1.064	.117	~.155					
340.0	1.017	.035	~.126					
351.0	1.016	.005	~.101					
358.0	1.014	~.035	~.074					
359.7	1.013	~.035	~.070					

TABLE A-8 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 9

VELOCITY COMPONENT RATIOS FOR MODEL 5365 FROM EXP. 9
PROPELLER DIAMETER = 6.00 FEET

RADIUS	.456	.633	.781	.963	.312	.350	.400	.500	.600	.700	.800	.900	1.000
VXBAR	1.116	1.055	1.064	1.057	1.224	1.191	1.152	1.094	1.060	1.060	1.064	1.061	1.057
VTBAR	- .007	.011	- .000	.008	- .047	- .034	- .020	.001	.011	.004	- .000	.002	.008
VRBAR	.006	- .009	.016	- .008	.054	.038	.021	- .002	- .010	.007	.016	.007	- .008
1-WVX	1.160	1.109	1.088	1.077	0.000	1.207	1.185	1.147	1.117	1.097	1.088	1.082	1.077
1-WX	1.196	1.122	1.095	1.082	0.000	1.265	1.229	1.172	1.132	1.107	1.095	1.088	1.082
BBAR	30.01	21.31	17.76	14.44	43.73	39.31	34.42	27.20	22.48	19.58	17.37	15.49	13.93
BPOS	3.79	2.23	1.13	.84	6.42	5.44	4.50	3.34	2.49	1.57	1.07	.84	.79
THETA	90.00	92.50	102.50	90.00	105.00	102.50	95.00	90.00	92.50	97.50	102.50	100.00	90.00
ENEG	-2.69	-1.26	- .98	- .74	-9.28	-6.94	-4.55	-1.89	-1.40	- .84	- .99	- .90	- .71
THETA	0.00	242.50	357.50	352.50	357.50	357.50	357.50	267.50	247.50	245.00	357.50	357.50	352.50

VXBAR IS CIRCUMFERENTIAL MEAN LONGITUDINAL VELOCITY.
 VTBAR IS CIRCUMFERENTIAL MEAN TANGENTIAL VELOCITY.
 VRBAR IS CIRCUMFERENTIAL MEAN RADIAL VELOCITY.
 1-WVX IS VOLUMETRIC MEAN WAKE VELOCITY WITHOUT TANGENTIAL CORRECTION.
 1-WX IS VOLUMETRIC MEAN WAKE VELOCITY WITH TANGENTIAL CORRECTION.
 BBAR IS MEAN ANGLE OF ADVANCE.
 BPOS IS VARIATION BETWEEN THE MAXIMUM AND MEAN ADVANCE ANGLES (DELTA BETA PLUS).
 BNNEG IS VARIATION BETWEEN THE MINIMUM AND MEAN ADVANCE ANGLES (DELTA BETA MINUS).
 THETA IS ANGLE IN DEGREES AT WHICH CORRESPONDING BPOS OR BNNEG OCCURS.

TABLE A-9 - HARMONIC ANALYSIS OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 9

VELOCITY COMPONENT RATIOS FOR MODEL 5365 FROM EXP. 9
PROPELLER DIAMETER = 6.00 FEET

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)							
HARMONIC	#	1	2	3	4	5	6
RADIUS = .456	#	.0328	.0226	.0159	.0098	.0063	.0031
AMPLITUDE	=	.0379	.256.8	.247.0	.237.5	.236.2	.221.4
PHASE ANGLE	#	254.5					
RADIUS = .633	#	.0222	.0093	.0027	.0042	.0033	.0019
AMPLITUDE	=	.0079	.252.9	.219.8	.161.2	.257.3	.270.6
PHASE ANGLE	#	298.9					
RADIUS = .781	#	.0151	.0069	.0056	.0063	.0014	.0016
AMPLITUDE	=	.0196	.267.9	.269.9	.345.6	.274.0	.258.9
PHASE ANGLE	#	228.3					
RADIUS = .963	#	.0167	.0095	.0029	.0033	.0015	.0014
AMPLITUDE	=	.0165	.269.1	.273.1	.325.0	.319.7	.344.8
PHASE ANGLE	#	256.5					
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)							
HARMONIC	#	9	10	11	12	13	14
RADIUS = .456	#	.0014	.0006	.0005	.0007	.0008	.0008
AMPLITUDE	=	.0021	.17.2	.44.4	.92.3	.135.5	.133.8
PHASE ANGLE	#	47.3					
RADIUS = .633	#	.0010	.0006	.0008	.0002	.0001	.0001
AMPLITUDE	=	.0013	.353.7	.29.4	.60.0	.68.2	.105.1
PHASE ANGLE	#	350.1					
RADIUS = .781	#	.0013	.0007	.0005	.0008	.0004	.0004
AMPLITUDE	=	.0013	.255.3	.282.7	.291.9	.267.3	.268.9
PHASE ANGLE	#	278.3					
RADIUS = .963	#	.0002	.0001	.0003	.0003	.0002	.0001
AMPLITUDE	=	.0002	.200.9	.242.7	.318.7	.310.6	.340.6
PHASE ANGLE	#	77.8					

TABLE A-10 - HARMONIC ANALYSIS OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 9

		VELOCITY COMPONENT RATIOS FOR MODEL 5365 FROM EXP. 9						J _A = .739	
		HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (V _X /V)							
HARMONIC		1	2	3	4	5	6	7	8
RADIUS = .312	=	.1039	.0435	.0460	.0400	.0203	.0132	.0106	.0022
AMPLITUDE	=	242.0	265.5	264.1	254.7	235.6	196.2	163.4	134.3
PHASE ANGLE	=								
RADIUS = .350	=	.0828	.0404	.0386	.0324	.0170	.0109	.0083	.0015
AMPLITUDE	=	244.1	263.0	260.6	251.5	235.4	200.9	165.3	125.8
PHASE ANGLE	=								
RADIUS = .400	=	.0590	.0367	.0302	.0238	.0133	.0084	.0056	.0007
AMPLITUDE	=	247.9	259.9	255.0	246.1	235.3	209.0	169.5	97.8
PHASE ANGLE	=								
RADIUS = .500	=	.0254	.0300	.0180	.0110	.0076	.0051	.0017	.0009
AMPLITUDE	=	262.8	254.7	239.5	227.7	238.0	233.6	200.4	356.1
PHASE ANGLE	=								
RADIUS = .600	=	.0101	.0240	.0109	.0040	.0046	.0036	.0016	.0015
AMPLITUDE	=	293.6	252.6	222.7	185.7	250.5	263.1	292.8	334.6
PHASE ANGLE	=								
RADIUS = .700	=	.0129	.0179	.0070	.0023	.0057	.0023	.0018	.0014
AMPLITUDE	=	239.7	259.4	243.6	350.2	266.6	262.7	296.4	307.4
PHASE ANGLE	=								
RADIUS = .800	=	.0204	.0147	.0071	.0060	.0063	.0012	.0013	.0012
AMPLITUDE	=	228.1	269.6	273.5	345.0	275.9	260.6	297.9	290.6
PHASE ANGLE	=								
RADIUS = .900	=	.0197	.0150	.0095	.0054	.0048	.0008	.0008	.0005
AMPLITUDE	=	237.0	274.3	276.8	339.5	291.6	317.4	330.6	324.0
PHASE ANGLE	=								
RADIUS = 1.000	=	.0165	.0167	.0095	.0029	.0033	.0015	.0009	.0005
AMPLITUDE	=	256.5	273.1	269.1	325.0	319.7	344.8	19.9	39.5
PHASE ANGLE	=								

TABLE A-10 (Continued)

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS							(V_X/V)		
VELOCITY COMPONENT RATIOS FOR MODEL 5365 FROM EXP. 9 PROPELLER DIAMETER = 6.00 FEET							$U_A = .739$		
HARMONIC	#	9	10	11	12	13	14	15	16
RADIUS = .312									
AMPLITUDE = .0035		.0012	.0003	.0014	.0016	.0016	.0015	.0008	
PHASE ANGLE = 77.5		37.5	258.2	230.6	179.7	149.1	148.3	176.8	
RADIUS = .350									
AMPLITUDE = .0021		.0013	.0001	.0009	.0013	.0014	.0013	.0007	
PHASE ANGLE = 70.7		30.2	334.7	222.6	171.0	145.7	143.7	167.3	
RADIUS = .400									
AMPLITUDE = .0026		.0014	.0004	.0003	.0010	.0011	.0010	.0005	
PHASE ANGLE = 60.6		23.3	38.5	181.1	156.1	140.5	137.0	152.2	
RADIUS = .500									
AMPLITUDE = .0018		.0014	.0007	.0007	.0006	.0006	.0006	.0003	
PHASE ANGLE = 35.5		12.8	44.4	77.3	118.6	128.0	121.5	117.7	
RADIUS = .600									
AMPLITUDE = .0014		.0011	.0007	.0009	.0004	.0002	.0003	.0002	
PHASE ANGLE = 3.1		.4	36.4	64.3	83.6	112.1	100.6	84.8	
RADIUS = .700									
AMPLITUDE = .0012		.0006	.0005	.0003	.0004	.0002	.0002	.0002	
PHASE ANGLE = 304.5		301.3	318.5	357.5	269.7	259.5	280.4	281.4	
RADIUS = .800									
AMPLITUDE = .0013		.0007	.0008	.0006	.0008	.0004	.0005	.0004	
PHASE ANGLE = 275.1		250.4	279.2	288.2	267.7	270.4	280.3	275.9	
RADIUS = .900									
AMPLITUDE = .0007		.0005	.0006	.0005	.0006	.0003	.0003	.0002	
PHASE ANGLE = 265.9		235.5	265.5	282.7	275.8	286.5	292.9	283.9	
RADIUS = 1.000									
AMPLITUDE = .0002		.0001	.0003	.0001	.0003	.0002	.0001	.0001	
PHASE ANGLE = 77.8		200.9	242.7	318.7	310.6	340.6	25.4	44.0	

TABLE A-11 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 9

VELOCITY COMPONENT RATIOS FOR MODEL 5365 FROM EXP. 9
PROPELLER DIAMETER = 6.00 FEET

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)

HARMONIC	*	1	2	3	4	5	6	7	8
RADIUS = .456	*	.2333	.0027	.0030	.0039	.0046	.0028	.0022	.0014
AMPLITUDE =		181.0	95.4	170.2	161.9	161.4	166.2	127.5	69.0
PHASE ANGLE =									
RADIUS = .633	*	.2047	.0105	.0074	.0063	.0048	.0039	.0037	.0024
AMPLITUDE =		184.2	281.9	271.3	263.9	275.6	303.8	334.7	.8
PHASE ANGLE =									
RADIUS = .781	*	.1873	.0015	.0044	.0021	.0022	.0020	.0011	.0012
AMPLITUDE =		181.3	305.1	304.1	273.6	269.7	259.4	286.7	294.9
PHASE ANGLE =									
RADIUS = .963	*	.1813	.0025	.0037	.0032	.0023	.0022	.0017	
AMPLITUDE =		178.8	39.5	26.5	51.8	53.6	58.4	60.3	82.4
PHASE ANGLE =									

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)

HARMONIC	*	9	10	11	12	13	14	15	16
RADIUS = .456	*	.0022	.0016	.0014	.0011	.0010	.0009	.0006	
AMPLITUDE =		70.0	63.1	83.8	95.8	109.8	114.9	115.2	119.4
PHASE ANGLE =									
RADIUS = .633	*	.0017	.0015	.0013	.0013	.0014	.0014	.0013	.0012
AMPLITUDE =		39.3	65.1	102.0	143.2	175.7	205.6	237.0	255.4
PHASE ANGLE =									
RADIUS = .781	*	.0010	.0008	.0008	.0006	.0006	.0005	.0005	
AMPLITUDE =		277.9	293.1	304.5	305.1	304.1	302.0	316.8	320.9
PHASE ANGLE =									
RADIUS = .963	*	.0013	.0008	.0005	.0004	.0004	.0004	.0004	.0004
AMPLITUDE =		103.3	101.2	98.6	93.3	88.0	78.8	71.7	89.7
PHASE ANGLE =									

TABLE A-12 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 9

VELOCITY COMPONENT RATIOS FOR MODEL 5365 FROM EXP. 9								JA = .739
PROPELLER DIAMETER = 6.00 FEET								
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)								
HARMONIC	1	2	3	4	5	6	7	8
RADIUS = .312								
AMPLITUDE =	.2652	.0329	.0179	.0191	.0190	.0154	.0139	.0050
PHASE ANGLE =	174.9	99.5	108.7	114.2	132.1	147.7	147.3	152.0
RADIUS = .350								
AMPLITUDE =	.2558	.0232	.0128	.0139	.0144	.0113	.0101	.0035
PHASE ANGLE =	176.8	99.4	112.9	118.2	135.1	149.0	145.8	143.6
RADIUS = .400								
AMPLITUDE =	.2446	.0124	.0071	.0082	.0091	.0068	.0059	.0020
PHASE ANGLE =	178.9	99.0	124.3	128.5	142.1	152.5	142.0	121.1
RADIUS = .500								
AMPLITUDE =	.2253	.0031	.0035	.0033	.0028	.0011	.0008	.0017
PHASE ANGLE =	182.3	284.2	232.2	215.3	201.5	232.4	36.6	35.7
RADIUS = .600								
AMPLITUDE =	.2094	.0101	.0070	.0060	.0044	.0035	.0034	.0024
PHASE ANGLE =	184.1	281.7	266.9	259.9	270.2	302.9	337.8	6.6
RADIUS = .700								
AMPLITUDE =	.1954	.0056	.0059	.0043	.0037	.0030	.0022	.0016
PHASE ANGLE =	182.8	283.7	283.5	264.9	271.2	281.8	315.2	327.9
RADIUS = .800								
AMPLITUDE =	.1859	.0010	.0041	.0016	.0019	.0018	.0009	.0011
PHASE ANGLE =	180.9	329.6	310.3	280.2	270.9	255.0	281.0	290.0
RADIUS = .900								
AMPLITUDE =	.1815	.0021	.0032	.0015	.0007	.0003	.0006	.0002
PHASE ANGLE =	179.5	53.7	355.4	39.6	25.8	79.8	65.6	71.5
RADIUS = 1.000								
AMPLITUDE =	.1813	.0025	.0037	.0032	.0023	.0022	.0022	.0017
PHASE ANGLE =	178.8	39.5	26.5	51.8	53.6	58.4	60.3	82.4

TABLE A-12 (Continued)

VELOCITY COMPONENT RATIOS FOR MODEL 5365 FROM EXP. 9							$JA = .739$
PROPELLER DIAMETER = 6.00 FEET							
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)							
HARMONIC	=	9	10	11	12	13	14
RADIUS = .312							
AMPLITUDE =	.0020	.0008	.0015	.0028	.0036	.0041	.0047
PHASE ANGLE =	130.7	320.3	350.3	6.3	33.8	55.9	76.0
RADIUS = .350							
AMPLITUDE =	.0019	.0007	.0011	.0019	.0025	.0030	.0034
PHASE ANGLE =	109.9	18.0	17.2	18.1	42.6	61.8	79.5
RADIUS = .400							
AMPLITUDE =	.0020	.0012	.0011	.0012	.0015	.0018	.0020
PHASE ANGLE =	87.0	52.6	58.6	48.5	64.6	76.3	88.0
RADIUS = .500							
AMPLITUDE =	.0022	.0019	.0016	.0013	.0012	.0010	.0006
PHASE ANGLE =	61.0	66.2	93.0	118.3	140.4	157.5	173.4
RADIUS = .600							
AMPLITUDE =	.0019	.0018	.0015	.0015	.0014	.0012	.0012
PHASE ANGLE =	45.2	66.8	101.3	139.2	170.0	199.0	230.9
RADIUS = .700							
AMPLITUDE =	.0008	.0005	.0002	.0002	.0005	.0007	.0008
PHASE ANGLE =	335.8	6.7	33.2	185.9	215.9	239.2	264.7
RADIUS = .800							
AMPLITUDE =	.0010	.0008	.0008	.0007	.0006	.0006	.0005
PHASE ANGLE =	272.4	288.7	303.0	308.3	311.6	312.3	328.0
RADIUS = .900							
AMPLITUDE =	.0003	.0003	.0004	.0004	.0004	.0004	.0004
PHASE ANGLE =	207.9	273.0	309.8	331.2	343.7	359.0	20.2
RADIUS = 1.000							
AMPLITUDE =	.0013	.0008	.0005	.0004	.0004	.0004	.0004
PHASE ANGLE =	103.3	101.2	98.6	93.3	88.0	78.8	71.7

APPENDIX B
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENT 10

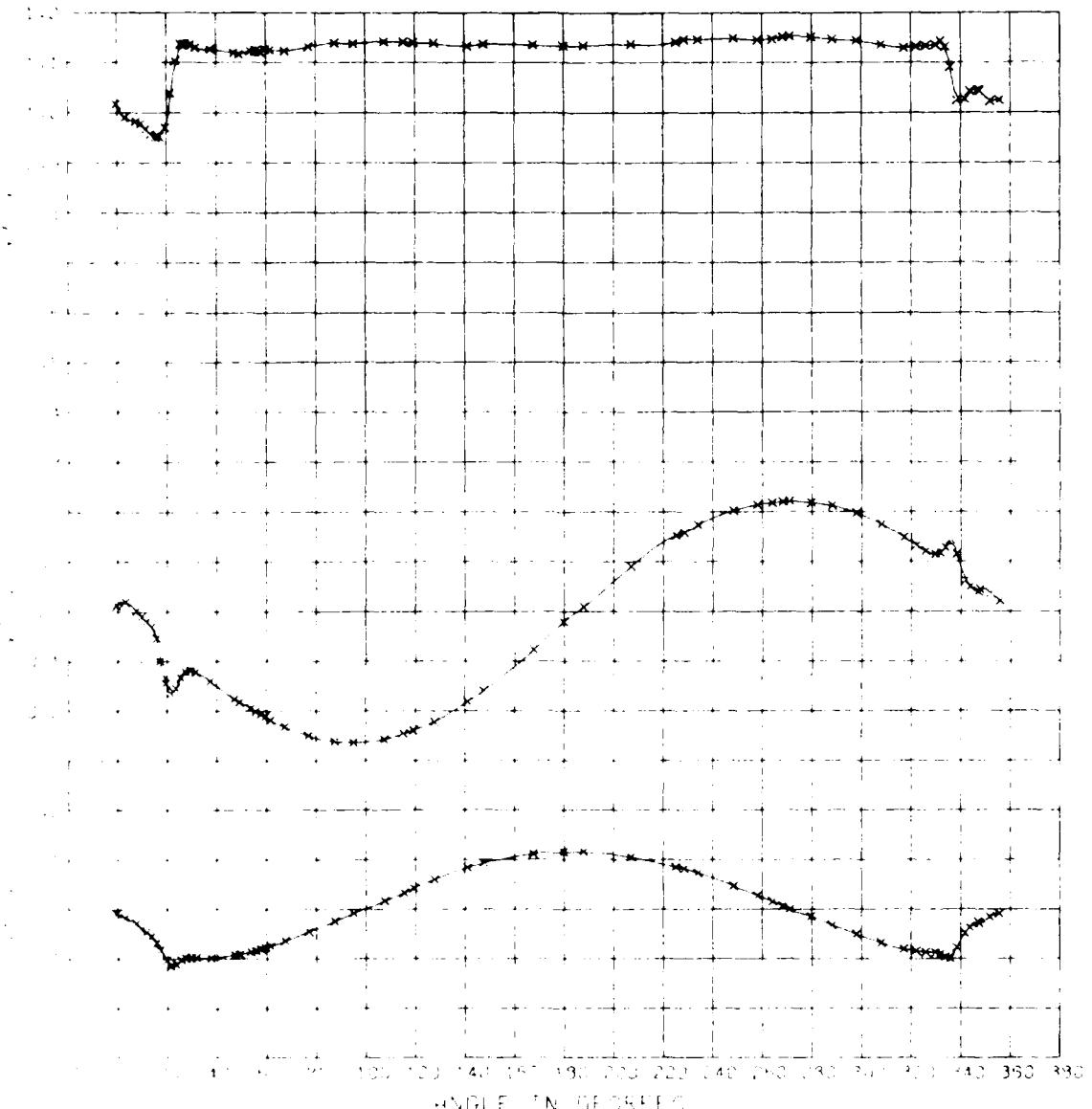
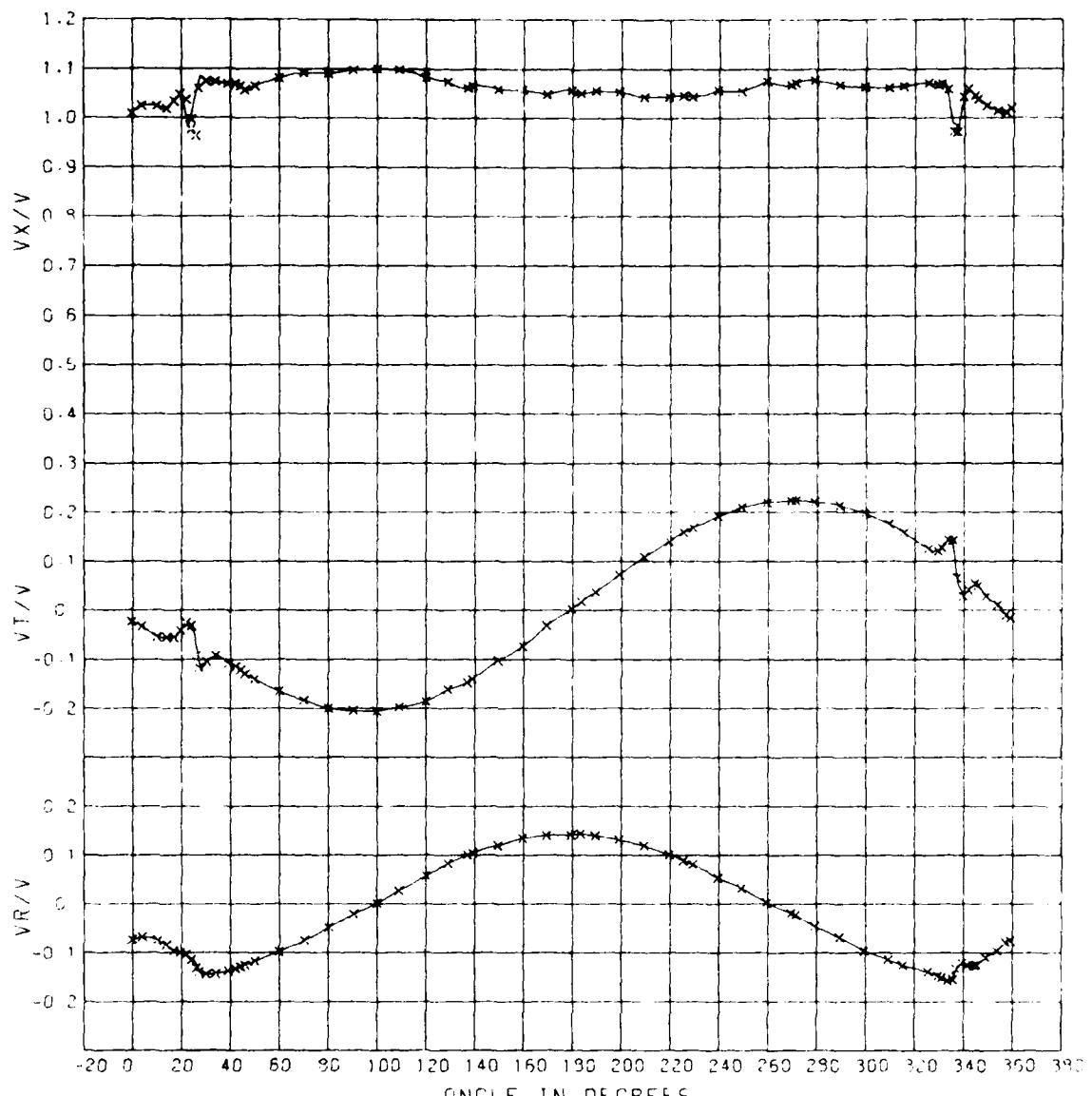


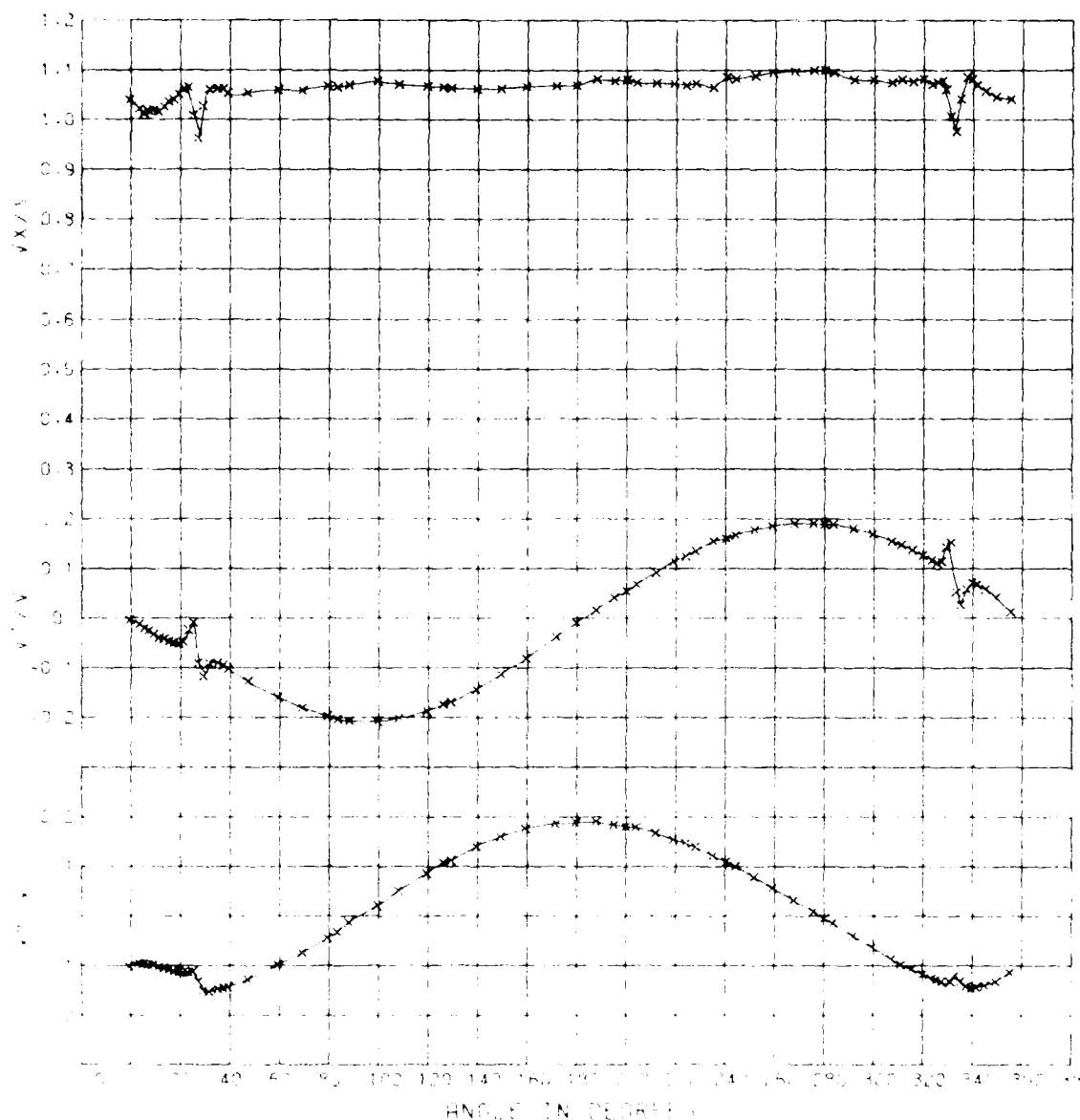
FIGURE 3-1 - CIRCUMFERENTIAL DISTRIBUTION OF THE LONGITUDINAL, TANGENTIAL, AND RADIAL VELOCITY COMPONENT RATIOS - RADIUS RATIO = 0.456 FOR EXPERIMENT 10
CORRELATION WITH R.V. AT RING 10
C-456 RAD.

Figure 3-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456
for Experiment 10



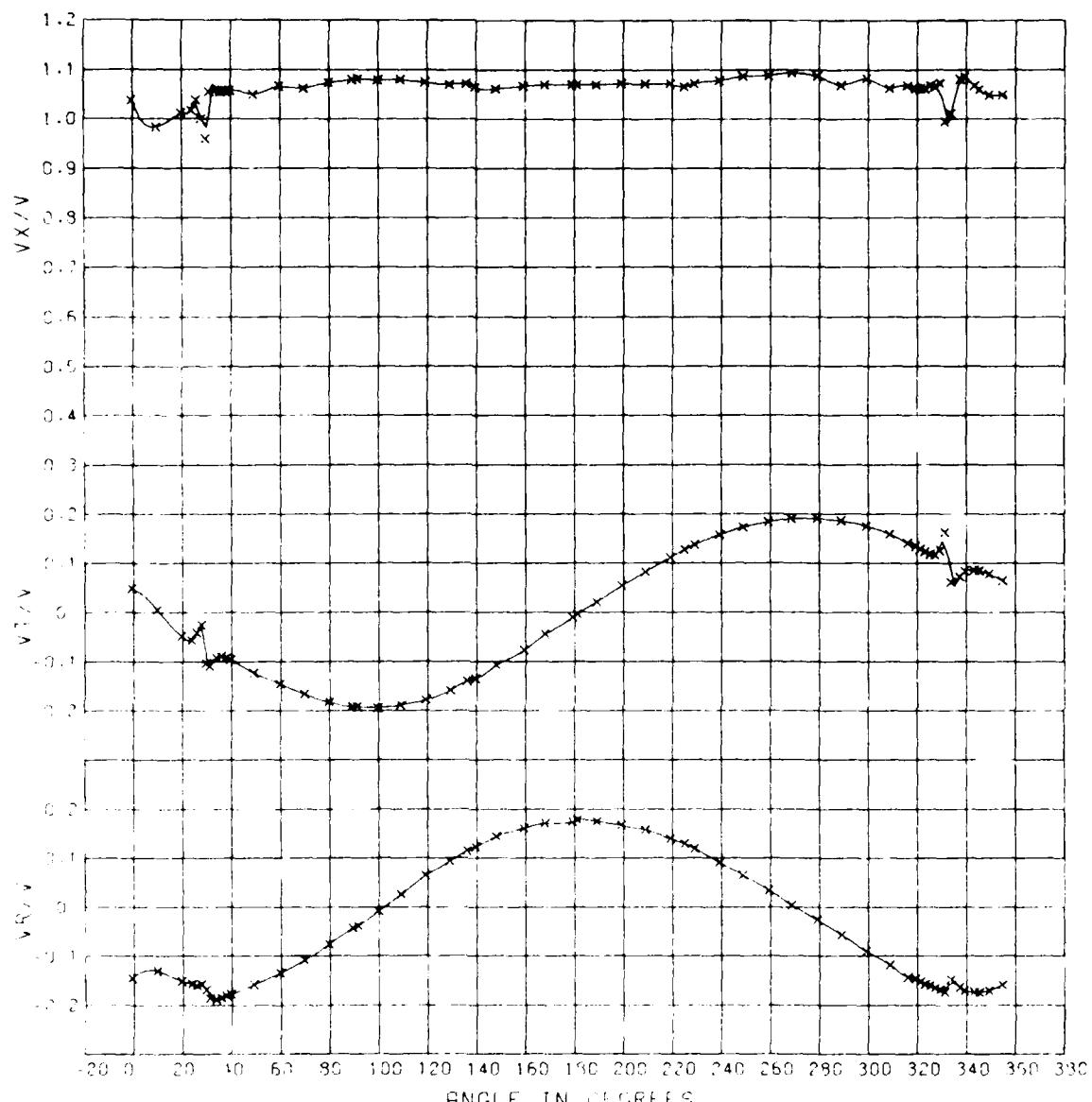
VELOCITY COMPONENT RATIOS FOR MODEL 5365 CORRELATION WITH R/V ATHENA 10
 $\theta = 0.633 \text{ RAD.}$

Figure B-2 - Circumferential Distribution of the Longitudinal, Tangential,
 and Radial Velocity Component Ratios - Radius Ratio = 0.633
 for Experiment 10



VELOCITY COMPONENT RATIOS FOR MODEL 5365 CORRELATION WITH R/V ATHENA 17
R = 0.781 RAD.

Figure B-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 10



VELOCITY COMPONENT RA 105 FOR MODEL 5365 CORRELATION WITH R/V ATHENA 10
0.963 RAD.

Figure B-4 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.963
for Experiment 10

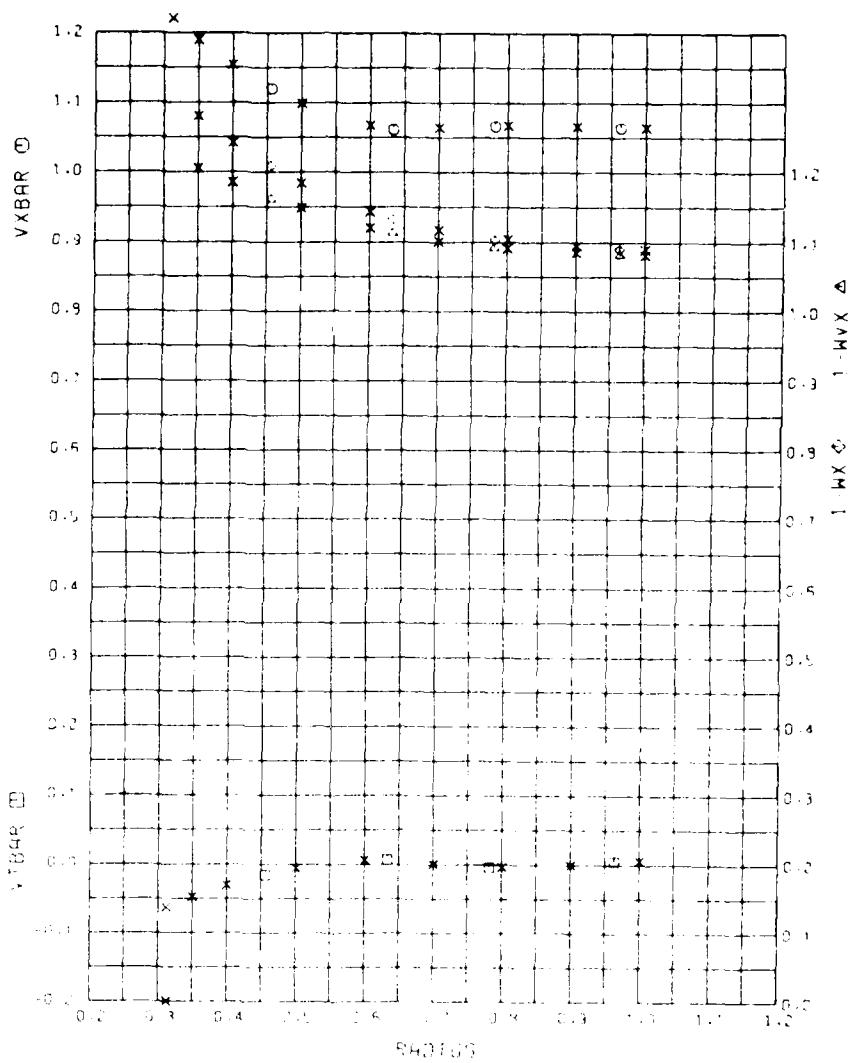


Figure B-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 10

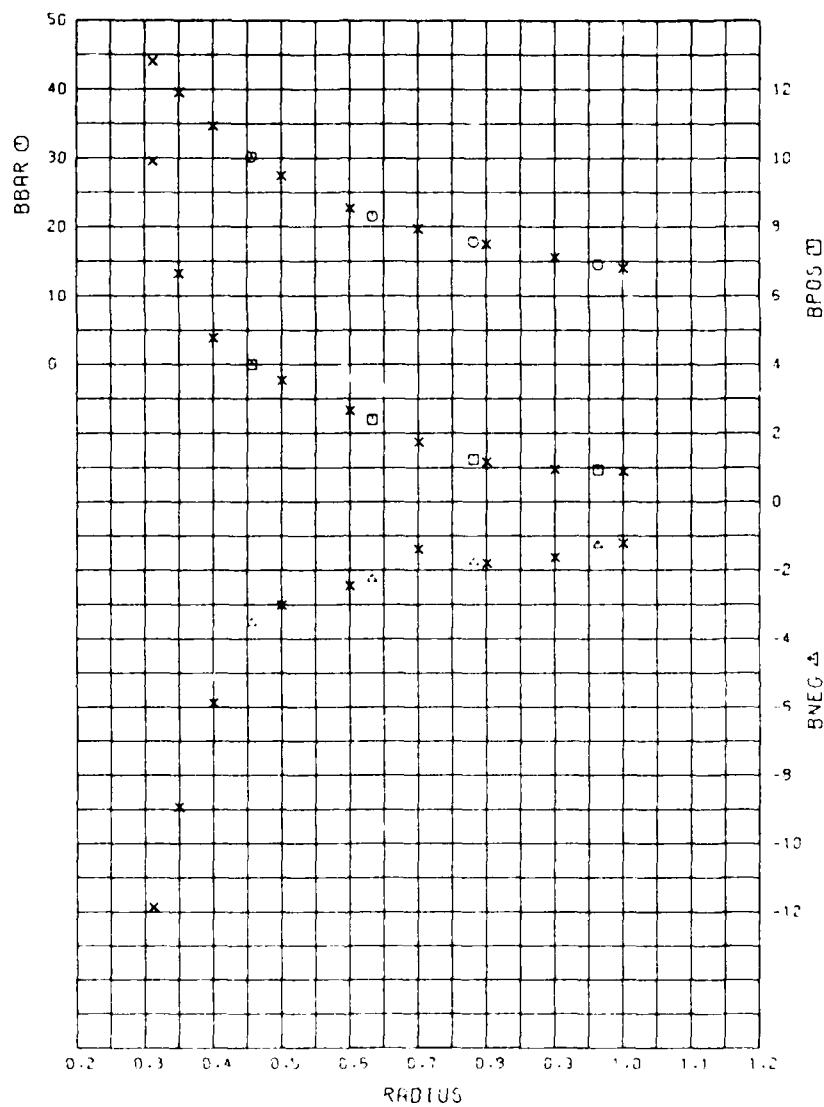


Figure B-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 10

TABLE B-1

INPUT DATA FOR HARMONIC ANALYSIS FOR R/V ATHENA,
MODEL 5365, EXPERIMENT 10

TABLE B-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 10

RADIUS	MEAN ADVANCE ANGLE	MEAN VELOCITY COMPONENT RATIO	INTERPOLATED RADII		EXPERIMENTAL RADII		INTERPOLATION WITH FIELD		A = .754
			INTERPOLATED	EXPERIMENTAL	INTERPOLATED	EXPERIMENTAL	INTERPOLATED	EXPERIMENTAL	
1.000	0.0	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
1.020	-1.120	1.056	1.056	1.051	1.095	1.104	1.057	1.064	1.064
1.040	-0.160	-0.044	-0.053	-0.043	-0.048	-0.041	-0.057	-0.050	-0.054
1.060	-0.570	-0.165	-0.110	-0.093	-0.035	-0.011	-0.052	-0.049	-0.051
1.080	-1.161	1.052	1.052	1.052	1.0205	1.0146	1.120	1.101	1.055
1.100	-1.100	1.133	1.104	1.095	1.290	1.242	1.143	1.117	1.095
1.120	-2.146	17.62	14.54	43.01	39.56	34.41	19.67	22.64	14.02
1.140	-2.00	2.39	1.24	35.93	31.61	6.65	4.07	2.15	1.74
1.160	-2.52	35.00	37.50	35.00	22.50	90.3	150.00	100.00	97.50
1.180	-2.54	-2.177	-1.27	-11.17	-8.93	-5.64	-7.77	-2.46	-1.22
1.200	-2.09	35.00	332.50	332.50	5.00	5.63	335.00	332.50	332.50

TABLE B-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 10

TABLE B-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 10

TABLE B-3 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 10

Harmonic	Order	Angle = 0°			Angle = 45°			Angle = 90°			Angle = 135°		
		1	2	3	1	2	3	1	2	3	1	2	3
HARMONIC ANALYSIS OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 10													
1	1	-0.349	-0.349	-0.349	-0.349	-0.349	-0.349	-0.349	-0.349	-0.349	-0.349	-0.349	-0.349
1	2	2.53.2	2.53.2	2.53.2	2.53.2	2.53.2	2.53.2	2.53.2	2.53.2	2.53.2	2.53.2	2.53.2	2.53.2
1	3	2.59.9	2.59.9	2.59.9	2.59.9	2.59.9	2.59.9	2.59.9	2.59.9	2.59.9	2.59.9	2.59.9	2.59.9
2	1	-0.322	-0.322	-0.322	-0.322	-0.322	-0.322	-0.322	-0.322	-0.322	-0.322	-0.322	-0.322
2	2	2.57.4	2.57.4	2.57.4	2.57.4	2.57.4	2.57.4	2.57.4	2.57.4	2.57.4	2.57.4	2.57.4	2.57.4
2	3	2.56.7	2.56.7	2.56.7	2.56.7	2.56.7	2.56.7	2.56.7	2.56.7	2.56.7	2.56.7	2.56.7	2.56.7
3	1	-0.313	-0.313	-0.313	-0.313	-0.313	-0.313	-0.313	-0.313	-0.313	-0.313	-0.313	-0.313
3	2	2.56.4	2.56.4	2.56.4	2.56.4	2.56.4	2.56.4	2.56.4	2.56.4	2.56.4	2.56.4	2.56.4	2.56.4
3	3	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0
4	1	-0.307	-0.307	-0.307	-0.307	-0.307	-0.307	-0.307	-0.307	-0.307	-0.307	-0.307	-0.307
4	2	2.56.5	2.56.5	2.56.5	2.56.5	2.56.5	2.56.5	2.56.5	2.56.5	2.56.5	2.56.5	2.56.5	2.56.5
4	3	2.56.2	2.56.2	2.56.2	2.56.2	2.56.2	2.56.2	2.56.2	2.56.2	2.56.2	2.56.2	2.56.2	2.56.2
5	1	-0.304	-0.304	-0.304	-0.304	-0.304	-0.304	-0.304	-0.304	-0.304	-0.304	-0.304	-0.304
5	2	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3
5	3	2.56.1	2.56.1	2.56.1	2.56.1	2.56.1	2.56.1	2.56.1	2.56.1	2.56.1	2.56.1	2.56.1	2.56.1
6	1	-0.303	-0.303	-0.303	-0.303	-0.303	-0.303	-0.303	-0.303	-0.303	-0.303	-0.303	-0.303
6	2	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0
6	3	2.55.7	2.55.7	2.55.7	2.55.7	2.55.7	2.55.7	2.55.7	2.55.7	2.55.7	2.55.7	2.55.7	2.55.7
7	1	-0.302	-0.302	-0.302	-0.302	-0.302	-0.302	-0.302	-0.302	-0.302	-0.302	-0.302	-0.302
7	2	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3
7	3	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0
8	1	-0.301	-0.301	-0.301	-0.301	-0.301	-0.301	-0.301	-0.301	-0.301	-0.301	-0.301	-0.301
8	2	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3
8	3	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0
9	1	-0.300	-0.300	-0.300	-0.300	-0.300	-0.300	-0.300	-0.300	-0.300	-0.300	-0.300	-0.300
9	2	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3	2.56.3
9	3	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0	2.56.0

TABLE B-4 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 10

		VELOCITY RATIOS OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 10						
		SATELLITE 5305 CORRELATION WITH R.V. ATHENA 10 PROPELLER DIRECTION X = .734						
		HARMONIC RATIOS OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)						
RADIUS	=	2	1	2	3	4	5	6
RADIUS	=	.312						
AMPLITUDE	=	.1100	.0418	.0422	.0422	.0272	.0248	.0187
PHASE ANGLE	=	.246.3	.265.9	.265.5	.255.9	.249.4	.228.0	.203.4
RADIUS	=	.350						
AMPLITUDE	=	.0959	.0428	.0515	.0557	.0235	.0206	.0151
PHASE ANGLE	=	.249.6	.265.2	.268.8	.257.4	.251.4	.230.0	.210.5
RADIUS	=	.400						
AMPLITUDE	=	.0593	.0310	.0272	.0265	.0192	.0157	.0109
PHASE ANGLE	=	.45.2	.264.3	.257.6	.259.3	.251.3	.233.5	.214.2
RADIUS	=	.500						
AMPLITUDE	=	.0246	.0316	.0375	.0122	.0122	.0083	.0046
PHASE ANGLE	=	.275.0	.262.5	.254.1	.260.1	.260.4	.244.8	.227.5
RADIUS	=	.660						
AMPLITUDE	=	.0118	.0250	.0264	.02031	.0073	.0040	.0012
PHASE ANGLE	=	.327.5	.260.5	.259.5	.244.5	.263.7	.265.4	.270.4
RADIUS	=	.700						
AMPLITUDE	=	.0639	.0176	.0174	.0047	.0047	.0024	.0003
PHASE ANGLE	=	.32.7	.259.0	.258.2	.260.1	.243.9	.271.6	.116.3
RADIUS	=	.800						
AMPLITUDE	=	.0112	.0140	.0163	.0112	.0047	.0019	.0034
PHASE ANGLE	=	.24.3	.257.0	.255.4	.241.7	.215.7	.233.5	.136.3
RADIUS	=	.900						
AMPLITUDE	=	.0704	.0155	.0102	.0051	.0062	.0039	.0010
PHASE ANGLE	=	.251.2	.255.6	.252.4	.248.4	.205.3	.196.8	.154.8
RADIUS	=	1.000						
AMPLITUDE	=	.0165	.0190	.0175	.0104	.0077	.0055	.0011
PHASE ANGLE	=	.246.8	.255.5	.257.3	.247.1	.211.1	.189.6	.166.3

TABLE B-4 (Continued)

COPPER CONCENTRATION IN THE ELECTROLYTE	COPPER CONCENTRATION IN THE ELECTROLYTE		COPPER CONCENTRATION IN THE ELECTROLYTE		COPPER CONCENTRATION IN THE ELECTROLYTE	
	100	120	140	160	180	200
0.0012	-3.2	-3.2	-3.2	-3.2	-3.2	-3.2
0.0014	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0016	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0018	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0020	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0022	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0024	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0026	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0028	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0030	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0032	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0034	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0036	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0038	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0040	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0042	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0044	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0046	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0048	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0050	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0052	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0054	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0056	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0058	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0060	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0062	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0064	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0066	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0068	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0070	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0072	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0074	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0076	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0078	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0080	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0082	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0084	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0086	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0088	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0090	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0092	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0094	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0096	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0098	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0
0.0100	-2.5	-2.4	-2.3	-2.2	-2.1	-2.0

TABLE B-5 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 10

TABLE B-6 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE INTERVOLATED RADII FOR EXPERIMENT 10

TABLE B-6 (Continued)

APPENDIX C
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENT 11

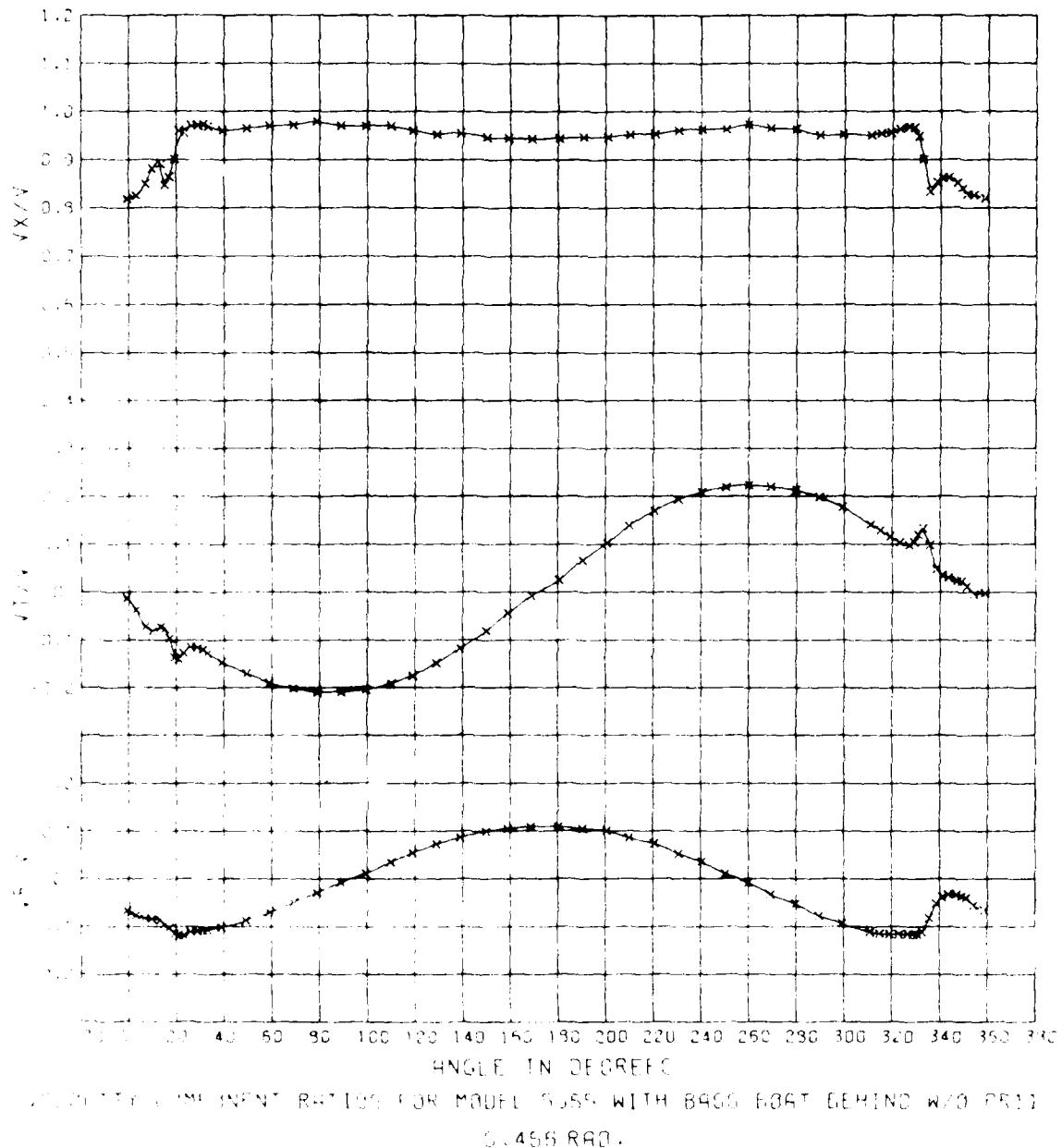
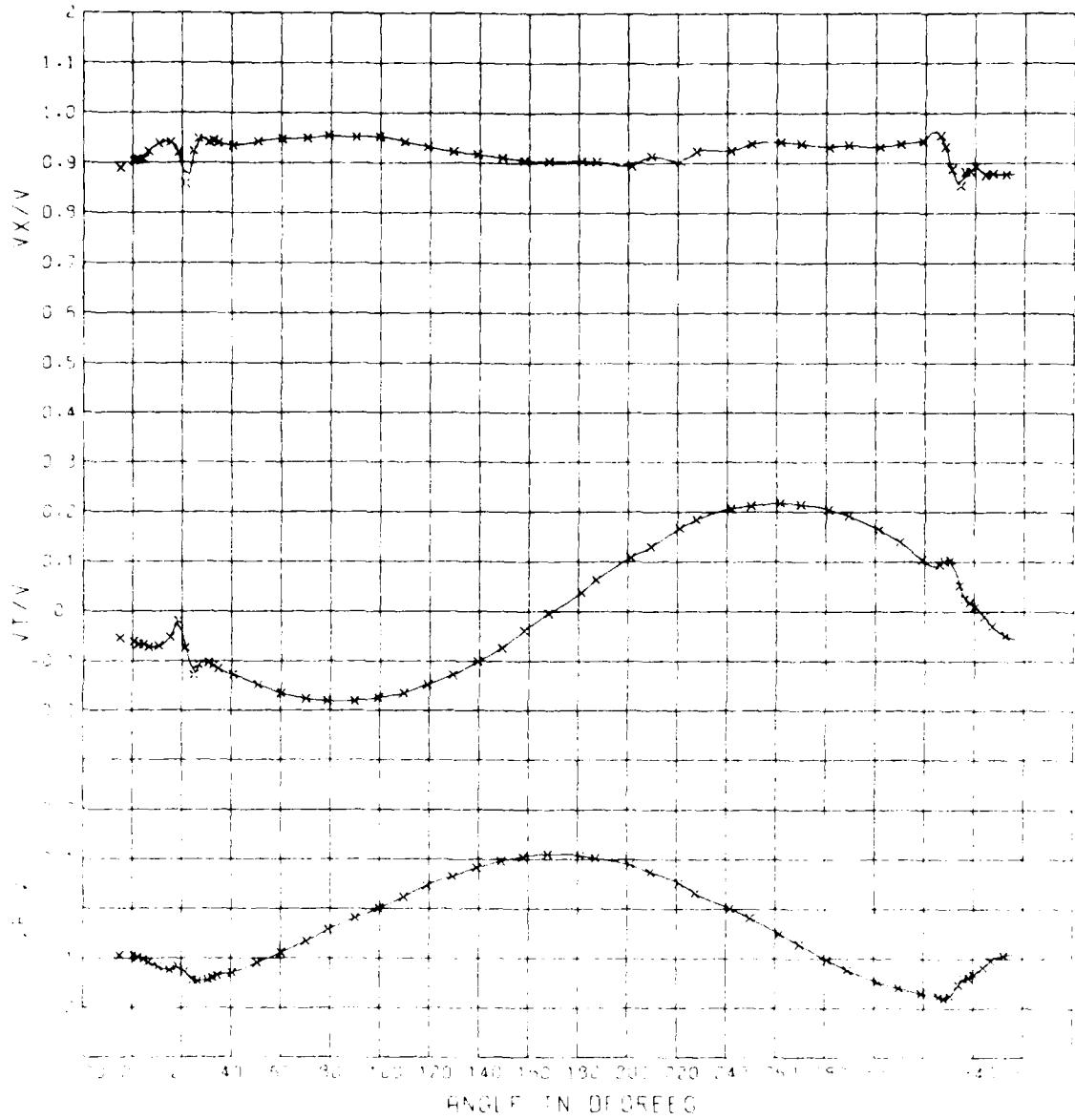


Figure C-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment II



VELOCITY COMPONENT RATIOS FOR MODEL 5354 WITH DIAH. RATIO = 0.633
G = 6.37 RAD.

Figure C-2 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.633
for Experiment 11

AD-A094 342

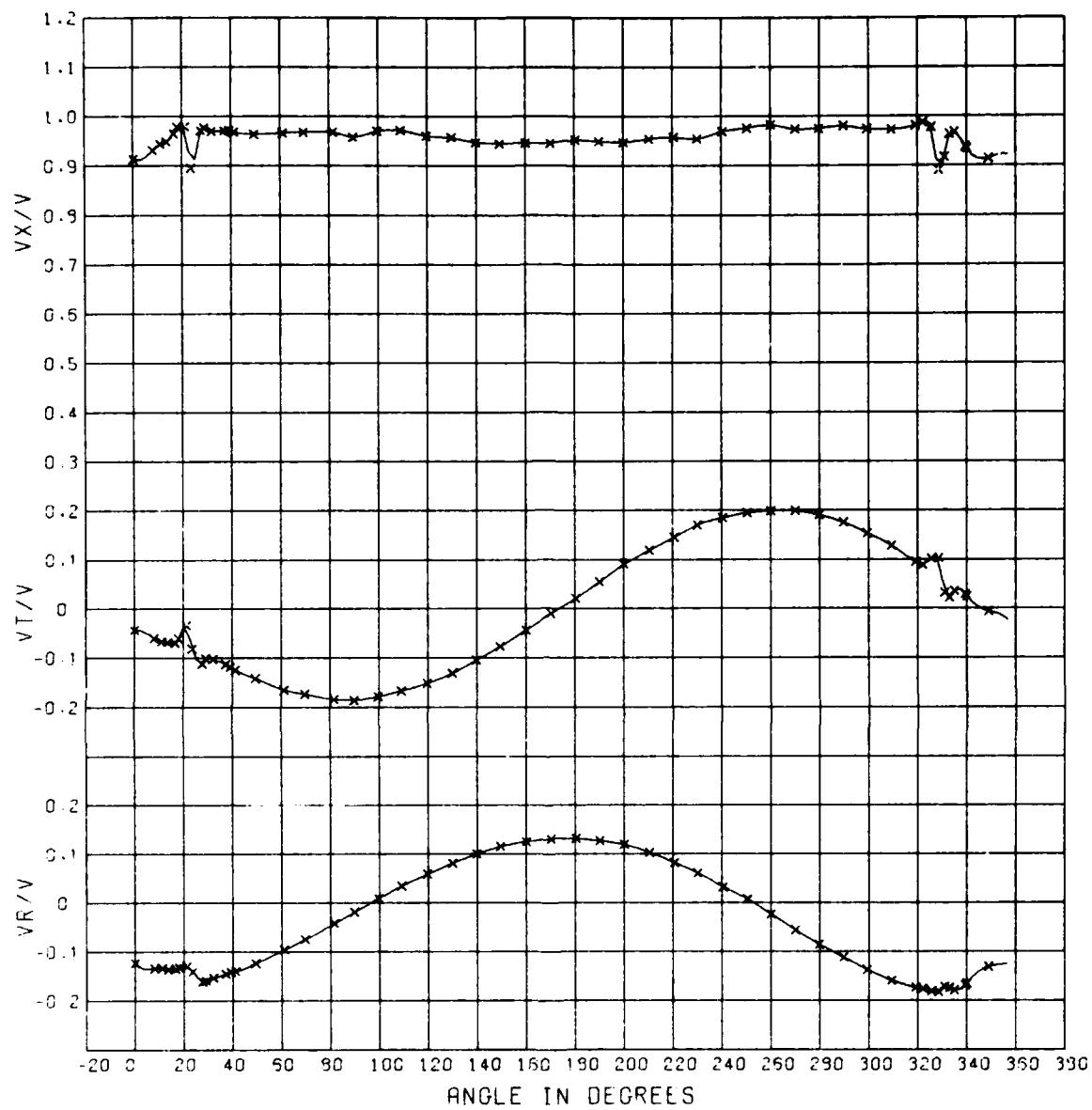
DAVID W TAYLOR NAVAL SHIP RESEARCH AND DEVELOPMENT CE--ETC F/G 13/10
ANALYSIS OF WAKE SURVEY EXPERIMENTAL DATA FOR MODEL 5365 REPRES--ETC(U)
JAN 81 R B HURWITZ, L B CROOK
DTNSRDC/SPD-0833-06

UNCLASSIFIED

NL

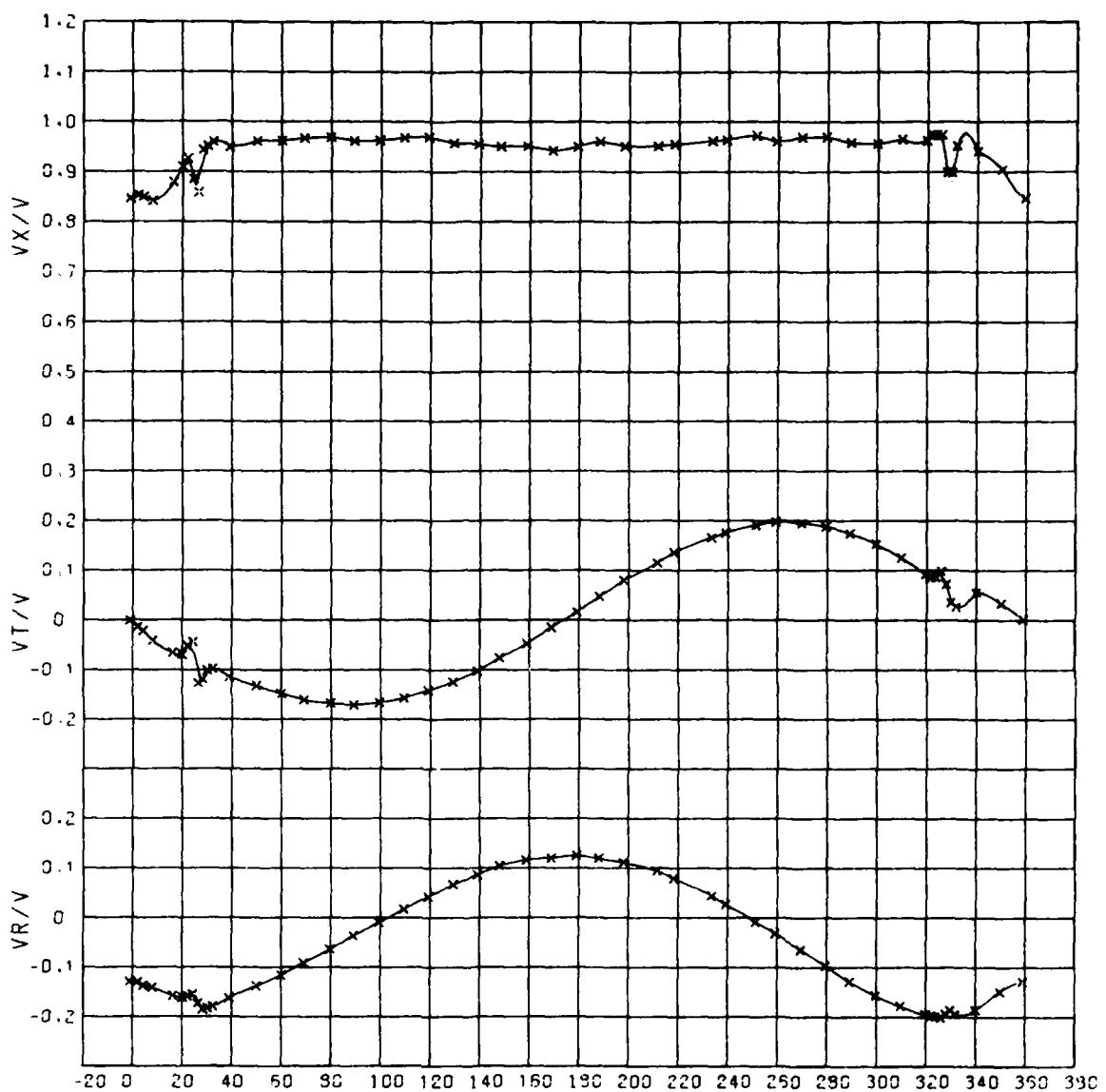
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VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND W/O PR11
0.781 RAD.

Figure C-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 11



VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND W/O PR11
0.963 RAD.

Figure C-4 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.963
for Experiment 11

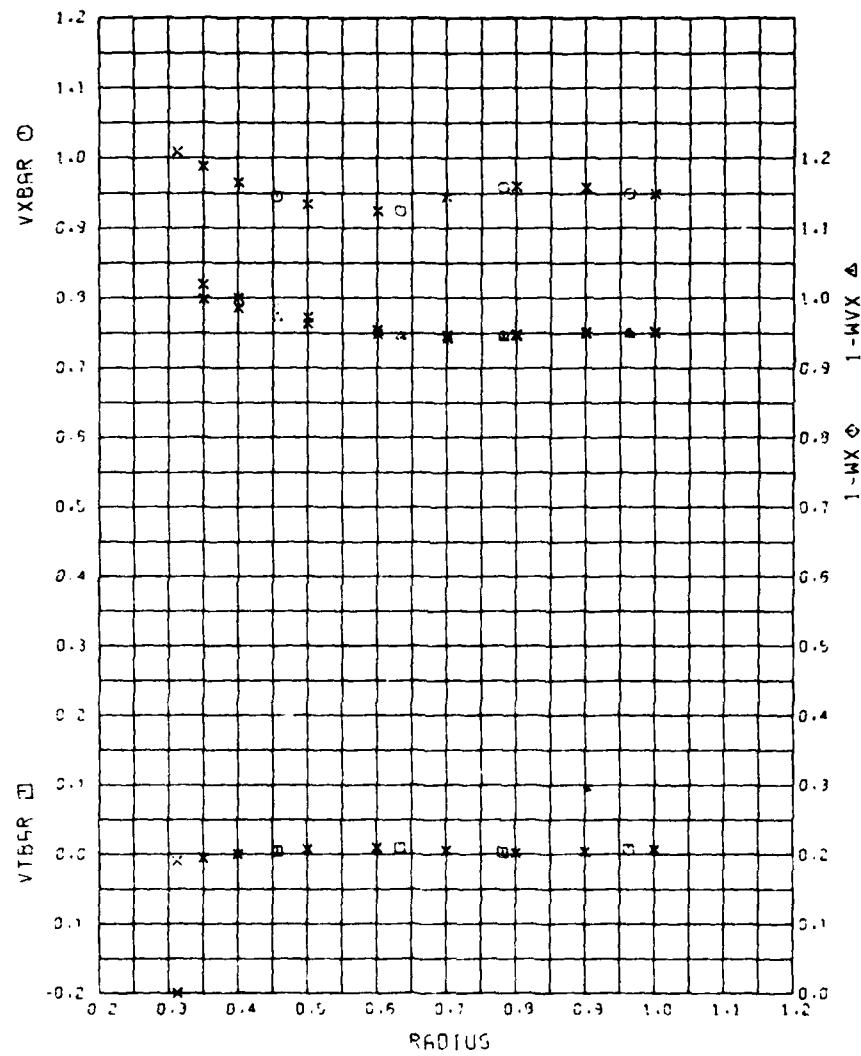


Figure C-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 11

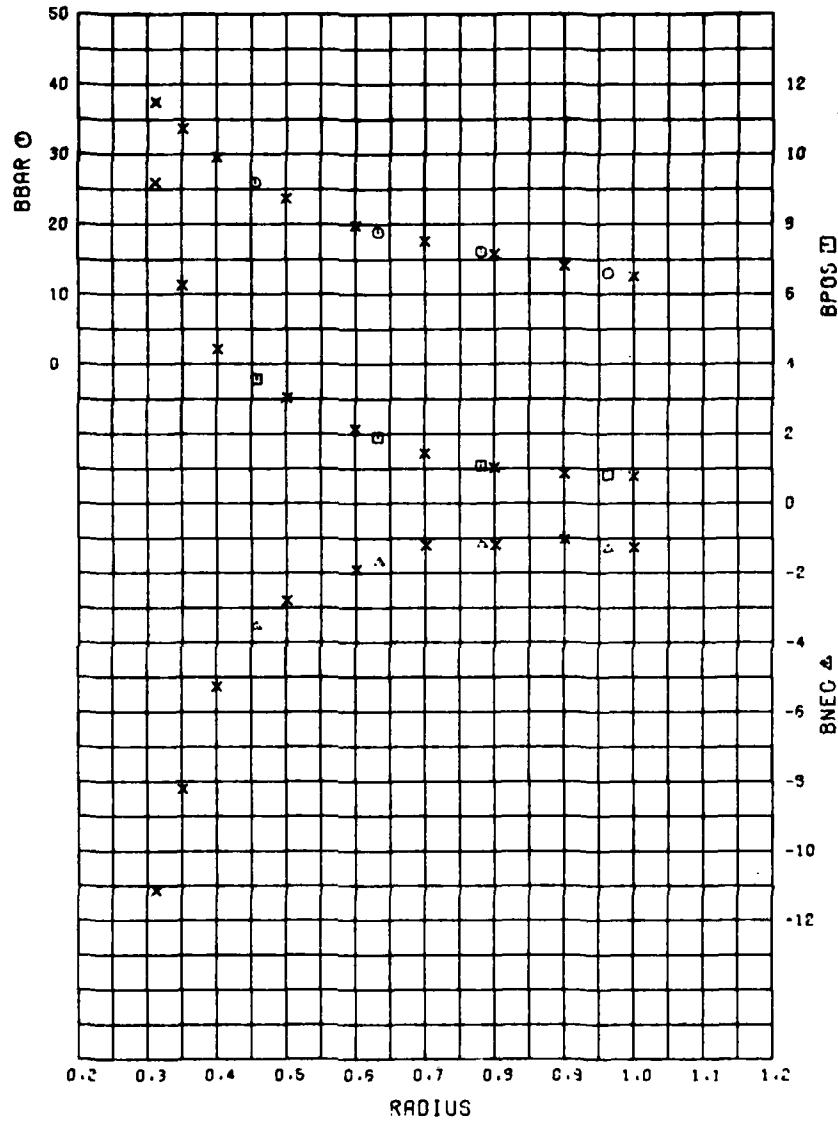


Figure C-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 11

TABLE C-1

INPUT DATA FOR HARMONIC ANALYSIS FOR R/V ATHENA,
MODEL 5365, EXPERIMENT 11

ANGLE	RADIUS *	Y/X	X/Y	W/V	ANGLE	RADIUS *	Y/X	X/Y	W/V	ANGLE	RADIUS *	Y/X	X/Y	W/V	ANGLE	RADIUS *	Y/X	X/Y	W/V
-9	.819	-.012	.000	.000	-9	.804	-.014	.000	.000	0	.913	-.003	.000	.000	0	.907	-.001	.000	.000
1	.827	-.017	.000	.000	1	.804	-.001	.000	.000	9	.931	-.000	.000	.000	9	.936	-.010	.000	.000
2	.835	-.022	.000	.000	2	.800	-.006	.000	.000	10	.943	-.004	.000	.000	10	.942	-.022	.000	.000
3	.843	-.027	.000	.000	3	.797	-.010	.000	.000	11	.953	-.000	.000	.000	11	.953	-.037	.000	.000
4	.851	-.031	.000	.000	4	.794	-.015	.000	.000	12	.960	-.006	.000	.000	12	.962	-.041	.000	.000
5	.859	-.036	.000	.000	5	.791	-.019	.000	.000	13	.965	-.000	.000	.000	13	.965	-.045	.000	.000
6	.867	-.040	.000	.000	6	.788	-.023	.000	.000	14	.969	-.006	.000	.000	14	.969	-.049	.000	.000
7	.875	-.044	.000	.000	7	.785	-.027	.000	.000	15	.970	-.000	.000	.000	15	.970	-.053	.000	.000
8	.883	-.048	.000	.000	8	.782	-.031	.000	.000	16	.970	-.004	.000	.000	16	.970	-.057	.000	.000
9	.891	-.051	.000	.000	9	.779	-.034	.000	.000	17	.971	-.000	.000	.000	17	.971	-.061	.000	.000
10	.899	-.054	.000	.000	10	.776	-.037	.000	.000	18	.971	-.004	.000	.000	18	.971	-.065	.000	.000
11	.907	-.057	.000	.000	11	.773	-.040	.000	.000	19	.971	-.008	.000	.000	19	.971	-.069	.000	.000
12	.914	-.060	.000	.000	12	.770	-.043	.000	.000	20	.971	-.012	.000	.000	20	.971	-.073	.000	.000
13	.921	-.063	.000	.000	13	.767	-.046	.000	.000	21	.971	-.016	.000	.000	21	.971	-.077	.000	.000
14	.929	-.066	.000	.000	14	.764	-.049	.000	.000	22	.971	-.020	.000	.000	22	.971	-.081	.000	.000
15	.936	-.069	.000	.000	15	.761	-.052	.000	.000	23	.971	-.024	.000	.000	23	.971	-.085	.000	.000
16	.943	-.071	.000	.000	16	.758	-.055	.000	.000	24	.971	-.028	.000	.000	24	.971	-.089	.000	.000
17	.950	-.073	.000	.000	17	.755	-.058	.000	.000	25	.971	-.032	.000	.000	25	.971	-.093	.000	.000
18	.957	-.075	.000	.000	18	.752	-.061	.000	.000	26	.971	-.036	.000	.000	26	.971	-.097	.000	.000
19	.964	-.077	.000	.000	19	.749	-.064	.000	.000	27	.971	-.040	.000	.000	27	.971	-.101	.000	.000
20	.971	-.079	.000	.000	20	.746	-.067	.000	.000	28	.971	-.044	.000	.000	28	.971	-.105	.000	.000
21	.978	-.081	.000	.000	21	.743	-.070	.000	.000	29	.971	-.048	.000	.000	29	.971	-.109	.000	.000
22	.985	-.083	.000	.000	22	.740	-.073	.000	.000	30	.971	-.052	.000	.000	30	.971	-.113	.000	.000
23	.992	-.085	.000	.000	23	.737	-.076	.000	.000	31	.971	-.056	.000	.000	31	.971	-.117	.000	.000
24	.999	-.087	.000	.000	24	.734	-.079	.000	.000	32	.971	-.060	.000	.000	32	.971	-.121	.000	.000
25	.006	-.089	.000	.000	25	.731	-.082	.000	.000	33	.971	-.064	.000	.000	33	.971	-.125	.000	.000
26	.003	-.091	.000	.000	26	.728	-.085	.000	.000	34	.971	-.068	.000	.000	34	.971	-.129	.000	.000
27	.000	-.093	.000	.000	27	.725	-.088	.000	.000	35	.971	-.072	.000	.000	35	.971	-.133	.000	.000
28	.007	-.095	.000	.000	28	.722	-.091	.000	.000	36	.971	-.076	.000	.000	36	.971	-.137	.000	.000
29	.014	-.097	.000	.000	29	.719	-.094	.000	.000	37	.971	-.080	.000	.000	37	.971	-.141	.000	.000
30	.021	-.099	.000	.000	30	.716	-.097	.000	.000	38	.971	-.084	.000	.000	38	.971	-.145	.000	.000
31	.028	-.001	.000	.000	31	.713	-.100	.000	.000	39	.971	-.088	.000	.000	39	.971	-.149	.000	.000
32	.035	-.003	.000	.000	32	.710	-.103	.000	.000	40	.971	-.092	.000	.000	40	.971	-.153	.000	.000
33	.042	-.005	.000	.000	33	.707	-.106	.000	.000	41	.971	-.096	.000	.000	41	.971	-.157	.000	.000
34	.049	-.007	.000	.000	34	.704	-.109	.000	.000	42	.971	-.100	.000	.000	42	.971	-.161	.000	.000
35	.056	-.009	.000	.000	35	.701	-.112	.000	.000	43	.971	-.104	.000	.000	43	.971	-.165	.000	.000
36	.063	-.011	.000	.000	36	.698	-.115	.000	.000	44	.971	-.108	.000	.000	44	.971	-.169	.000	.000
37	.070	-.013	.000	.000	37	.695	-.118	.000	.000	45	.971	-.112	.000	.000	45	.971	-.173	.000	.000
38	.077	-.015	.000	.000	38	.692	-.121	.000	.000	46	.971	-.116	.000	.000	46	.971	-.177	.000	.000
39	.084	-.017	.000	.000	39	.689	-.124	.000	.000	47	.971	-.120	.000	.000	47	.971	-.181	.000	.000
40	.091	-.019	.000	.000	40	.686	-.127	.000	.000	48	.971	-.124	.000	.000	48	.971	-.185	.000	.000
41	.098	-.021	.000	.000	41	.683	-.130	.000	.000	49	.971	-.128	.000	.000	49	.971	-.189	.000	.000
42	.105	-.023	.000	.000	42	.680	-.133	.000	.000	50	.971	-.132	.000	.000	50	.971	-.193	.000	.000
43	.112	-.025	.000	.000	43	.677	-.136	.000	.000	51	.971	-.136	.000	.000	51	.971	-.197	.000	.000
44	.119	-.027	.000	.000	44	.674	-.139	.000	.000	52	.971	-.140	.000	.000	52	.971	-.201	.000	.000
45	.126	-.029	.000	.000	45	.671	-.142	.000	.000	53	.971	-.144	.000	.000	53	.971	-.205	.000	.000
46	.133	-.031	.000	.000	46	.668	-.145	.000	.000	54	.971	-.148	.000	.000	54	.971	-.209	.000	.000
47	.140	-.033	.000	.000	47	.665	-.148	.000	.000	55	.971	-.152	.000	.000	55	.971	-.213	.000	.000
48	.147	-.035	.000	.000	48	.662	-.151	.000	.000	56	.971	-.156	.000	.000	56	.971	-.217	.000	.000
49	.154	-.037	.000	.000	49	.659	-.154	.000	.000	57	.971	-.160	.000	.000	57	.971	-.221	.000	.000
50	.161	-.039	.000	.000	50	.656	-.157	.000	.000	58	.971	-.164	.000	.000	58	.971	-.225	.000	.000
51	.168	-.041	.000	.000	51	.653	-.160	.000	.000	59	.971	-.168	.000	.000	59	.971	-.229	.000	.000
52	.175	-.043	.000	.000	52	.650	-.163	.000	.000	60	.971	-.172	.000	.000	60	.971	-.233	.000	.000
53	.182	-.045	.000	.000	53	.647	-.166	.000	.000	61	.971	-.176	.000	.000	61	.971	-.237	.000	.000
54	.189	-.047	.000	.000	54	.644	-.169	.000	.000	62	.971	-.180	.000	.000	62	.971	-.241	.000	.000
55	.196	-.049	.000	.000	55	.641	-.172	.000	.000	63	.971	-.184	.000	.000	63	.971	-.245	.000	.000
56	.203	-.051	.000	.000	56	.638	-.175	.000	.000	64	.971	-.188	.000	.000	64	.971	-.249	.000	.000
57	.210	-.053	.000	.000	57	.635	-.178	.000	.000	65	.971	-.192	.000	.000	65	.971	-.253	.000	.000
58	.217	-.055	.000	.000	58	.632	-.181	.000	.000	66	.971	-.196	.000	.000	66	.971	-.257	.000	.000
59	.224	-.057	.000	.000	59	.629	-.184	.000	.000	67	.971	-.200	.000	.000	67	.971	-.261	.000	.000
60	.231	-.059	.000	.000	60	.626	-.187	.000	.000	68	.971	-.204	.000	.000	68	.971	-.265	.000	.000
61	.238	-.061	.000	.000	61	.623	-.190	.000	.000	69	.971	-.208	.000	.000	69	.971	-.269	.000	.000
62	.245	-.063	.000	.000	62	.620	-.193	.000	.000	70	.971	-.212	.000	.000	70	.971	-.273	.000	.000
63	.252	-.065	.000	.000	63	.617	-.196	.000	.000	71	.971	-.216	.000	.000	71	.971	-.277	.000	.000
64	.259	-.067	.000	.000	64	.614	-.199	.000	.000	72	.971	-.220	.000	.000	72	.971	-.281	.000	.000
65	.266	-.069	.000	.000	65	.611	-.202	.000	.000	73	.971								

TABLE C-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 11

VELOCITY COMPONENT RATIOS, FOR R = 53.0 FEET WITH BOAT SITTING W/O PR11
PROPELLER DIAMETER = 6.00 FEET
 $\Delta A = .739$

RADIUS =	.456	.633	.781	.963	.312	.350	.400	.500	.600	.700	.800	.900	1.000
VXBAR =	.945	.925	.958	.949	1.009	.998	.965	.934	.924	.945	.960	.958	.949
VTBAR =	.004	.009	.003	.007	-.010	-.005	-.300	.007	.009	.005	.002	.004	.007
VRBAR =	-.007	-.033	-.026	-.040	.040	.025	.025	.017	-.031	-.028	-.027	-.033	-.040
1-WVX =	.971	.945	.943	.948	0.000	.998	.985	.963	.948	.943	.946	.949	.950
1-NX =	.984	.950	.946	.950	0.000	1.019	1.001	.972	.954	.947	.948	.951	.952
BBAR =	25.93	18.90	16.08	13.02	37.46	33.67	29.56	23.64	19.34	17.58	15.74	14.04	12.56
BPOS =	3.56	1.91	1.03	.83	9.18	6.25	4.63	3.01	2.14	1.44	1.03	.81	.78
$\gamma_{\text{WT}} \Delta A$ =	80.00	80.00	102.50	77.50	20.00	10.00	5.00	0.00	80.00	80.00	102.50	77.50	77.50
BNEG	-3.53	-1.67	-1.18	-1.31	-11.09	-8.15	-5.19	-2.80	-1.89	-1.21	-1.20	-1.04	-1.27
THETA	= 335.00	332.50	327.50	357.50	0.00	0.00	0.00	35.00	332.50	330.00	327.50	327.50	357.50

VXBAR IS CIRCUMFERENTIAL MEAN LONGITUDINAL VELOCITY.
 VTBAR IS CIRCUMFERENTIAL MEAN TANGENTIAL VELOCITY.
 VRBAR IS CIRCUMFERENTIAL MEAN RADIAL VELOCITY.
 1-WVX IS VOLUMETRIC MEAN WAKE VELOCITY WITHOUT TANGENTIAL CORRECTION.
 1-NX IS VOLUMETRIC MEAN WAKE VELOCITY WITH TANGENTIAL CORRECTION.
 BBAR IS MEAN ANGLE OF ADVANCE.
 BPOS IS VARIATION BETWEEN THE MAXIMUM AND MEAN ADVANCE ANGLES (DELTA BETA PLUS).
 BNEG IS VARIATION BETWEEN THE MINIMUM AND MEAN ADVANCE ANGLES (DELTA BETA MINUS).
 THETA IS ANGLE IN DEGREES AT WHICH CORRESPONDING BPOS OR BNEG OCCURS.

TABLE C-3 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT II

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND W/O PR11
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)

HARMONIC	1	2	3	4	5	6	7	8
RADIUS = .456	.0233	.0307	.0115	.0167	.0152	.0116	.0061	.0018
AMPLITUDE =	283.6	283.5	282.2	283.3	288.8	298.0	305.6	303.8
PHASE ANGLE =								
RADIUS = .633	.0083	.0237	.0054	.0044	.0080	.0060	.0052	.0046
AMPLITUDE =	37.0	273.5	237.3	312.8	324.3	355.9	27.4	50.9
PHASE ANGLE =								
RADIUS = .781	.0036	.0178	.0075	.0061	.0069	.0031	.0024	.0013
AMPLITUDE =	196.3	276.8	294.9	311.8	290.3	339.8	347.7	272.1
PHASE ANGLE =								

RADIUS = .963	.0184	.0255	.0148	.0130	.0125	.0065	.0066	.0042
AMPLITUDE =	263.7	263.7	241.18	245.1	237.9	237.2	235.2	235.1
PHASE ANGLE =								

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)

HARMONIC	9	10	11	12	13	14	15	16
RADIUS = .456	.0020	.0035	.0037	.0041	.0027	.0007	.0023	.0041
AMPLITUDE =	156.6	128.6	136.1	159.1	156.7	235.5	274.0	305.2
PHASE ANGLE =								
RADIUS = .633	.0028	.0034	.0013	.0006	.0034	.0035	.0046	.0053
AMPLITUDE =	58.3	88.3	99.7	207.8	290.5	322.8	298.2	318.0
PHASE ANGLE =								
RADIUS = .781	.0007	.0018	.0013	.0026	.0024	.0018	.0009	.0012
AMPLITUDE =	299.5	91.4	263.7	283.8	261.8	332.6	313.0	175.5
PHASE ANGLE =								
RADIUS = .963	.0041	.0015	.0031	.0026	.0009	.0019	.0012	.0013
AMPLITUDE =	190.2	241.9	257.2	329.6	351.8	335.0	337.4	27.3
PHASE ANGLE =								

TABLE C-4 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 11

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND W/O PR11 PROPELLER DIAMETER = 6.00 FEET									
JA = .739									
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	1	2	3	4	5	6	7	8	
RADIUS = .312									
AMPLITUDE =	.0732	.0472	.0416	.0372	.0317	.0267	.0202	.0148	
PHASE ANGLE =	265.3	287.5	279.6	279.3	266.9	273.2	269.8	252.2	
RADIUS = .350									
AMPLITUDE =	.0573	.0436	.0364	.0322	.0263	.0217	.0155	.0104	
PHASE ANGLE =	267.9	286.5	280.0	279.9	271.1	277.5	274.4	255.0	
RADIUS = .400									
AMPLITUDE =	.0393	.0392	.0278	.0242	.0203	.0163	.0104	.0055	
PHASE ANGLE =	273.1	285.1	250.8	261.0	278.1	285.2	284.2	263.4	
RADIUS = .500									
AMPLITUDE =	.0141	.0316	.0142	.0100	.0123	.0090	.0048	.0023	
PHASE ANGLE =	300.1	282.2	234.1	286.5	299.0	311.9	333.5	24.1	
RADIUS = .600									
AMPLITUDE =	.0079	.0254	.0056	.0053	.0087	.0064	.0051	.0047	
PHASE ANGLE =	19.9	279.3	293.1	303.7	320.7	347.6	21.8	49.7	
RADIUS = .700									
AMPLITUDE =	.0033	.0158	.0041	.0016	.0073	.0049	.0021	.0018	
PHASE ANGLE =	75.5	279.2	304.5	323.3	313.2	355.3	17.1	34.7	
RADIUS = .800									
AMPLITUDE =	.0046	.0178	.0071	.0042	.0070	.0027	.0021	.0017	
PHASE ANGLE =	209.9	275.7	290.7	305.9	283.7	330.5	333.1	261.1	
RADIUS = .900									
AMPLITUDE =	.0118	.0209	.0101	.0041	.0094	.0036	.0034	.0031	
PHASE ANGLE =	249.0	211.0	210.3	214.3	251.4	254.4	250.4	241.9	
RADIUS = 1.000									
AMPLITUDE =	.0184	.0255	.0143	.0130	.0125	.0065	.0060	.0042	
PHASE ANGLE =	263.7	263.7	243.8	245.5	237.9	237.2	235.2	235.1	

TABLE C-4 (Continued)

VELOCITY COMPONENT RATIOS FOR MATELLES WITH BASS BOAT SIZING W/O PRIM
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (Vx/V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .312									
AMPLITUDE = .0094		.00660	.0053	.0049	.0044	.0039	.0034	.0029	.0024
PHASE ANGLE = 209.5		179.6	166.5	159.5	152.5	146.5	138.8	130.5	123.7
RADIUS = .350									
AMPLITUDE = .0068		.00449	.00410	.00372	.00328	.00272	.00218	.00162	.00102
PHASE ANGLE = 204.7		169.1	159.0	152.5	146.3	140.2	134.8	129.3	123.7
RADIUS = .400									
AMPLITUDE = .0040		.00340	.00310	.00275	.00240	.00205	.00170	.00135	.00100
PHASE ANGLE = 192.7		151.1	149.0	141.3	134.8	128.6	122.3	116.0	109.7
RADIUS = .500									
AMPLITUDE = .0018		.00135	.00127	.00103	.00089	.00074	.00060	.00046	.00032
PHASE ANGLE = 107.3		113.2	125.0	158.1	172.6	186.6	200.1	213.6	227.1
RADIUS = .600									
AMPLITUDE = .0028		.00235	.00177	.00110	.00060	.00030	.00015	.00007	.00003
PHASE ANGLE = 63.7		91.9	105.3	119.0	132.6	146.1	159.6	172.1	184.6
RADIUS = .700									
AMPLITUDE = .0014		.00128	.00111	.00091	.00070	.00050	.00033	.00017	.00007
PHASE ANGLE = 30.0		83.3	106.3	129.1	152.0	174.0	196.9	219.8	242.7
RADIUS = .800									
AMPLITUDE = .0008		.00115	.00095	.00077	.00060	.00043	.00025	.00012	.00005
PHASE ANGLE = 272.5		293.3	263.8	234.3	205.8	177.3	148.8	120.3	91.8
RADIUS = .900									
AMPLITUDE = .0024		.00204	.00171	.00140	.00110	.00080	.00050	.00020	.00008
PHASE ANGLE = 207.5		194.4	181.3	168.2	155.1	142.0	128.9	115.8	102.7
RADIUS = 1.000									
AMPLITUDE = .0041		.00315	.00271	.00226	.00181	.00136	.00091	.00046	.00019
PHASE ANGLE = 190.2		241.9	257.2	272.5	287.8	303.1	318.4	333.7	349.0

TABLE C-5 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 11

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND W/D PR11
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VR/V)

HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .456									
AMPLITUDE =	.2175	.0025	.0019	.0013	.0022	.0041	.0012	.0008	
PHASE ANGLE =	187.3	305.7	205.8	204.7	186.1	205.1	207.7	214.4	
RADIUS = .633									
AMPLITUDE =	.1986	.0140	.0070	.0051	.0062	.0041	.0049	.0045	
PHASE ANGLE =	190.1	305.5	301.5	307.0	314.3	313.2	317.4	331.0	
RADIUS = .781									
AMPLITUDE =	.1884	.0100	.0054	.0034	.0021	.0016	.0015	.0014	
PHASE ANGLE =	187.5	322.6	352.0	314.2	315.0	298.9	326.2	323.2	
RADIUS = .963									
AMPLITUDE =	.1799	.0077	.0033	.0029	.0036	.0031	.0029	.0025	
PHASE ANGLE =	185.7	325.9	25.0	87.7	119.5	123.6	135.3	157.1	
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .456									
AMPLITUDE =	.0019	.0023	.0032	.0025	.0027	.0015	.0017	.0018	
PHASE ANGLE =	46.2	47.7	63.1	63.2	84.5	100.0	147.5	199.2	
RADIUS = .633									
AMPLITUDE =	.0030	.0034	.0013	.0005	.0016	.0024	.0031	.0028	
PHASE ANGLE =	339.4	331.7	15.6	279.1	168.0	193.6	186.5	193.4	
RADIUS = .781									
AMPLITUDE =	.0004	.0004	.0006	.0021	.0020	.0022	.0017	.0008	
PHASE ANGLE =	124.2	181.7	150.1	190.1	191.4	192.0	201.7	196.5	
RADIUS = .963									
AMPLITUDE =	.0025	.0018	.0024	.0023	.0016	.0016	.0009	.0008	
PHASE ANGLE =	175.3	194.1	202.7	221.8	236.2	252.5	313.0	336.9	

LE C-6 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED
RADII FOR EXPERIMENT 11

VELOCITY COMPONENT RATIOS FOR MODEL SIZES WITH BASS BOAT BEHIND W/O PR11
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)

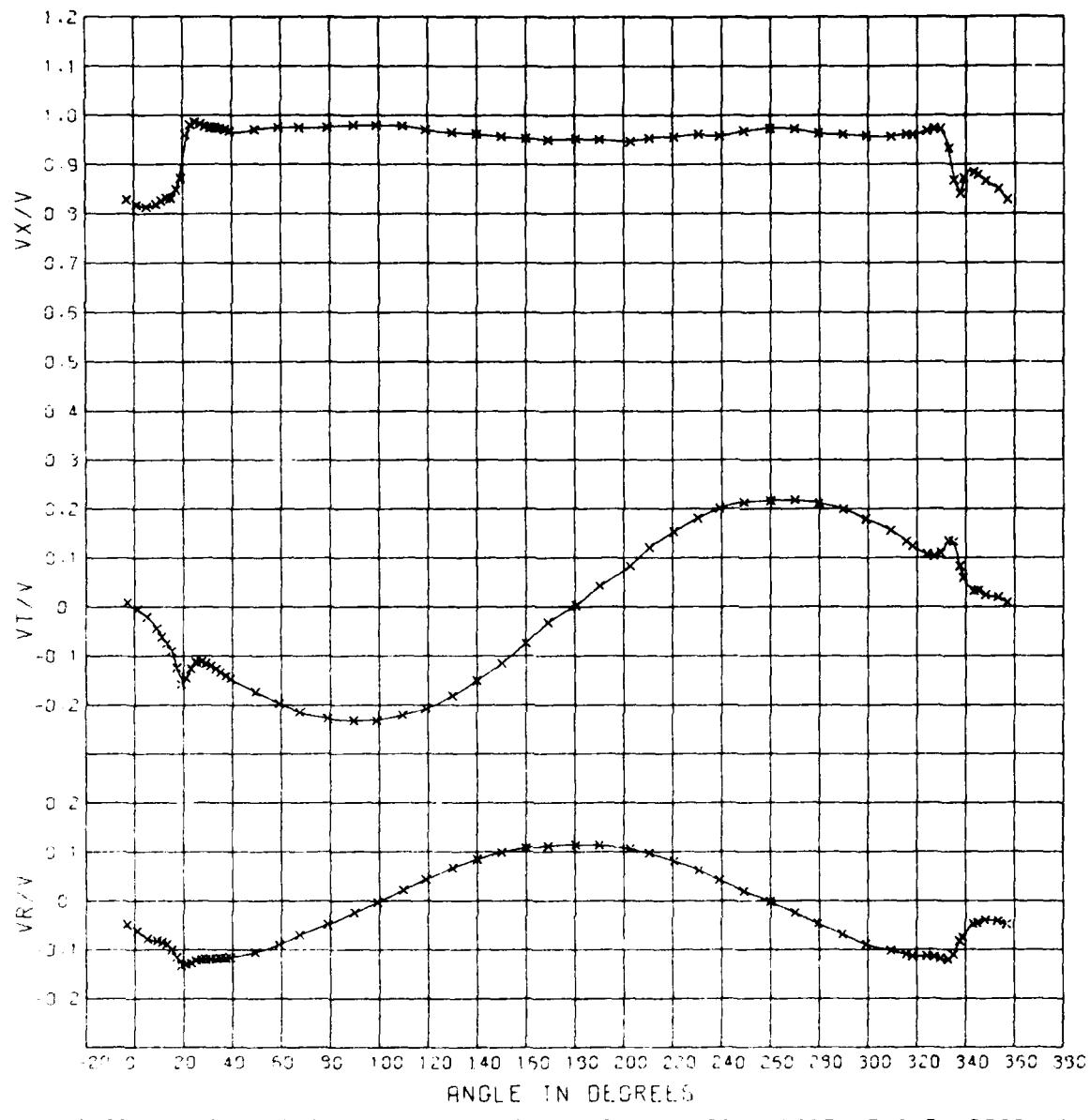
HARMONIC	1	2	3	4	5	6	7	8
RADIUS = .312								
AMPLITUDE =	.240.1	.0205	.0170	.0144	.0110	.0125	.0116	
PHASE ANGLE =	181.5	114.4	135.2	164.9	149.0	171.7	150.4	161.7
RADIUS = .350								
AMPLITUDE =	.2335	.0132	.0113	.0146	.0129	.0127	.0118	.0100
PHASE ANGLE =	183.2	110.4	133.1	163.0	151.0	175.1	152.8	163.3
RADIUS = .400								
AMPLITUDE =	.2254	.0050	.0011	.0012	.0071	.0080	.0045	.0041
PHASE ANGLE =	185.3	116.5	147.1	178.1	155.7	103.1	159.3	163.2
RADIUS = .500								
AMPLITUDE =	.2120	.0071	.0033	.0039	.0021	.0027	.0020	.0018
PHASE ANGLE =	188.5	303.6	279.8	247.4	281.0	246.7	294.4	316.0
RADIUS = .600								
AMPLITUDE =	.2015	.0133	.0074	.0057	.0058	.0041	.0047	.0043
PHASE ANGLE =	190.1	305.3	303.2	301.5	312.4	308.2	315.7	330.2
RADIUS = .700								
AMPLITUDE =	.1936	.0119	.0067	.0051	.0044	.0032	.0034	.0031
PHASE ANGLE =	188.9	314.2	317.1	308.3	313.4	307.8	319.8	329.2
RADIUS = .800								
AMPLITUDE =	.1873	.0097	.0061	.0010	.0016	.0012	.0011	.0010
PHASE ANGLE =	187.3	324.2	356.0	317.2	317.1	294.9	330.2	319.1
RADIUS = .900								
AMPLITUDE =	.1824	.0083	.0034	.0012	.0016	.0013	.0013	.0012
PHASE ANGLE =	186.1	329.3	17.0	316.4	115.2	132.0	128.9	163.6
RADIUS = 1.000								
AMPLITUDE =	.1799	.0077	.0033	.0024	.0036	.0031	.0029	.0025
PHASE ANGLE =	185.7	325.9	25.0	87.7	119.5	123.6	135.3	157.1

TABLE C-6 (Continued)

VELOCITY COMPONENT RATIOS FOR MODEL 5265 WITH BASS BOAT BEHIND W/C P411
PROPELLER DIAMETER = 6.00 FEET
JA = .339

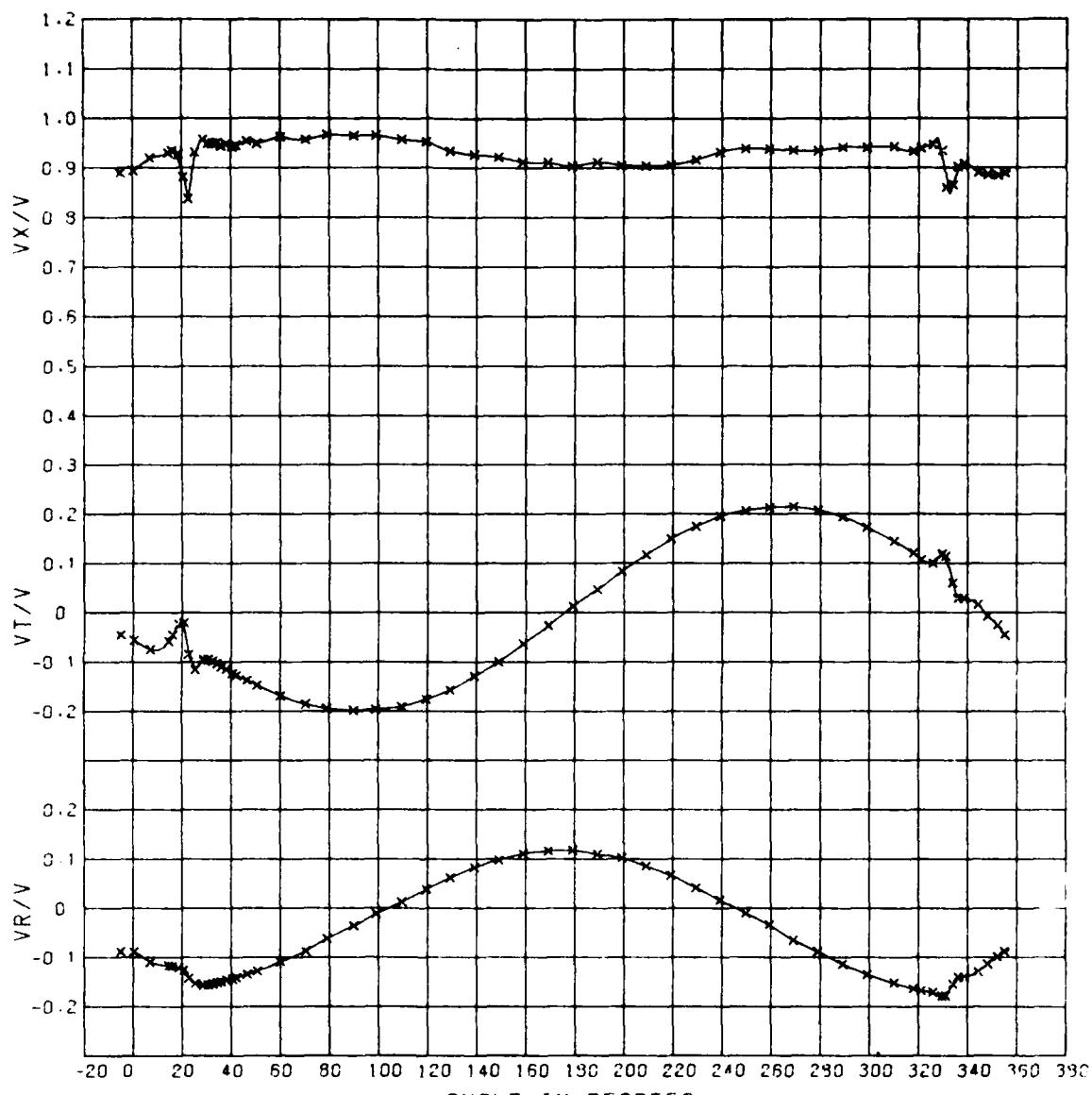
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)							
HARMONIC	=	9	10	11	12	13	14
RADIUS = .312							
AMPLITUDE =	.0077	.0095	.0011	.0060	.0060	.0038	.0017
PHASE ANGLE =	121.8	114.8	88.7	83.4	65.0	56.7	46.6
RADIUS = .350							
AMPLITUDE =	.0054	.0068	.0057	.0011	.0054	.0045	.0026
PHASE ANGLE =	115.1	108.3	83.7	78.7	68.0	60.9	59.7
RADIUS = .400							
AMPLITUDE =	.0030	.0040	.0013	.0040	.0040	.0016	.0007
PHASE ANGLE =	96.6	81.8	75.3	73.4	73.7	71.2	96.6
RADIUS = .500							
AMPLITUDE =	.0022	.0025	.0025	.0013	.0020	.0013	.0024
PHASE ANGLE =	8.8	2.3	51.4	50.2	39.0	342.8	166.8
RADIUS = .600							
AMPLITUDE =	.0031	.0035	.0013	.0005	.0015	.0022	.0031
PHASE ANGLE =	342.3	335.9	23.2	328.7	153.6	189.5	163.5
RADIUS = .700							
AMPLITUDE =	.0013	.0014	.0006	.0012	.0019	.0025	.0018
PHASE ANGLE =	348.9	330.7	46.0	195.6	179.9	169.7	191.6
RADIUS = .800							
AMPLITUDE =	.0007	.0007	.0007	.0007	.0020	.0021	.0015
PHASE ANGLE =	142.3	174.6	162.7	146.4	194.2	193.8	205.4
RADIUS = .900							
AMPLITUDE =	.00020	.00117	.00117	.00117	.0018	.0016	.0007
PHASE ANGLE =	165.8	172.9	192.2	202.7	24.3	216.5	256.1
RADIUS = 1.000							
AMPLITUDE =	.0025	.0018	.0024	.0023	.0016	.0016	.0008
PHASE ANGLE =	175.3	194.1	202.7	221.8	252.5	313.0	356.9

APPENDIX D
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENT 12



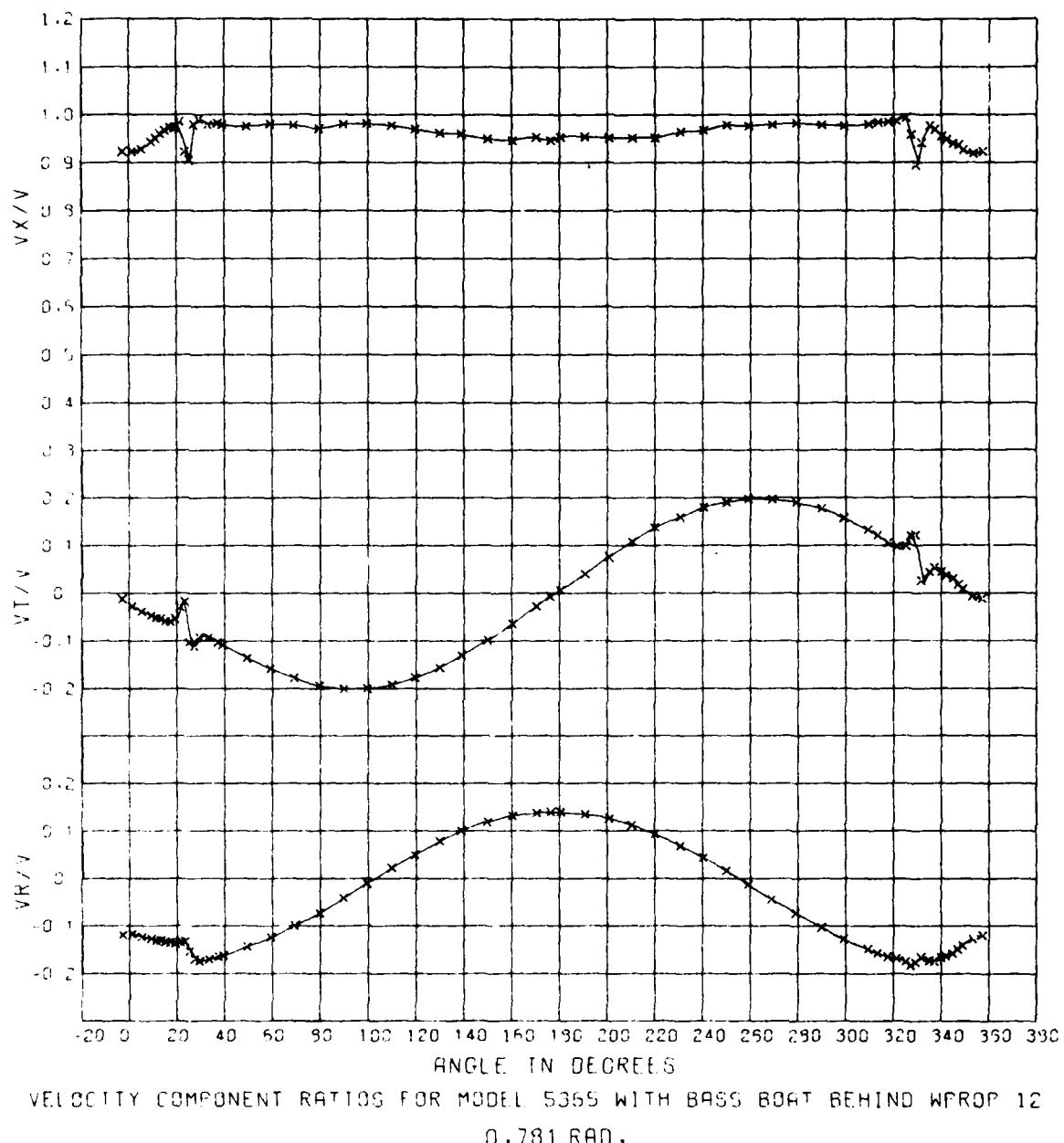
VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12
0.456 RAD.

Figure D-1 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.456
for Experiment 12



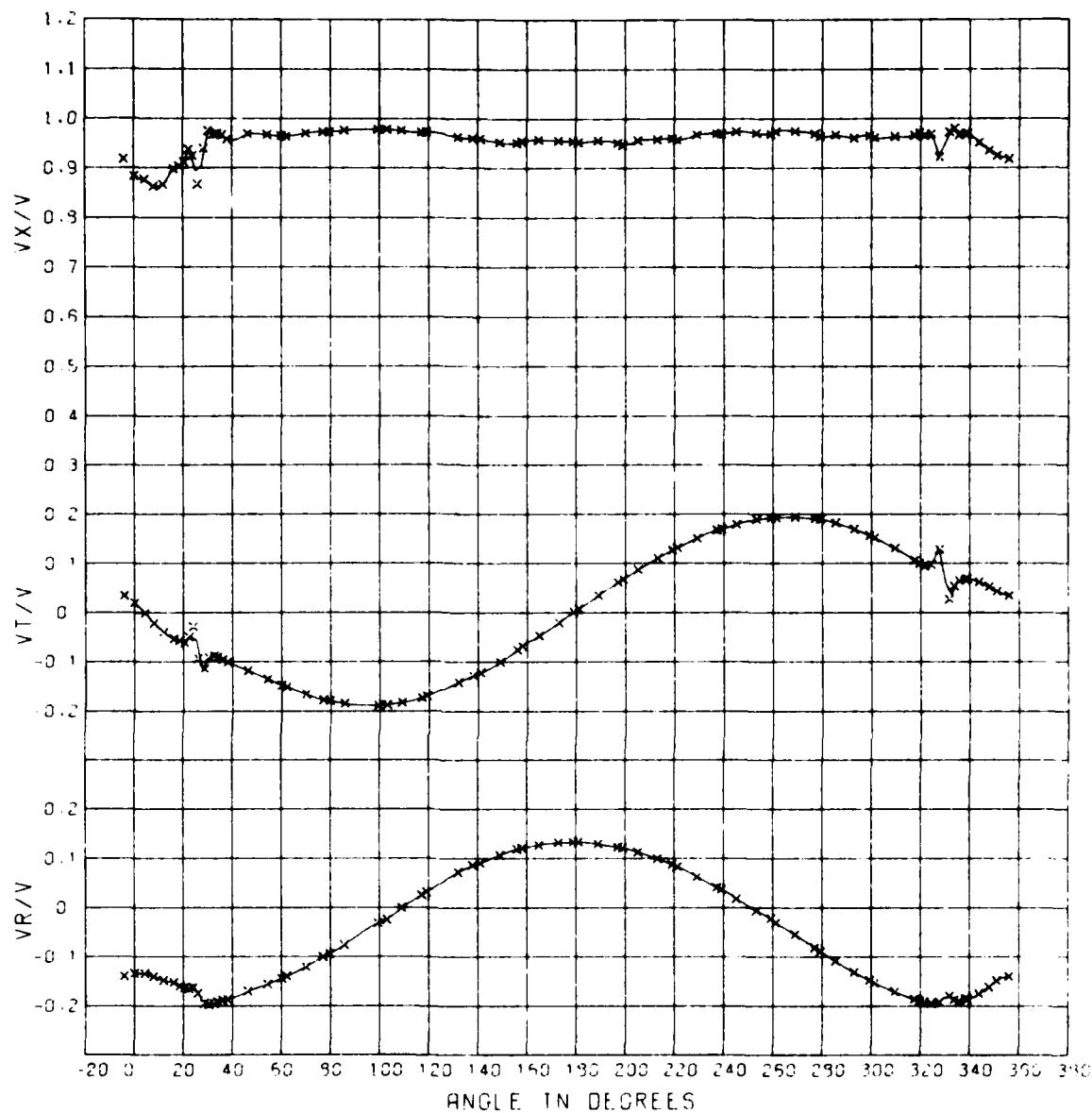
VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12
0.633 RAD.

Figure D-2 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.633
for Experiment 12



VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12
0.781 RAD.

Figure D-3 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.781
for Experiment 12



VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12
0.963 RAD.

Figure D-4 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.963
for Experiment 12

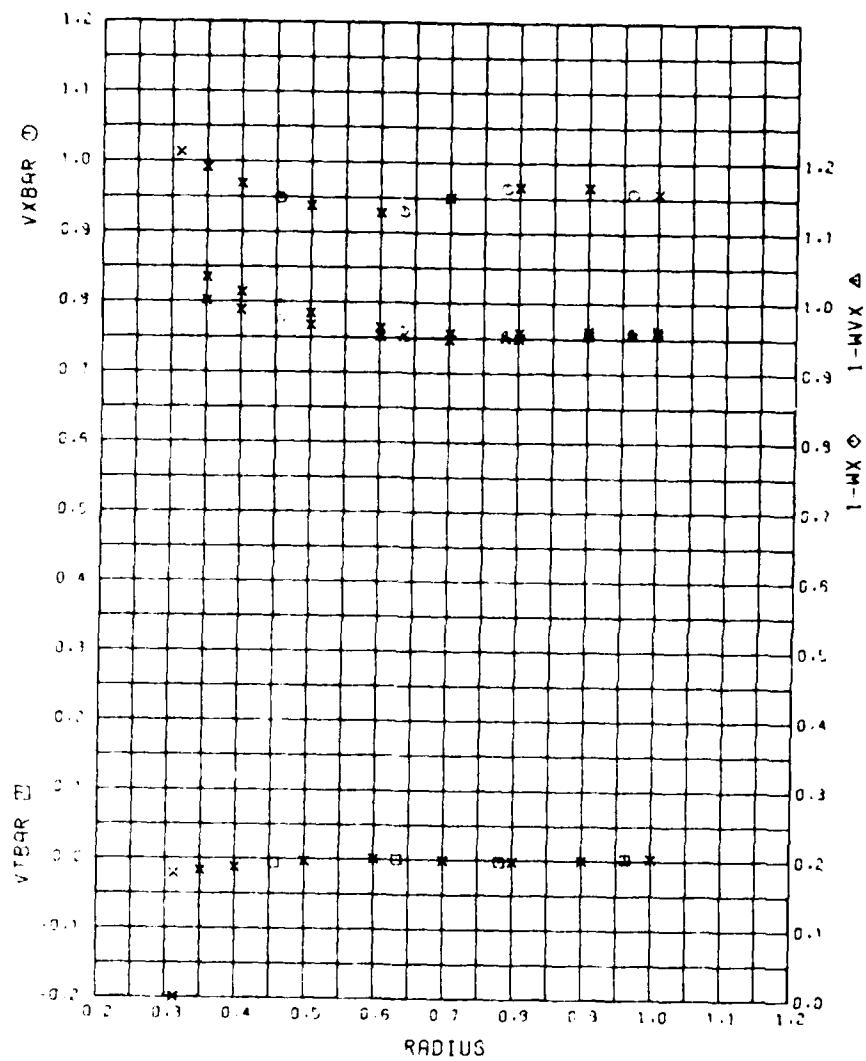


Figure D-5 - Radial Distribution of the Mean Velocity Component Ratios
for Experiment 12

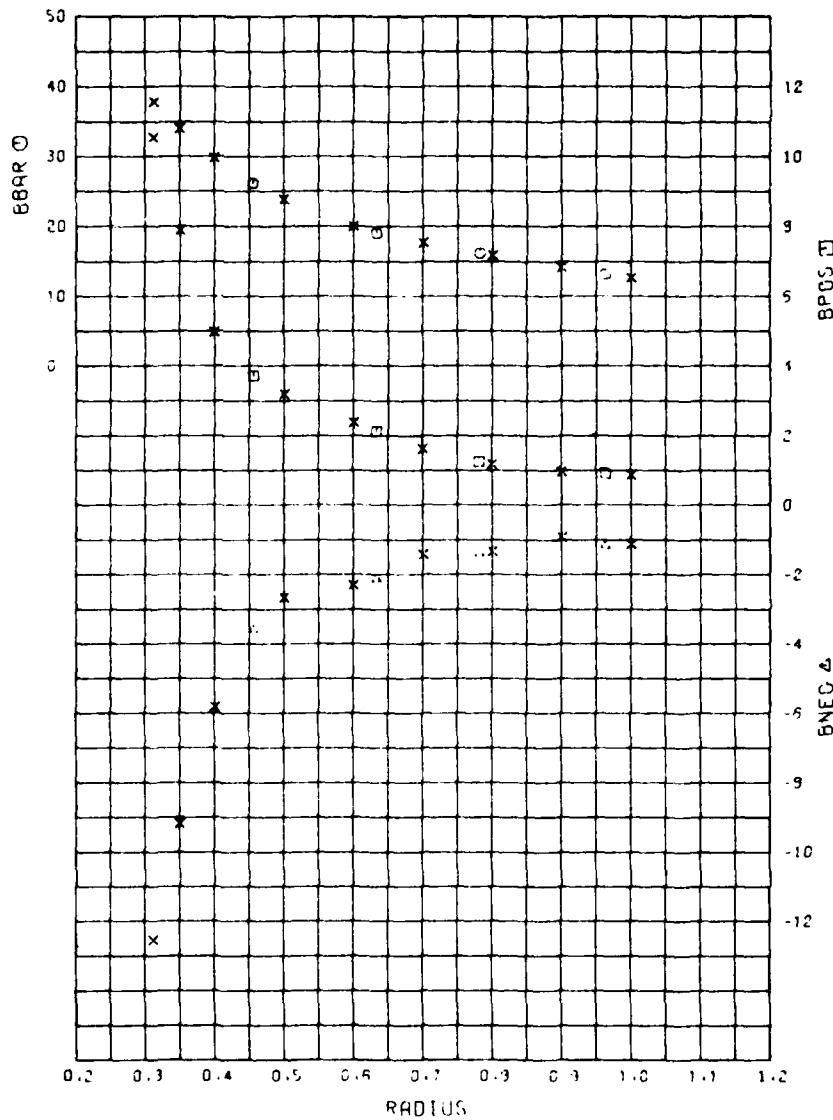


Figure D-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 12

TABLE D-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 12

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12
PROPELLER DIAMETER = 6.00 FEET $\Delta A = .739$

RADIUS = .456	.633	.781	.963	.312	.350	.400	.500	.600	.700	.800	.900	1.000
VXBAR = .949	.930	.964	.957	1.013	.992	.969	.938	.928	.950	.966	.966	.957
VTBAR = -.006	.001	-.002	.003	-.022	-.017	-.012	-.003	-.001	-.001	-.002	-.000	.003
VRBAR = -.009	-.033	-.027	-.043	.035	.021	.005	-.018	-.031	-.029	-.028	-.035	-.043
1-WVX = .975	.949	.948	.954	0.000	1.002	.988	.967	.952	.947	.950	.954	.956
1-WX = .997	.960	.955	.959	0.000	1.035	1.014	.934	.964	.956	.958	.960	.961
BBAR = 26.15	19.05	16.20	13.14	37.82	33.29	29.92	24.84	19.99	17.71	15.86	14.16	12.67
BPOS θ = 3.71	2.14	1.25	.92	10.55	7.89	4.97	3.19	2.38	1.63	1.18	.96	.87
THETA = 92.50	82.50	95.00	102.50	20.00	22.50	22.50	22.50	82.50	95.00	95.00	97.50	102.50
BNEG θ = -3.59	-2.13	-1.40	-1.17	-12.54	-9.19	-5.82	-2.67	-2.31	-1.42	-1.34	-1.92	-1.13
THETA = 337.50	332.50	330.00	7.50	5.00	5.00	335.00	332.50	330.00	330.00	327.50	327.50	7.50

101

VXBAR IS CIRCUMFERNENTIAL MEAN LONGITUDINAL VELOCITY.
 VTBAR IS CIRCUMFERNENTIAL MEAN TANGENTIAL VELOCITY.
 VRBAR IS CIRCUMFERNENTIAL MEAN RADIAL VELOCITY.
 1-WVX IS VOLUMETRIC MEAN WAKE VELOCITY WITHOUT TANGENTIAL CORRECTION.
 1-WX IS VOLUMETRIC MEAN WAKE VELOCITY WITH TANGENTIAL CORRECTION.
 BBAR IS MEAN ANGLE OF ADVANCE.
 BPOS IS VARIATION BETWEEN THE MAXIMUM AND MEAN ADVANCE ANGLES ($\Delta\delta$ DELTA BETA PLUS).
 BNEG IS VARIATION BETWEEN THE MINIMUM AND MEAN ADVANCE ANGLES ($\Delta\beta$ DELTA BETA MINUS).
 THETA IS ANGLE IN DEGREES AT WHICH CORRESPONDING BPOS OR BNEG OCCURS.

TABLE D-3 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 12

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12
PROPELLER DIAMETER = 6.00 FEET
JA = .739

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)

HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .456		.0247	.0352	.0210	.0181	.0171	.0121	.0064	.0039
AMPLITUDE =		285.3	274.5	276.0	273.2	271.1	269.3	263.1	214.0
PHASE ANGLE =									
RADIUS = .633		.0132	.0254	.0061	.0039	.0061	.0034	.0023	.0021
AMPLITUDE =		16.3	271.1	280.1	300.8	303.7	22.8	91.3	32.0
PHASE ANGLE =									
RADIUS = .781		.0025	.0177	.0070	.0054	.0072	.0025	.0014	.0018
AMPLITUDE =		87.3	272.0	284.1	302.6	279.1	312.4	308.4	346.4
PHASE ANGLE =									
RADIUS = .963		.0123	.0217	.0101	.0097	.0106	.0077	.0056	.0046
AMPLITUDE =		268.4	261.6	232.3	228.6	236.1	213.3	214.1	192.1
PHASE ANGLE =									
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .456		.0054	.0061	.0076	.0067	.0048	.0022	.0004	.0019
AMPLITUDE =		191.3	151.6	150.6	148.9	147.1	147.5	209.0	333.7
PHASE ANGLE =									
RADIUS = .633		.0032	.0023	.0010	.0009	.0021	.0039	.0036	.0045
AMPLITUDE =		73.7	56.3	67.6	5.8	326.9	304.7	307.0	294.8
PHASE ANGLE =									
RADIUS = .781		.0009	.0013	.0012	.0029	.0031	.0032	.0015	.0011
AMPLITUDE =		261.2	216.8	282.3	300.4	315.0	306.3	301.4	357.0
PHASE ANGLE =									
RADIUS = .963		.0028	.0024	.0005	.0001	.0004	.0011	.0013	.0006
AMPLITUDE =		193.3	211.3	247.2	221.6	216.9	339.8	69.5	68.4
PHASE ANGLE =									

TABLE D-4 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 12

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12 PROPELLER DIAMETER = 6.00 FEET JA = .739									
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .312									
AMPLITUDE = .0712		.0440	.0458	.0430	.0390	.0373	.0236	.0146	
PHASE ANGLE = 257.5		278.5	275.8	270.4	260.0	259.6	267.4	218.2	
RADIUS = .350									
AMPLITUDE = .0560		.0416	.0382	.0353	.0321	.0294	.0182	.0112	
PHASE ANGLE = 261.7		277.4	275.8	270.8	262.0	260.9	266.8	217.5	
RADIUS = .400									
AMPLITUDE = .0391		.0385	.0293	.0264	.0242	.0203	.0120	.0074	
PHASE ANGLE = 269.7		276.0	275.9	271.6	265.4	263.5	265.6	216.2	
RADIUS = .500									
AMPLITUDE = .0174		.0327	.0156	.0128	.0127	.0071	.0030	.0017	
PHASE ANGLE = 306.0		273.4	276.3	275.6	277.6	279.3	257.8	209.6	
RADIUS = .600									
AMPLITUDE = .0133		.0271	.0076	.0051	.0070	.0029	.0018	.0016	
PHASE ANGLE = 4.2		271.5	278.6	290.8	298.3	4.5	97.1	36.0	
RADIUS = .700									
AMPLITUDE = .0071		.0207	.0067	.0051	.0067	.0031	.0011	.0023	
PHASE ANGLE = 37.8		272.5	288.6	311.6	294.5	354.8	32.3	7.6	
RADIUS = .800									
AMPLITUDE = .0018		.0174	.0070	.0054	.0073	.0025	.0015	.0015	
PHASE ANGLE = 113.3		271.4	280.9	297.4	274.9	298.4	293.7	338.6	
RADIUS = .900									
AMPLITUDE = .0059		.0186	.0079	.0065	.0088	.0046	.0033	.0018	
PHASE ANGLE = 249.6		266.7	252.6	253.0	250.5	232.1	234.3	211.0	
RADIUS = 1.000									
AMPLITUDE = .0123		.0217	.0101	.0097	.0106	.0077	.0056	.0046	
PHASE ANGLE = 268.4		261.6	232.3	228.6	236.1	213.3	214.1	192.1	

TABLE D-4 (Continued)

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPRODP 12
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)							
HARMONIC	=	9	10	11	12	13	14
RADIUS = .312		.0199	.0184	.0190	.0171	.0152	.0123
AMPLITUDE =		215.4	174.5	161.3	158.0	149.4	134.6
PHASE ANGLE =							.0080
RADIUS = .350		.0151	.0144	.0155	.0140	.0091	.0055
AMPLITUDE =		212.5	171.1	159.4	156.3	149.0	.0054
PHASE ANGLE =							.0083
RADIUS = .400		.0099	.0099	.0114	.0102	.0084	.0055
AMPLITUDE =		206.2	164.6	156.1	153.4	148.3	.0027
PHASE ANGLE =							.0025
RADIUS = .500		.0031	.0040	.0051	.0043	.0025	.0015
AMPLITUDE =		163.6	133.4	143.9	143.2	145.5	.0031
PHASE ANGLE =							.54.8
RADIUS = .600		.0031	.0025	.0015	.0007	.0013	.0034
AMPLITUDE =		83.2	70.0	102.1	76.1	329.6	.0046
PHASE ANGLE =							.295.3
RADIUS = .700		.0010	.0005	.0005	.0021	.0029	.0026
AMPLITUDE =		56.3	78.6	320.8	310.8	319.4	.0024
PHASE ANGLE =							.308.7
RADIUS = .800		.0012	.0015	.0013	.0029	.0030	.0013
AMPLITUDE =		253.1	218.2	279.9	299.2	314.1	.0010
PHASE ANGLE =							.13.6
RADIUS = .900		.0022	.0024	.0011	.0018	.0016	.0005
AMPLITUDE =		219.1	216.7	270.0	294.1	304.9	.0010
PHASE ANGLE =							.61.3
RADIUS = 1.000		.0028	.0024	.0005	.0001	.0004	.0013
AMPLITUDE =		193.3	211.3	247.2	221.6	216.9	.0006
PHASE ANGLE =							.68.4

TABLE D-5 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL
RADII FOR EXPERIMENT 12

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12									
PROPELLER DIAMETER = 6.00 FEET $JA = .739$									
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
HARMONIC	1	2	3	4	5	6	7	8	9
RADIUS = .456									
AMPLITUDE =	.2264	.0041	.0017	.0055	.0019	.0046	.0014	.0020	
PHASE ANGLE =	182.3	7.8	197.5	182.4	181.9	167.6	152.7	99.5	
RADIUS = .633									
AMPLITUDE =	.2044	.0141	.0055	.0061	.0060	.0049	.0045	.0032	
PHASE ANGLE =	184.9	319.9	298.6	293.4	296.9	286.6	298.6	309.8	
RADIUS = .781									
AMPLITUDE =	.1937	.0122	.0065	.0029	.0017	.0015	.0013	.0008	
PHASE ANGLE =	182.4	349.8	329.2	288.7	296.7	267.8	302.0	287.4	
RADIUS = .963									
AMPLITUDE =	.1865	.0096	.0028	.0033	.0041	.0033	.0021	.0018	
PHASE ANGLE =	180.0	6.5	17.4	124.8	132.7	132.8	139.3	132.5	
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
HARMONIC	9	10	11	12	13	14	15	16	17
RADIUS = .456									
AMPLITUDE =	.0033	.0038	.0050	.0051	.0047	.0030	.0019	.0009	
PHASE ANGLE =	49.3	54.7	47.1	50.3	63.5	50.9	81.0	233.6	
RADIUS = .633									
AMPLITUDE =	.0027	.0015	.0012	.0015	.0023	.0030	.0032	.0029	
PHASE ANGLE =	308.1	292.4	265.3	211.8	203.8	199.1	198.4	198.1	
RADIUS = .781									
AMPLITUDE =	.0010	.0004	.0006	.0013	.0014	.0017	.0010	.0006	
PHASE ANGLE =	306.9	191.2	204.1	192.5	198.1	214.2	194.7	202.9	
RADIUS = .963									
AMPLITUDE =	.0010	.0012	.0010	.0013	.0007	.0009	.0002		
PHASE ANGLE =	119.2	169.4	152.8	203.8	197.8	205.4	235.4	357.8	

TABLE D-6 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 12

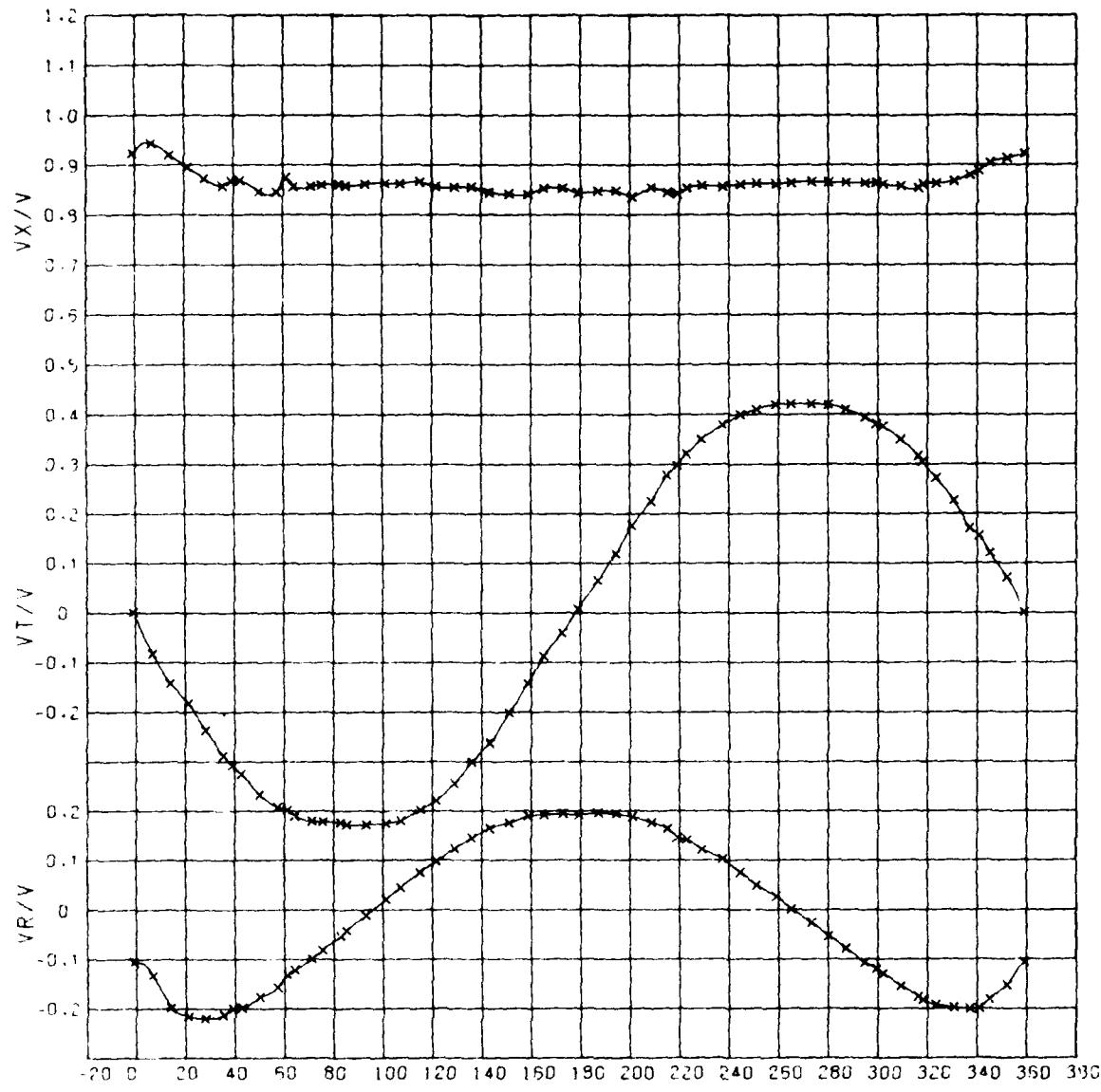
VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND *PROP 12 DISSECTOR DIAMETER = 6.00 FEET JA = .739							
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)							
HARMONIC	1	2	3	4	5	6	7
RADIUS = .312							
AMPLITUDE =	.2533	.0234	.0174	.0226	.0167	.0203	.0134
PHASE ANGLE =	176.9	103.7	122.1	150.4	133.0	139.3	126.6
RADIUS = .350							
AMPLITUDE =	.2453	.0159	.0121	.0170	.0118	.0152	.0095
PHASE ANGLE =	178.6	99.6	125.1	153.6	135.4	142.1	128.0
RADIUS = .400							
AMPLITUDE =	.2358	.0077	.0061	.0107	.0063	.0095	.0052
PHASE ANGLE =	180.5	84.2	134.8	161.2	142.4	148.6	131.5
RADIUS = .500							
AMPLITUDE =	.2200	.0072	.0034	.0035	.0024	.0026	.0013
PHASE ANGLE =	183.5	323.7	273.6	224.3	268.4	211.7	276.6
RADIUS = .600							
AMPLITUDE =	.2078	.0132	.0079	.0056	.0058	.0045	.0042
PHASE ANGLE =	184.9	318.6	295.0	258.2	295.1	281.9	297.5
RADIUS = .700							
AMPLITUDE =	.1990	.0129	.0075	.0048	.0041	.0033	.0030
PHASE ANGLE =	183.8	334.9	313.2	292.3	298.2	283.5	300.9
RADIUS = .800							
AMPLITUDE =	.1926	.0121	.0062	.0024	.0012	.0011	.0006
PHASE ANGLE =	182.1	352.6	332.7	286.3	293.7	256.1	301.0
RADIUS = .900							
AMPLITUDE =	.1883	.0109	.0043	.0010	.0020	.0018	.0010
PHASE ANGLE =	180.7	3.2	353.4	143.0	134.0	143.1	139.5
RADIUS = 1.000							
AMPLITUDE =	.1865	.0096	.0028	.0033	.0041	.0033	.0021
PHASE ANGLE =	180.0	6.5	17.4	124.8	132.7	139.3	132.5

TABLE D-6 (Continued)

VELOCITY COMPONENT RATIOS FOR MODEL 5365 WITH BASS BOAT BEHIND WPROP 12
 PROPELLER DIAMETER = 6.00 FEET JA = .739

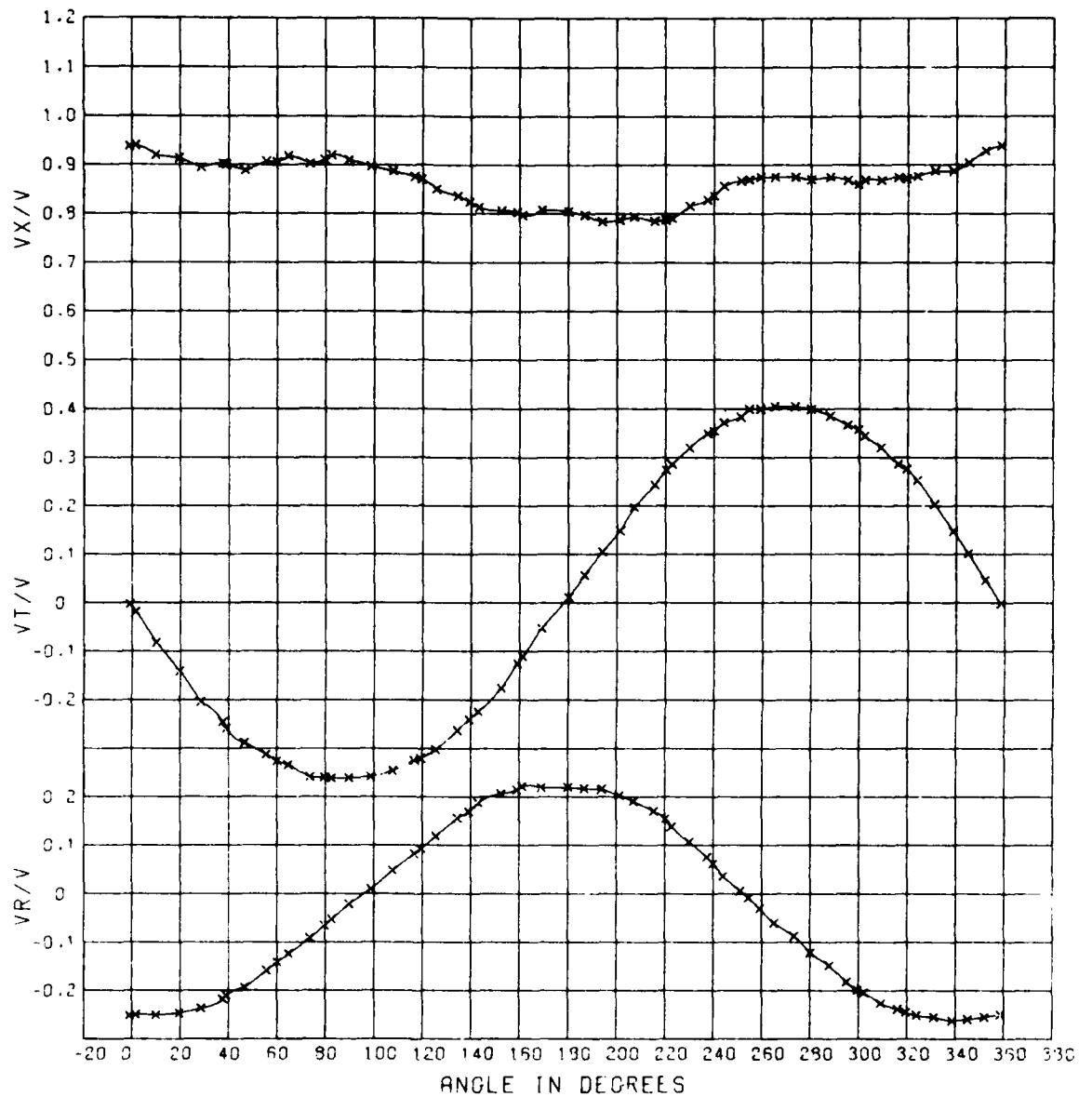
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)						
HARMONIC	=	9	10	11	12	13
RADIUS = .312						
AMPLITUDE = .0115		.0124	.0150	.0159	.0163	.0132
PHASE ANGLE = 80.3		71.7	55.3	48.9	53.4	35.3
RADIUS = .350						
AMPLITUDE = .0088		.0097	.0119	.0126	.0127	.0100
PHASE ANGLE = 76.5		69.3	55.1	49.0	54.6	36.9
RADIUS = .400						
AMPLITUDE = .0058		.0066	.0083	.0097	.0085	.0063
PHASE ANGLE = 68.4		64.6	51.7	49.3	57.2	40.5
RADIUS = .500						
AMPLITUDE = .0023		.0022	.0029	.0023	.0024	.0012
PHASE ANGLE = 18.8		37.9	39.5	52.8	77.2	86.3
RADIUS = .600						
AMPLITUDE = .0026		.0014	.0008	.0008	.0018	.0025
PHASE ANGLE = 315.7		308.4	291.6	203.2	194.2	194.4
RADIUS = .700						
AMPLITUDE = .0020		.0007	.0018	.0014	.0018	.0023
PHASE ANGLE = 307.3		275.5	246.0	200.4	201.3	206.2
RADIUS = .800						
AMPLITUDE = .0008		.0005	.0007	.0013	.0016	.0008
PHASE ANGLE = 307.1		178.4	194.0	191.6	197.5	215.8
RADIUS = .900						
AMPLITUDE = .0003		.0009	.0009	.0011	.0012	.0010
PHASE ANGLE = 115.3		163.3	161.3	153.9	196.3	217.7
RADIUS = 1.000						
AMPLITUDE = .0010		.0012	.0010	.0013	.0007	.0009
PHASE ANGLE = 119.2		167.4	152.8	203.8	197.8	205.4

APPENDIX E
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENT 13



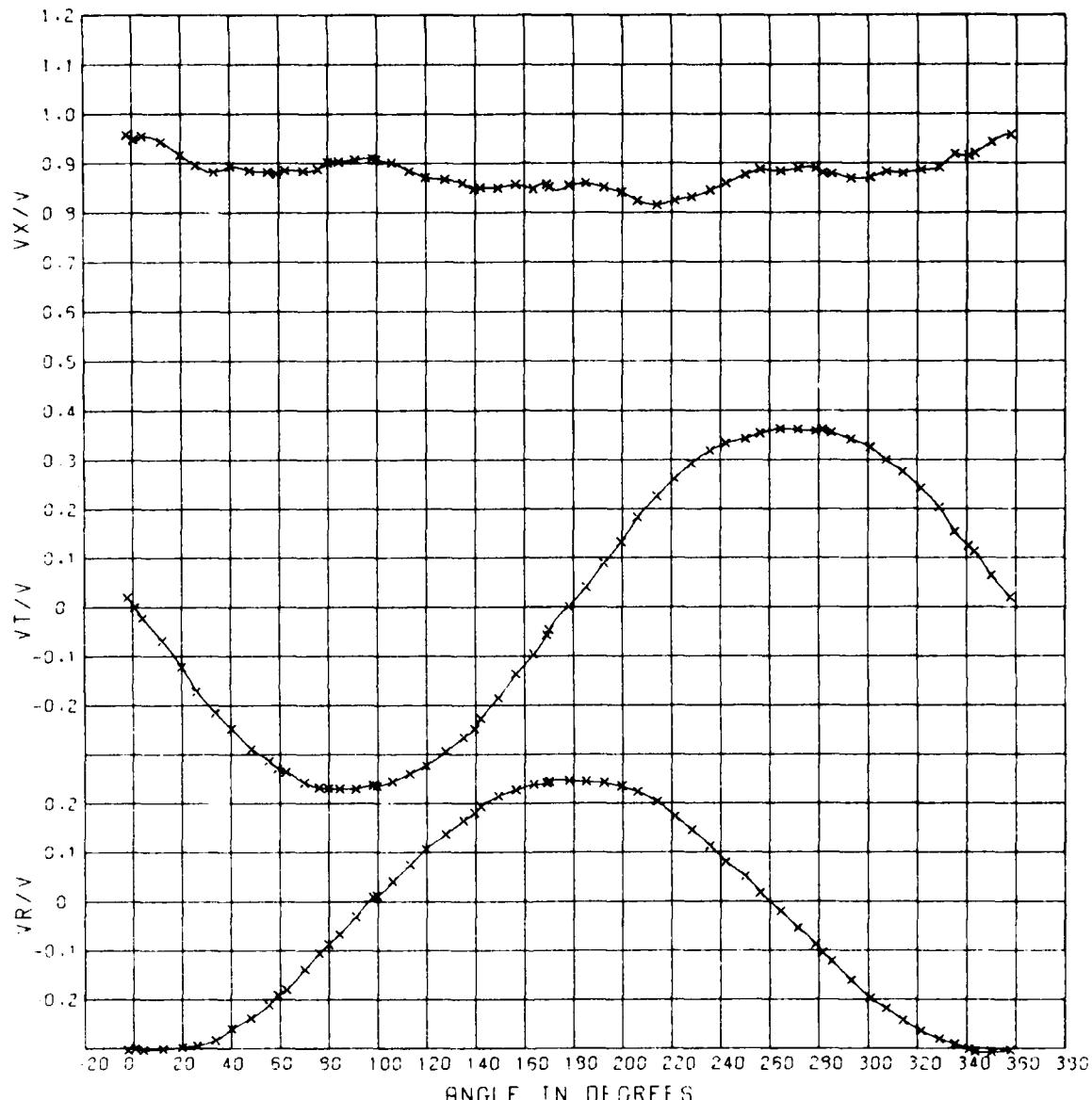
VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ALONE 200 INC 4KTS13
0.456 RAD.

Figure E-1 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.456 for Experiment 13



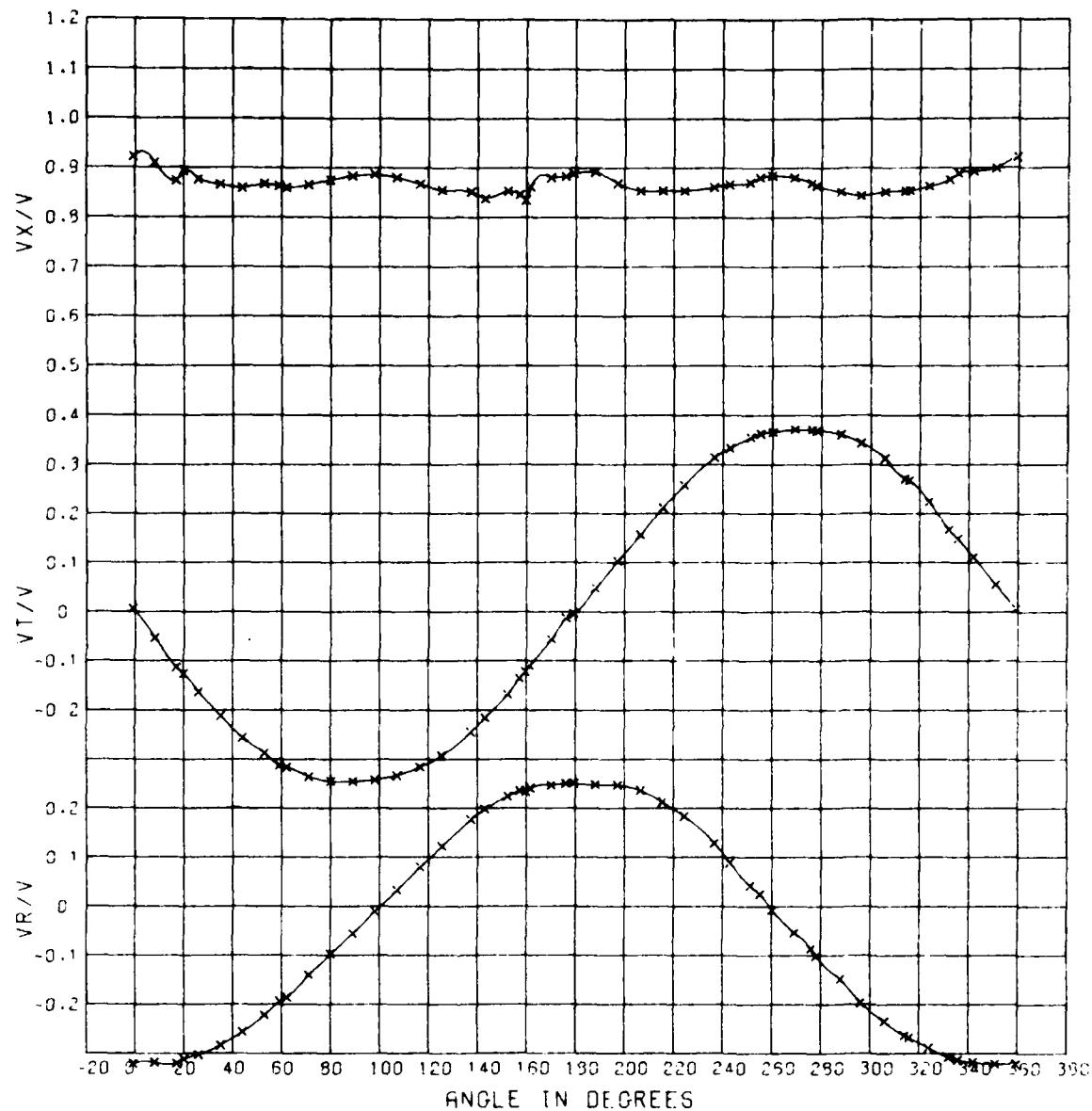
VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ALONE 200 INC 4KTS13
0.633 RAD.

Figure E-2 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.633
for Experiment 13



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ALONE 200 INC 4KTS13
0.781 RAD.

Figure E-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 13



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ALONE 200 INC 4KTS13
0.363 RAD.

Figure E-4 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.963
for Experiment 13

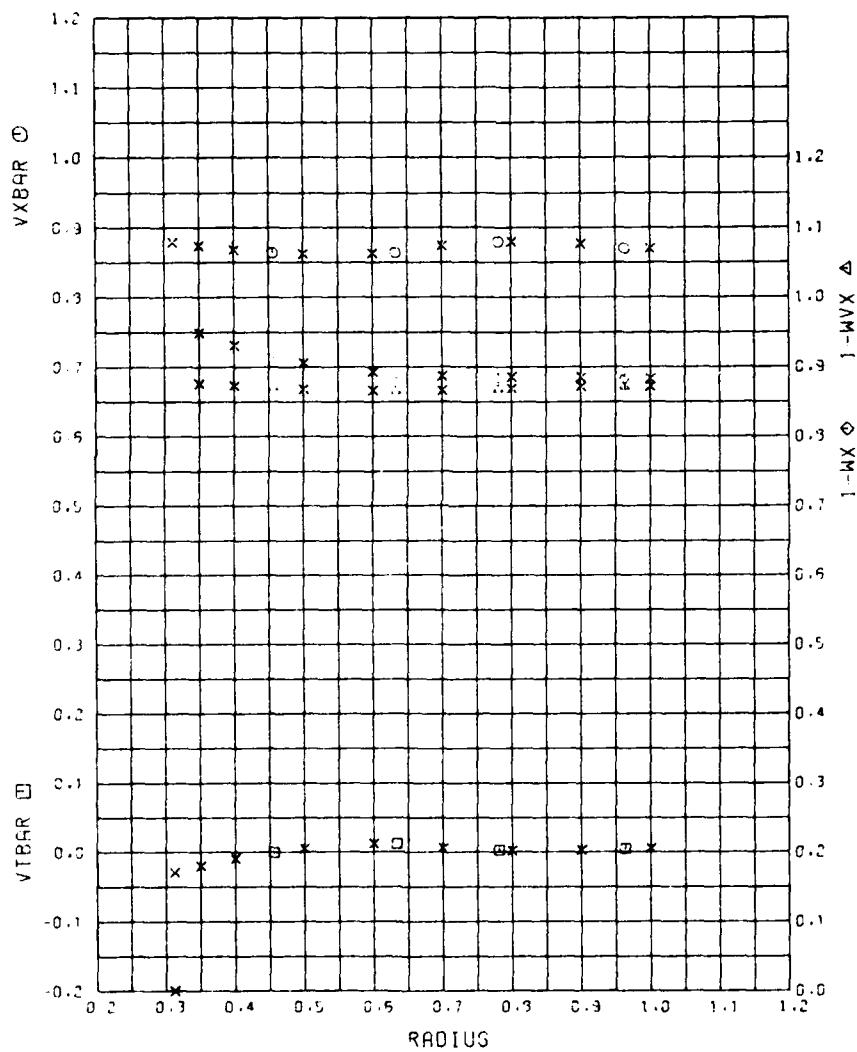


Figure E-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 13

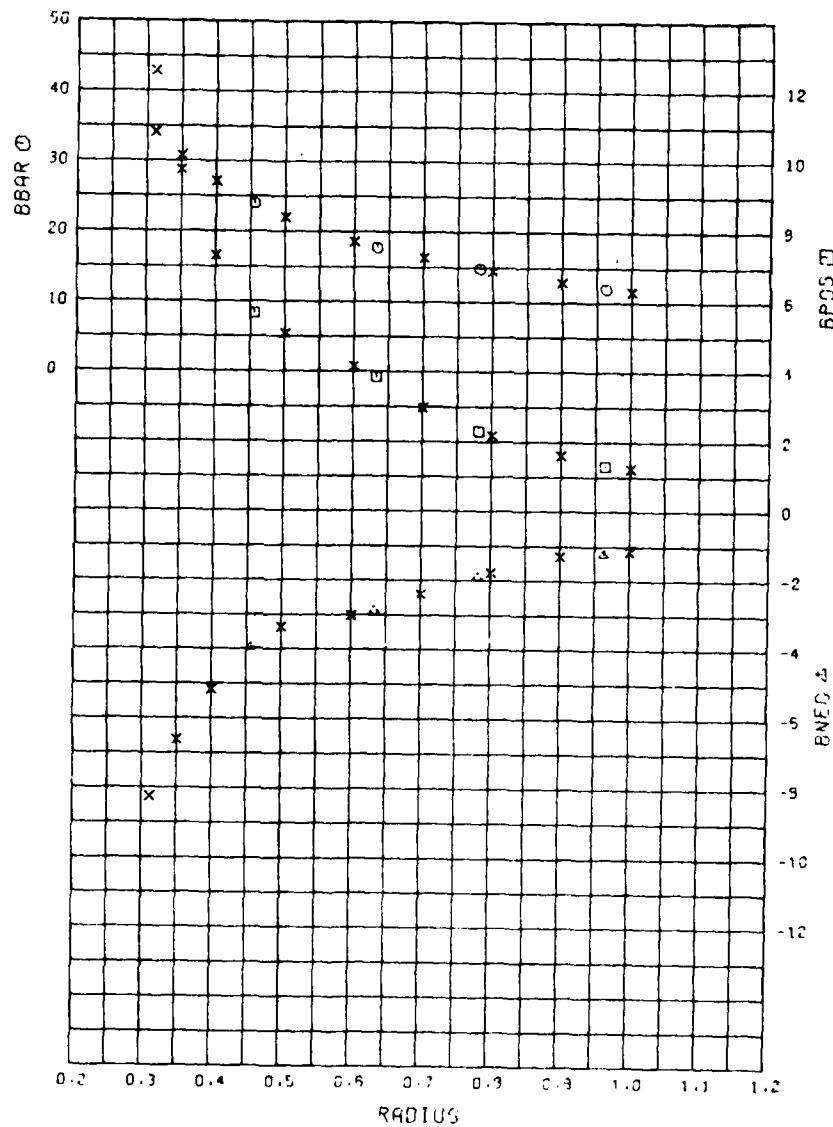


Figure E-6 - Radial Distribution of the Mean Advance Angles and Advance Angle Variations for Experiment 13

TABLE E -1

INPUT DATA FOR HARMONIC ANALYSIS FOR R/V ATHENA
WITH BASS DYNAMOMETER BOAT, EXPERIMENT 13

ANGLE	RADIUS *	WZ/W	ANGLE	RADIUS *	WZ/W	ANGLE	RADIUS *	WZ/W	ANGLE	RADIUS *	WZ/W
-1.0	.923	.981	-0.9	.923	.979	-0.8	.923	.979	-0.7	.922	.980
-0.9	.931	.982	-0.8	.931	.979	-0.7	.930	.980	-0.6	.929	.980
-0.8	.932	.982	-0.7	.932	.979	-0.6	.932	.980	-0.5	.932	.980
-0.7	.933	.982	-0.6	.933	.979	-0.5	.933	.980	-0.4	.933	.980
-0.6	.933	.982	-0.5	.933	.979	-0.4	.933	.980	-0.3	.933	.980
-0.5	.933	.982	-0.4	.933	.979	-0.3	.933	.980	-0.2	.933	.980
-0.4	.933	.982	-0.3	.933	.979	-0.2	.933	.980	-0.1	.933	.980
-0.3	.933	.982	-0.2	.933	.979	-0.1	.933	.980	0.0	.933	.980
-0.2	.933	.982	-0.1	.933	.979	0.1	.933	.980	0.2	.933	.980
-0.1	.933	.982	0.0	.933	.979	0.3	.933	.980	0.5	.933	.980
0.0	.933	.982	0.4	.933	.979	0.7	.933	.980	1.0	.933	.980
0.1	.933	.982	0.5	.933	.979	0.8	.933	.980	1.3	.933	.980
0.2	.933	.982	0.6	.933	.979	1.1	.933	.980	1.6	.933	.980
0.3	.933	.982	0.7	.933	.979	1.4	.933	.980	2.0	.933	.980
0.4	.933	.982	0.8	.933	.979	1.7	.933	.980	2.4	.933	.980
0.5	.933	.982	0.9	.933	.979	2.0	.933	.980	2.8	.933	.980
0.6	.933	.982	1.0	.933	.979	2.3	.933	.980	3.2	.933	.980
0.7	.933	.982	1.1	.933	.979	2.6	.933	.980	3.9	.933	.980
0.8	.933	.982	1.2	.933	.979	2.9	.933	.980	4.6	.933	.980
0.9	.933	.982	1.3	.933	.979	3.2	.933	.980	5.3	.933	.980
1.0	.933	.982	1.4	.933	.979	3.5	.933	.980	6.0	.933	.980
1.1	.933	.982	1.5	.933	.979	3.8	.933	.980	6.7	.933	.980
1.2	.933	.982	1.6	.933	.979	4.1	.933	.980	7.4	.933	.980
1.3	.933	.982	1.7	.933	.979	4.4	.933	.980	8.1	.933	.980
1.4	.933	.982	1.8	.933	.979	4.7	.933	.980	8.8	.933	.980
1.5	.933	.982	1.9	.933	.979	5.0	.933	.980	9.5	.933	.980
1.6	.933	.982	2.0	.933	.979	5.3	.933	.980	10.2	.933	.980
1.7	.933	.982	2.1	.933	.979	5.6	.933	.980	10.9	.933	.980
1.8	.933	.982	2.2	.933	.979	5.9	.933	.980	11.6	.933	.980
1.9	.933	.982	2.3	.933	.979	6.2	.933	.980	12.3	.933	.980
2.0	.933	.982	2.4	.933	.979	6.5	.933	.980	13.0	.933	.980
2.1	.933	.982	2.5	.933	.979	6.8	.933	.980	13.7	.933	.980
2.2	.933	.982	2.6	.933	.979	7.1	.933	.980	14.4	.933	.980
2.3	.933	.982	2.7	.933	.979	7.4	.933	.980	15.1	.933	.980
2.4	.933	.982	2.8	.933	.979	7.7	.933	.980	15.8	.933	.980
2.5	.933	.982	2.9	.933	.979	8.0	.933	.980	16.5	.933	.980
2.6	.933	.982	3.0	.933	.979	8.3	.933	.980	17.2	.933	.980
2.7	.933	.982	3.1	.933	.979	8.6	.933	.980	17.9	.933	.980
2.8	.933	.982	3.2	.933	.979	8.9	.933	.980	18.6	.933	.980
2.9	.933	.982	3.3	.933	.979	9.2	.933	.980	19.3	.933	.980
3.0	.933	.982	3.4	.933	.979	9.5	.933	.980	20.0	.933	.980
3.1	.933	.982	3.5	.933	.979	9.8	.933	.980	20.7	.933	.980
3.2	.933	.982	3.6	.933	.979	10.1	.933	.980	21.4	.933	.980
3.3	.933	.982	3.7	.933	.979	10.4	.933	.980	22.1	.933	.980
3.4	.933	.982	3.8	.933	.979	10.7	.933	.980	22.8	.933	.980
3.5	.933	.982	3.9	.933	.979	11.0	.933	.980	23.5	.933	.980
3.6	.933	.982	4.0	.933	.979	11.3	.933	.980	24.2	.933	.980
3.7	.933	.982	4.1	.933	.979	11.6	.933	.980	24.9	.933	.980
3.8	.933	.982	4.2	.933	.979	11.9	.933	.980	25.6	.933	.980
3.9	.933	.982	4.3	.933	.979	12.2	.933	.980	26.3	.933	.980
4.0	.933	.982	4.4	.933	.979	12.5	.933	.980	27.0	.933	.980
4.1	.933	.982	4.5	.933	.979	12.8	.933	.980	27.7	.933	.980
4.2	.933	.982	4.6	.933	.979	13.1	.933	.980	28.4	.933	.980
4.3	.933	.982	4.7	.933	.979	13.4	.933	.980	29.1	.933	.980
4.4	.933	.982	4.8	.933	.979	13.7	.933	.980	29.8	.933	.980
4.5	.933	.982	4.9	.933	.979	14.0	.933	.980	30.5	.933	.980
4.6	.933	.982	5.0	.933	.979	14.3	.933	.980	31.2	.933	.980
4.7	.933	.982	5.1	.933	.979	14.6	.933	.980	31.9	.933	.980
4.8	.933	.982	5.2	.933	.979	14.9	.933	.980	32.6	.933	.980
4.9	.933	.982	5.3	.933	.979	15.2	.933	.980	33.3	.933	.980
5.0	.933	.982	5.4	.933	.979	15.5	.933	.980	34.0	.933	.980
5.1	.933	.982	5.5	.933	.979	15.8	.933	.980	34.7	.933	.980
5.2	.933	.982	5.6	.933	.979	16.1	.933	.980	35.4	.933	.980
5.3	.933	.982	5.7	.933	.979	16.4	.933	.980	36.1	.933	.980
5.4	.933	.982	5.8	.933	.979	16.7	.933	.980	36.8	.933	.980
5.5	.933	.982	5.9	.933	.979	17.0	.933	.980	37.5	.933	.980
5.6	.933	.982	6.0	.933	.979	17.3	.933	.980	38.2	.933	.980
5.7	.933	.982	6.1	.933	.979	17.6	.933	.980	38.9	.933	.980
5.8	.933	.982	6.2	.933	.979	17.9	.933	.980	39.6	.933	.980
5.9	.933	.982	6.3	.933	.979	18.2	.933	.980	40.3	.933	.980
6.0	.933	.982	6.4	.933	.979	18.5	.933	.980	41.0	.933	.980
6.1	.933	.982	6.5	.933	.979	18.8	.933	.980	41.7	.933	.980
6.2	.933	.982	6.6	.933	.979	19.1	.933	.980	42.4	.933	.980
6.3	.933	.982	6.7	.933	.979	19.4	.933	.980	43.1	.933	.980
6.4	.933	.982	6.8	.933	.979	19.7	.933	.980	43.8	.933	.980
6.5	.933	.982	6.9	.933	.979	20.0	.933	.980	44.5	.933	.980
6.6	.933	.982	7.0	.933	.979	20.3	.933	.980	45.2	.933	.980
6.7	.933	.982	7.1	.933	.979	20.6	.933	.980	45.9	.933	.980
6.8	.933	.982	7.2	.933	.979	20.9	.933	.980	46.6	.933	.980
6.9	.933	.982	7.3	.933	.979	21.2	.933	.980	47.3	.933	.980
7.0	.933	.982	7.4	.933	.979	21.5	.933	.980	48.0	.933	.980
7.1	.933	.982	7.5	.933	.979	21.8	.933	.980	48.7	.933	.980
7.2	.933	.982	7.6	.933	.979	22.1	.933	.980	49.4	.933	.980
7.3	.933	.982	7.7	.933	.979	22.4	.933	.980	50.1	.933	.980
7.4	.933	.982	7.8	.933	.979	22.7	.933	.980	50.8	.933	.980
7.5	.933	.982	7.9	.933	.979	23.0	.933	.980	51.5	.933	.980
7.6	.933	.982	8.0	.933	.979	23.3	.933	.980	52.2	.933	.980
7.7	.933	.982	8.1	.933	.979	23.6	.933	.980	52.9	.933	.980
7.8	.933	.982	8.2	.933	.979	23.9	.933	.980	53.6	.933	.980
7.9	.933	.982	8.3	.933	.979	24.2	.933	.980	54.3	.933	.980
8.0	.933	.982	8.4	.933	.979	24.5	.933	.980	55.0	.933	.980
8.1	.933	.982	8.5	.933	.979	24.8	.933	.980	55.7	.933	.980
8.2	.933	.982	8.6	.933	.979	25.1	.933	.980	56.4	.933	.980
8.3	.933	.982	8.7	.933	.979	25.4	.933	.980	57.1	.933	.980
8.4	.933	.982	8.8	.933	.979	25.7	.933	.980	57.8	.933	.980
8.5	.933	.982	8.9	.933	.979	26.0	.933	.980	58.5	.933	.980
8.6	.933	.982	9.0	.933	.979	26.3	.933	.980	59.2	.933	.980
8.7	.933	.982	9.1	.933	.979	26.6	.933	.980	59.9	.933	.980
8.8	.933	.982	9.2	.933	.979	26.9	.933	.980	60.6	.933	.980
8.9	.933	.982	9.3	.933	.979	27.2	.933	.980	61.3	.933	.980
9.0	.933	.982	9.4	.933	.979	27.5	.933	.980	62.0	.933	.980
9.1	.933	.982	9.5	.933	.979	27.8	.933	.980	62.7	.933	.980
9.2	.933	.982	9.6	.933	.979	28.1	.933	.980	63.4	.933	.980
9.3	.933	.982	9.7	.933	.979	28.4	.933	.980	64.1	.933	.980
9.4	.933	.982	9.8	.933	.979	28.7	.933	.980	64.8	.933	.980
9.5	.933	.982	9.9	.933	.979	29.0	.933	.980	65.5	.933	.980
9.6</td											

TABLE E-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 13

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ALONE 200 INC 4KTS 3
PROPELLER DIAMETER = 6.00 FEET
JA = .739

RADIUS = .456	.633	.781	.963	.312	.350	.400	.500	.600	.700	.800	.900	1.000
VXBAR = .864	.864	.880	.870	.879	.874	.868	.862	.863	.874	.880	.877	.870
VTBAR = -.000	.012	.003	.005	-.029	-.020	-.009	.005	.012	.006	.002	.003	.005
VRBAR = -.011	-.035	-.039	-.044	.024	.013	.001	-.019	-.032	-.037	-.039	-.042	-.044
1-WX = .870	.865	.868	.871	0.000	.876	.873	.878	.866	.866	.869	.872	.872
1-WX = .020	.890	.885	.883	0.000	.949	.931	.906	.893	.887	.886	.885	.883
BBAR = 24.02	17.73	14.82	11.98	34.09	30.74	27.17	22.62	18.60	16.33	14.50	12.90	11.55
B2G3 = 5.67	3.84	2.30	1.31	12.57	9.75	7.31	5.06	4.15	2.97	2.18	1.62	1.23
THETA = 97.50	95.00	97.50	100.00	105.00	105.00	105.00	105.00	85.00	85.00	95.00	95.00	97.50
BEG = -3.96	-2.87	-1.89	-1.23	-8.26	-6.63	-5.17	-3.36	-3.02	-2.40	-1.77	-1.30	-1.16
THETA = 260.00	220.00	217.50	295.00	315.00	290.00	260.00	231.50	220.00	220.00	227.50	295.00	295.00

VXBAR IS CIRCUMFERNENTIAL MEAN LONGITUDINAL VELOCITY.
 VTBAR IS CIRCUMFERNENTIAL MEAN TANGENTIAL VELOCITY.
 VRBAR IS CIRCUMFERNENTIAL MEAN RADIAL VELOCITY.
 1-WX IS VOLUMETRIC MEAN WAKE VELOCITY WITHOUT TANGENTIAL CORRECTION.
 1-WX IS VOLUMETRIC MEAN WAKE VELOCITY WITH TANGENTIAL CORRECTION.
 BBAR IS MEAN ANGLE OF ADVANCE.
 B2G3 IS VARIATION BETWEEN THE MAXIMUM AND MEAN ADVANCE ANGLES (G2TA BETA PLUS).
 BEG IS VARIATION BETWEEN THE MINIMUM AND MEAN ADVANCE ANGLES (G2TA BETA MINUS).
 THETA IS ANGLE IN DEGREES AT WHICH CORRESPONDING BPPS OR BNEE VALUES.

TABLE E-3 - HARMONIC ANALYSIS OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 13

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
ELECTRIC FIELD RADIUS = 0.456 FEET, 600 VOLTS, 60 CYCLES PER SEC, 600 FEET, 60 CYCLES PER SEC, 60 CYCLES PER SEC ALONE, 200 INC 4KTS13 JA = .739									
RADIAL	1	2	3	4	5	6	7	8	
RADIUS = .456	.0209	.0537	.0147	.0520	.0057	.0055	.0023	.0014	
AMPLITUDE =	92.7	88.8	82.7	79.4	69.4	84.8	29.1	62.0	
PHASE ANGLE =									
RADIUS = .633	.0575	.0172	.0032	.0011	.0057	.0015	.0016		
AMPLITUDE =	71.8	252.4	51.3	31.7	25.7	66.8	87.9	134.4	
PHASE ANGLE =									
RADIUS = .781	.0368	.0500	.0117	.0021	.0018	.0034	.0041	.0039	
AMPLITUDE =	75.6	172.8	41.4	25.5	25.8	64.8	112.2	48.1	
PHASE ANGLE =									
RADIUS = .963	.0086	.0244	.0032	.0018	.0052	.0033	.0013	.0043	
AMPLITUDE =	72.2	88.6	104.5	75.5	249.4	92.4	64.7	93.4	
PHASE ANGLE =									
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
RADIAL	9	10	11	12	13	14	15	16	
RADIUS = .456	.0018	.0010	.0024	.0025	.0011	.0021	.0013	.0009	
AMPLITUDE =	21.6	38.8	13.2	30.6	325.1	280.5	226.0	355.0	
PHASE ANGLE =									
RADIUS = .633	.0020	.0024	.0035	.0025	.0007	.0007	.0020	.0019	
AMPLITUDE =	50.1	132.8	161.1	113.2	357.6	50.6	223.0	145.4	
PHASE ANGLE =									
RADIUS = .781	.0012	.0017	.0022	.0023	.0007	.0011	.0014		
AMPLITUDE =	72.5	320.7	261.1	328.2	123.4	147.6	214.5	162.5	
PHASE ANGLE =									
RADIUS = .963	.0010	.0004	.0018	.0012	.0027	.0026	.0023	.0011	
AMPLITUDE =	255.4	34.0	85.0	71.6	90.8	49.3	79.8	35.5	
PHASE ANGLE =									

TABLE E-4 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 15

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ALONE 200 INC 4KTS13 PROPELLER DIAMETER = 6.00 FEET JA = .739								
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX V)								
HARMONIC	1	2	3	4	5	6	7	8
RADIUS = .312								
AMPLITUDE = .0656	.0698	.0239	.0173	.0161	.0049	.0041	.0078	
PHASE ANGLE = 232.4	95.9	85.3	41.6	69.2	129.2	27.0	24.7	
RADIUS = .350								
AMPLITUDE = .0400	.0502	.0210	.0149	.0129	.0048	.0036	.0056	
PHASE ANGLE = 226.2	95.3	84.7	49.4	69.2	113.9	25.8	27.4	
RADIUS = .400								
AMPLITUDE = .0139	.0262	.0177	.0128	.0092	.0051	.0030	.0032	
PHASE ANGLE = 131.0	91.0	81.8	52.0	69.3	97.5	25.7	35.0	
RADIUS = .500								
AMPLITUDE = .0356	.0031	.0123	.0122	.0034	.0058	.0019	.0011	
PHASE ANGLE = 79.2	292.6	62.0	67.7	69.4	77.9	36.6	111.6	
RADIUS = .600								
AMPLITUDE = .0556	.0170	.0103	.0143	.0003	.0059	.0016	.0016	
PHASE ANGLE = 72.4	274.6	81.1	100.4	254.5	68.6	74.7	143.3	
RADIUS = .700								
AMPLITUDE = .0483	.0089	.0114	.0182	.0012	.0044	.0033	.0024	
PHASE ANGLE = 73.7	244.3	81.9	97.7	255.8	64.1	107.9	57.8	
RADIUS = .800								
AMPLITUDE = .0340	.0063	.0116	.0205	.0020	.0032	.0041	.0041	
PHASE ANGLE = 76.0	158.7	86.0	95.2	254.2	66.0	112.1	49.0	
RADIUS = .900								
AMPLITUDE = .0187	.0077	.0039	.0203	.0037	.0029	.0028	.0043	
PHASE ANGLE = 76.5	106.8	96.0	94.7	250.9	80.4	104.3	66.9	
RADIUS = 1.000								
AMPLITUDE = .0086	.0084	.0042	.0188	.0052	.0033	.0013	.0043	
PHASE ANGLE = 72.2	63.6	101.5	95.3	249.4	32.4	64.7	93.4	

TABLE E-4 (Continued)

VELOCITY COEFFICIENT RATINGS FOR V=5271 FEET SEC. 5450 FEET SEC. 200 FEET
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF CONSTITUTIONAL VELOCITY COMPONENT RATINGS (VX VI)						
HARMONIC	=	9	10	11	12	13
RADIUS = .312		.0019	.0085	.0078	.0120	.0016
AMPLITUDE =		327.6	331.5	5.4	302.2	195.6
PHASE ANGLE =						263.7
RADIUS = .350						
AMPLITUDE =		.0017	.0059	.0051	.0055	.0058
PHASE ANGLE =		344.1	334.6	6.6	301.9	208.3
RADIUS = .400						
AMPLITUDE =		.0017	.0030	.0042	.0047	.0005
PHASE ANGLE =		4.4	344.1	8.7	301.4	262.4
RADIUS = .500						
AMPLITUDE =		.0019	.0014	.0014	.0006	.0010
PHASE ANGLE =		31.3	108.4	20.9	120.3	339.2
RADIUS = .600						
AMPLITUDE =		.0020	.0026	.0005	.0026	.0012
PHASE ANGLE =		46.2	131.1	142.3	116.2	353.1
RADIUS = .700						
AMPLITUDE =		.0017	.0001	.0004	.0010	.0003
PHASE ANGLE =		61.7	14.6	213.3	353.7	20.6
RADIUS = .800						
AMPLITUDE =		.0011	.0019	.0001	.0028	.0008
PHASE ANGLE =		74.9	320.7	280.5	327.5	121.8
RADIUS = .900						
AMPLITUDE =		.0001	.0015	.0018	.0018	.0014
PHASE ANGLE =		181.0	327.3	72.6	340.1	102.8
RADIUS = 1.000						
AMPLITUDE =		.0010	.0004	.0018	.0012	.0027
PHASE ANGLE =		255.4	34.0	80.0	71.6	90.8

TABLE E-5 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 13

VELOCITY COEFFICIENTS FOR FIELD 5271 BASS BOAT ALONE 200 INC 4KTS13
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)							
HARMONIC	=	1	2	3	4	5	6
RADIUS = .456							
AMPLITUDE =	.4438	.0074	.0050	.0043	.0026	.0012	.0030
PHASE ANGLE =	181.9	150.6	185.5	183.2	20.9	207.7	184.0
RADIUS = .633							
AMPLITUDE =	.3919	.004	.0073	.0024	.0019	.0006	.0026
PHASE ANGLE =	181.4	246.8	176.9	176.4	318.5	201.9	346.2
RADIUS = .781							
AMPLITUDE =	.3747	.0062	.0013	.0044	.0011	.0022	.0007
PHASE ANGLE =	180.8	99.9	173.4	323.2	11.4	158.1	12.1
RADIUS = .963							
AMPLITUDE =	.3649	.0081	.0013	.0041	.0018	.0005	.0006
PHASE ANGLE =	180.2	246.0	23.7	111.6	352.0	122.6	84.0
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)							
HARMONIC	=	9	10	11	12	13	14
RADIUS = .456							
AMPLITUDE =	.0016	.0020	.0016	.0015	.0014	.0006	.0011
PHASE ANGLE =	147.9	189.9	176.9	209.2	142.3	166.1	174.4
RADIUS = .633							
AMPLITUDE =	.0015	.0007	.0009	.0005	.0010	.0011	.0010
PHASE ANGLE =	335.4	187.7	101.3	176.0	76.8	325.2	218.8
RADIUS = .781							
AMPLITUDE =	.0012	.0002	.0014	.0009	.0017	.0005	.0007
PHASE ANGLE =	352.5	281.2	245.1	151.4	275.0	225.2	250.3
RADIUS = .963							
AMPLITUDE =	.0005	.0009	.0004	.0004	.0004	.0006	.0005
PHASE ANGLE =	11.5	11.2	11.4	162.6	53.1	214.6	34.0

TABLE II-6 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 13

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)		EFFECTS OF FISHES ON PROPULSION									
		FISHES IN WATER				FISHES IN AIR				FISHES IN AIR	
HARMONIC	RADIUS	1	2	3	4	5	6	7	8	1	2
	RADIUS = .312	.5114	.0408	.0229	.0062	.0136	.0061	.0081	.0077		
	AMPLITUDE = 182.2	100.5	178.4	197.4	36.6	201.6	166.8				
	PHASE ANGLE =										
	RADIUS = .350	.4913	.0252	.0201	.0059	.0105	.0050	.0059	.0063		
	AMPLITUDE = 182.1	104.5	182.1	193.0	34.7	202.9	168.3				
	PHASE ANGLE =										
	RADIUS = .400	.4674	.0166	.0170	.0055	.0071	.0038	.0035	.0046		
	AMPLITUDE = 182.0	114.8	182.6	187.9	30.5	205.0	171.7				
	PHASE ANGLE =										
	RADIUS = .500	.4277	.0067	.0118	.0045	.0026	.0019	.0004	.0020		
	AMPLITUDE = 181.8	205.6	187.8	186.2	5.9	209.8	289.6				
	PHASE ANGLE =										
	RADIUS = .600	.3989	.0108	.0052	.0030	.0018	.0008	.0023	.0003		
	AMPLITUDE = 181.5	244.5	191.1	176.2	319.9	209.3					
	PHASE ANGLE =										
	RADIUS = .700	.3831	.0022	.0055	.0005	.0031	.0008	.0025	.0005		
	AMPLITUDE = 181.1	166.3	180.9	239.5	1.3	177.7	359.5				
	PHASE ANGLE =										
	RADIUS = .800	.3731	.0065	.0051	.0014	.0046	.0012	.0021	.0007		
	AMPLITUDE = 180.8	98.8	172.6	328.1	11.7	154.1	14.8				
	PHASE ANGLE =										
	RADIUS = .900	.3669	.0023	.0032	.0008	.0047	.0015	.0011	.0006		
	AMPLITUDE = 180.4	142.3	179.4	10.4	5.3	134.3	33.4				
	PHASE ANGLE =										
	RADIUS = 1.000	.3649	.0081	.0021	.0013	.0041	.0018	.0005	.0006		
	AMPLITUDE = 180.2	246.0	210.7	111.8	352.0	122.6	84.0				
	PHASE ANGLE =										

TABLE E-6 (Continued)

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .312	=	.0067	.0032	.0044	.0032	.0039	.0045	.0017	.0043
AMPLITUDE =		147.8	195.4	213.4	209.7	211.9	158.6	135.7	154.4
PHASE ANGLE =									
RADIUS = .350	=	.0051	.0029	.0034	.0026	.0028	.0032	.0014	.0031
AMPLITUDE =		148.0	193.9	207.6	210.1	201.9	158.8	144.6	153.4
PHASE ANGLE =									
RADIUS = .400	=	.0033	.0024	.0024	.0020	.0018	.0018	.0012	.0017
AMPLITUDE =		148.1	192.3	196.5	210.2	179.8	159.9	158.0	151.3
PHASE ANGLE =									
RADIUS = .500	=	.0005	.0016	.0013	.0011	.0014	.0002	.0010	.0001
AMPLITUDE =		144.7	188.4	155.5	206.7	116.4	294.4	187.0	1.5
PHASE ANGLE =									
RADIUS = .600	=	.0012	.0009	.0010	.0006	.0013	.0010	.0010	.0009
AMPLITUDE =		334.7	185.7	110.9	187.5	85.1	326.6	211.8	325.9
PHASE ANGLE =									
RADIUS = .700	=	.0014	.0003	.0001	.0008	.0007	.0005	.0009	.0007
AMPLITUDE =		343.3	228.1	22.0	156.2	284.5	293.1	234.5	259.7
PHASE ANGLE =									
RADIUS = .800	=	.0012	.0002	.0004	.0009	.0018	.0005	.0007	.0009
AMPLITUDE =		354.8	284.0	284.9	151.8	274.7	217.4	254.5	223.6
PHASE ANGLE =									
RADIUS = .900	=	.0008	.0003	.0001	.0009	.0011	.0006	.0003	.0004
AMPLITUDE =		13.0	157.1	296.2	163.1	279.1	205.6	319.8	225.1
PHASE ANGLE =									
RADIUS = 1.000	=	.0005	.0009	.0006	.0009	.0004	.0005	.0006	.0005
AMPLITUDE =		41.5	149.2	69.9	142.0	53.1	214.6	34.0	11.1
PHASE ANGLE =									

APPENDIX F
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENT 14

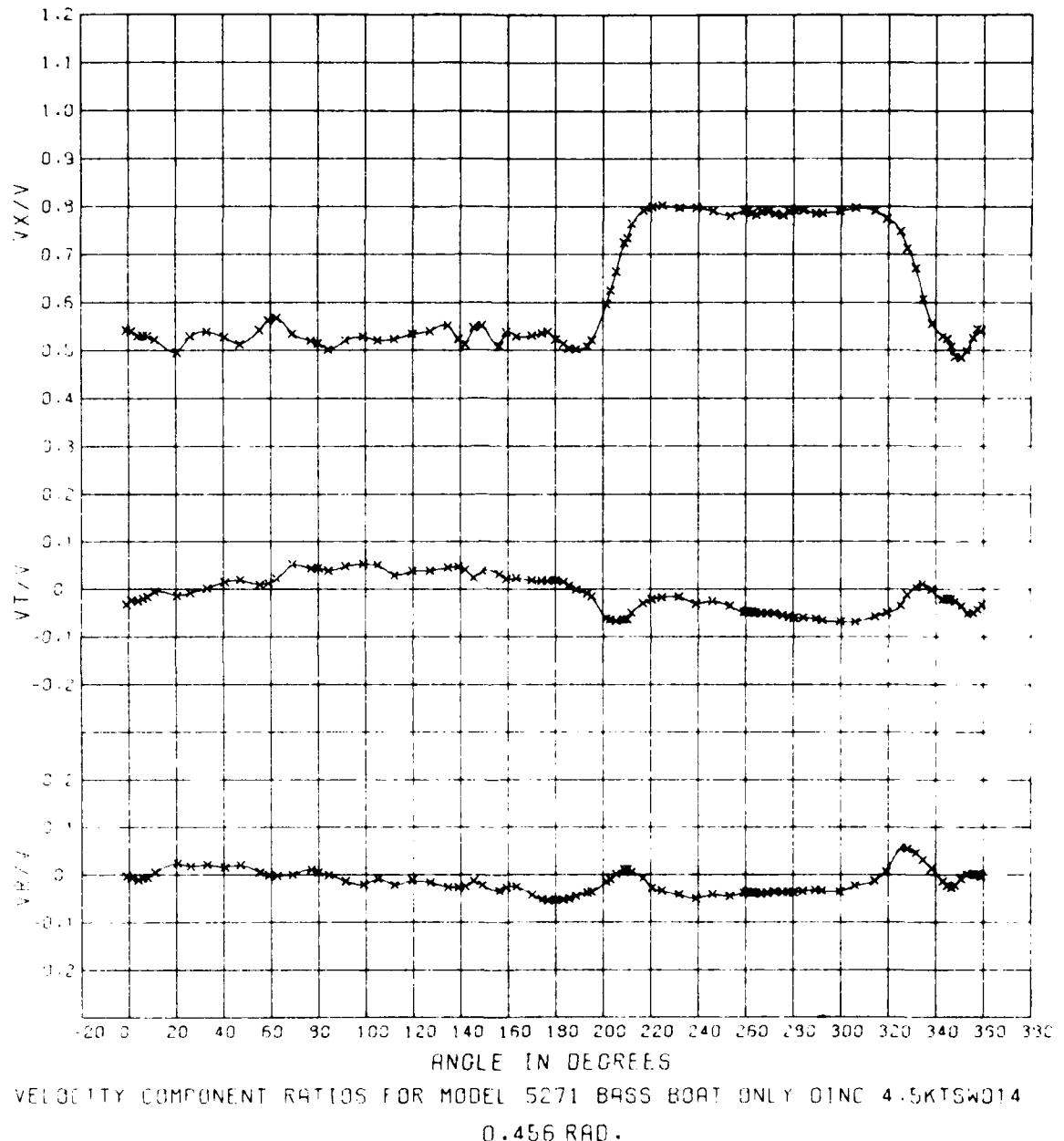
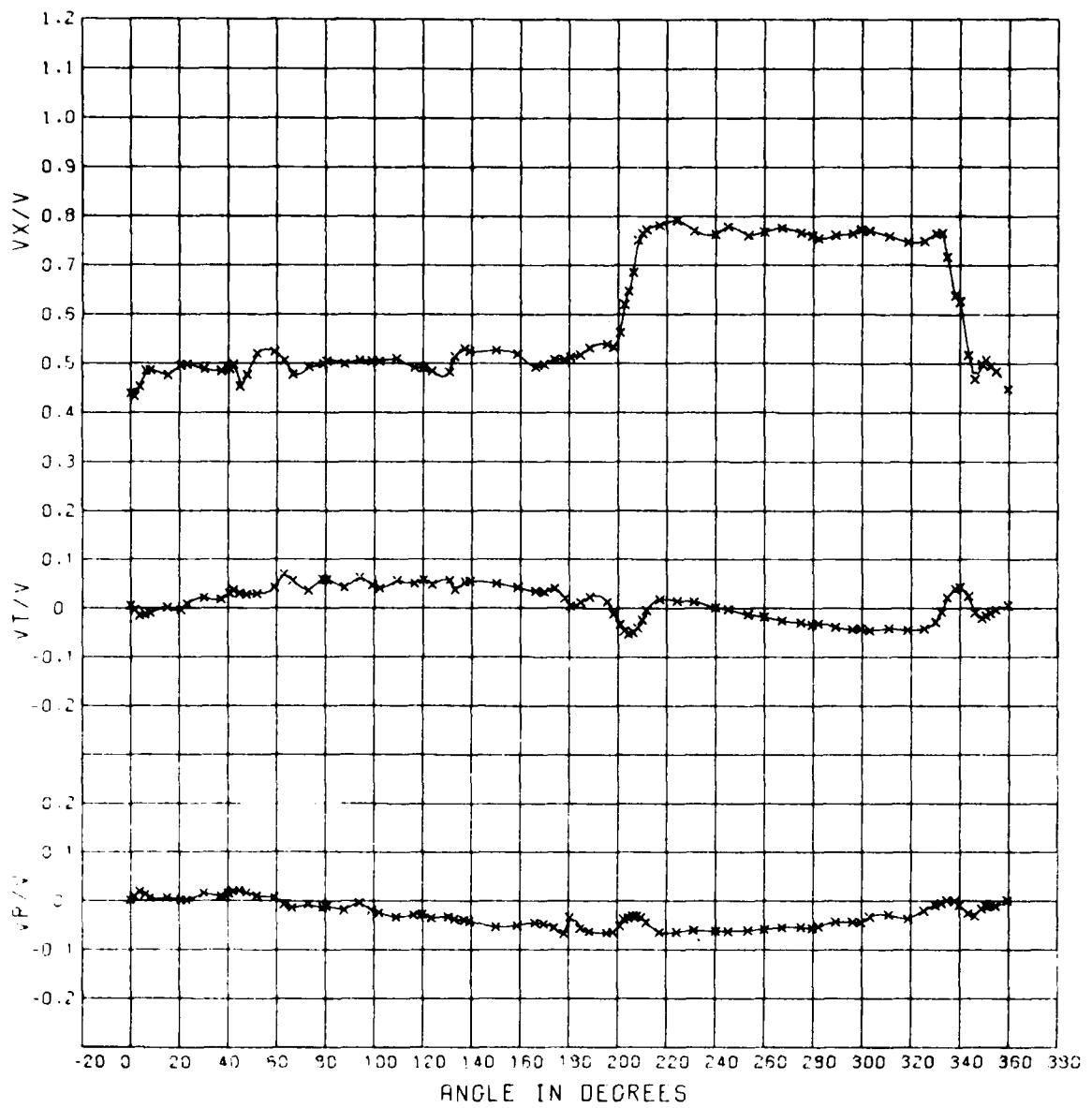
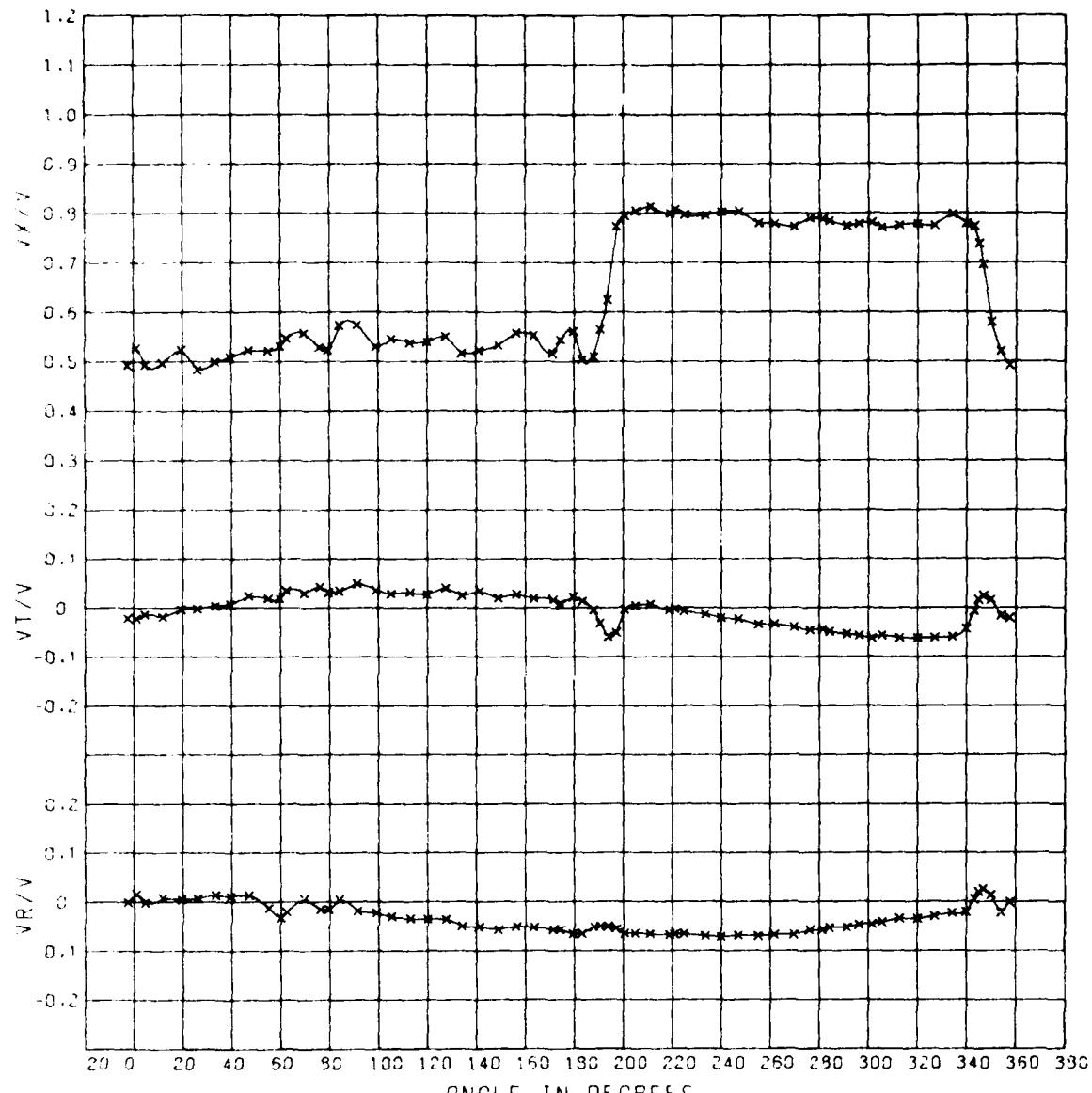


Figure F-1 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.456
for Experiment 14



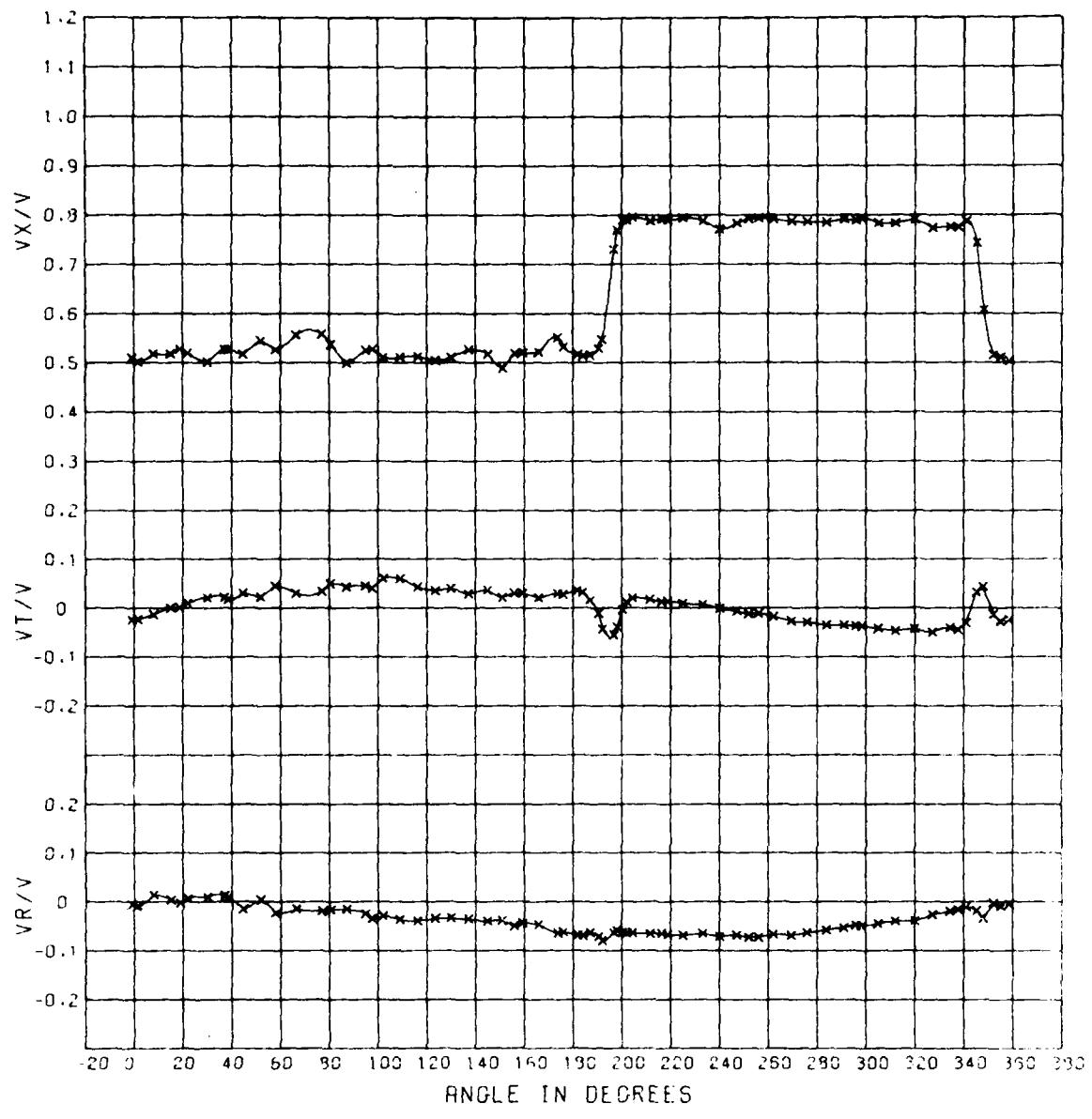
VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY DINC 4.5KTSWD14
0.633 RAD.

Figure F-2 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.633
for Experiment 14



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY DINC 4.5KTSW014
0.781 RAD.

Figure F-3 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.781
for Experiment 14



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY DINC 4.5KTSW014
0.963 RAD.

Figure F-4 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.963
for Experiment 14

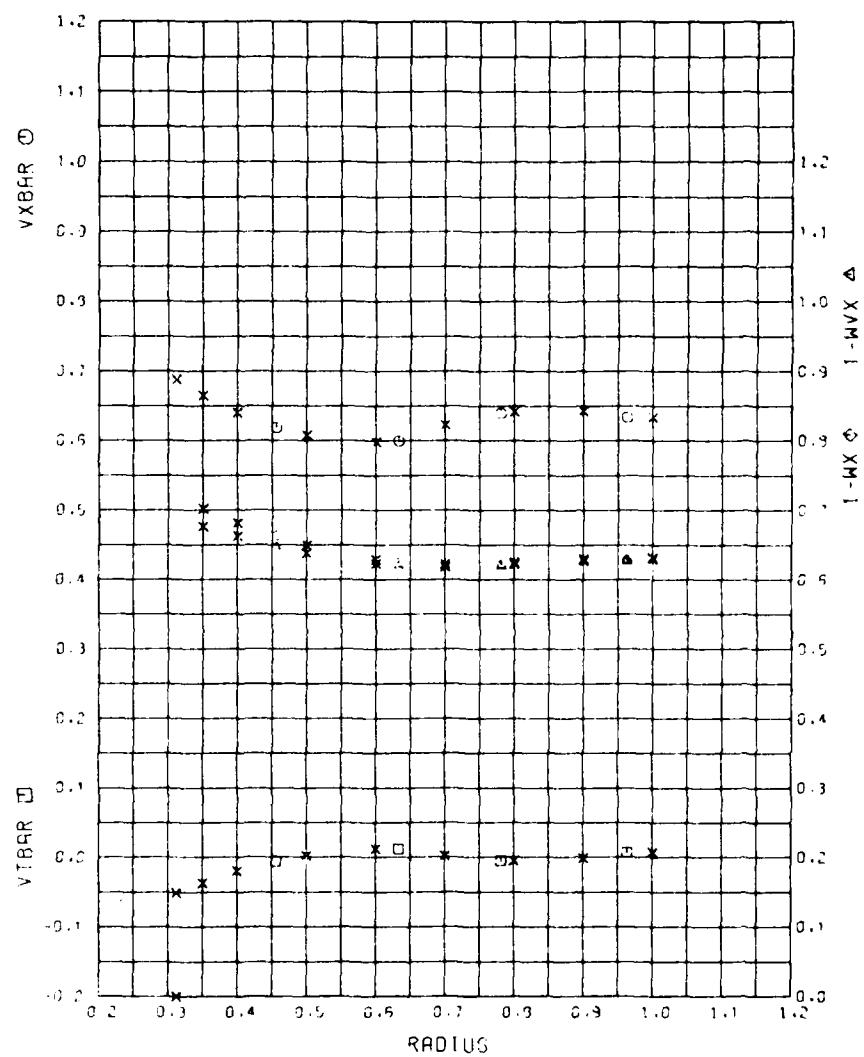


Figure F-5 - Radial Distribution of the Mean Velocity Component Ratios for Experiment 14

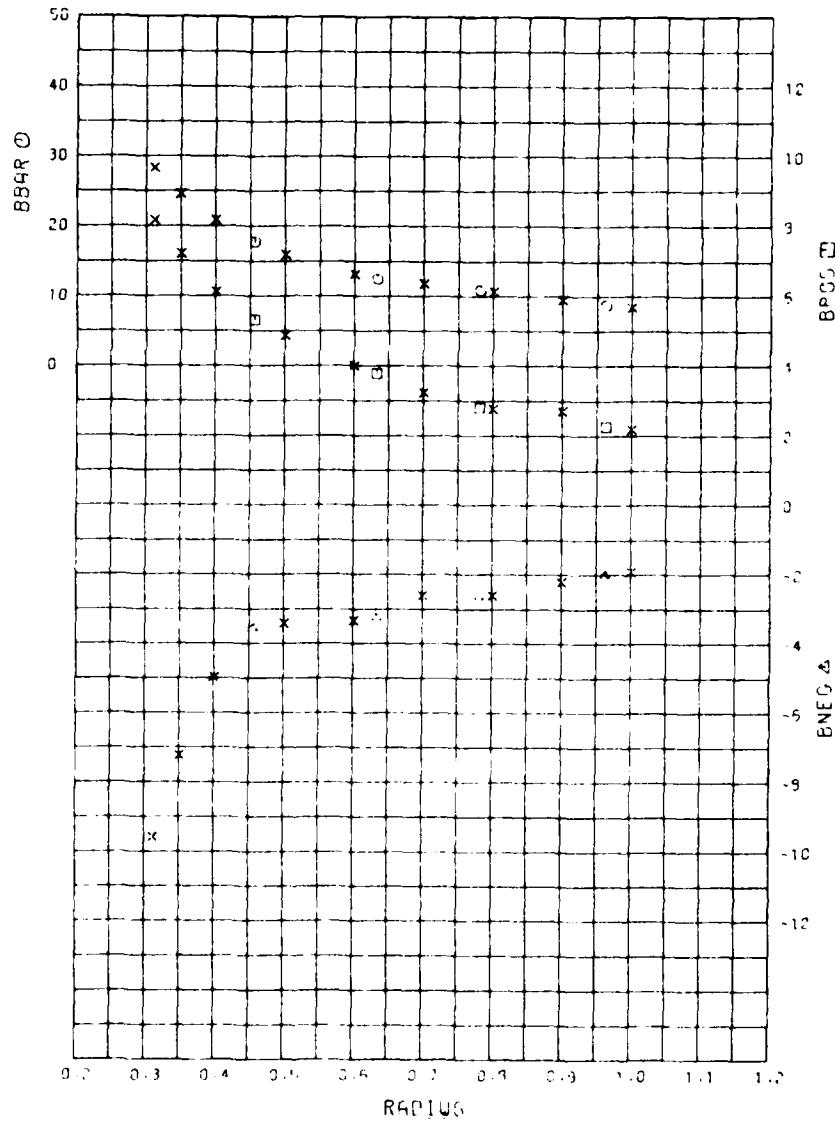


Figure F-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 14

TABLE F-1

INPUT DATA FOR HARMONIC ANALYSIS FOR R/V ATHENA
WITH BASS DYNAMOMETER BOAT, EXPERIMENT 14

TABLE F-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 14

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 0 INC 4.5 MTSW014
PROPELLER DIAMETER = 6.00 FEET
JA = .739

RADIUS = .456	.633	.781	.963	.312	.350	.400	.500	.600	.700	.800	.900	1.000
VXBAR = .619	.600	.640	.634	.688	.665	.640	.608	.598	.623	.642	.643	.634
VTBAR = -.006	.012	-.005	.007	-.051	-.037	-.020	.002	.012	.002	-.005	-.001	.007
VRBAR = -.014	-.030	-.035	-.037	.007	.000	-.007	-.019	-.028	-.033	-.035	-.037	-.037
1-WVX = .647	.620	.619	.627	0.000	.676	.652	.638	.623	.618	.622	.627	.630
1-WX = .663	.625	.622	.629	0.000	.702	.691	.649	.629	.622	.625	.630	.632
BBAR = 17.76	12.51	10.92	8.78	28.34	24.62	20.45	15.43	13.13	11.81	10.70	9.53	8.46
BPOS THETA = 5.32 3007.50	3.77 222.50	2.81 210.00	2.27 300.00	8.17 282.50	7.21 282.50	6.12 282.50	4.87 300.00	4.00 300.00	3.23 222.50	2.77 335.00	2.71 200.00	2.19 300.00
BNEG THETA = -3.55 350.00	-3.25 0.00	-2.64 27.50	-2.00 15.00	-9.59 187.50	-7.24 187.50	-4.47 187.50	-3.41 347.50	-3.33 0.00	-2.61 357.50	-2.21 27.50	-1.92 150.00	

133

VXBAR IS CIRCUMFERENTIAL MEAN LONGITUDINAL VELOCITY.
 VTBAR IS CIRCUMFERENTIAL MEAN TANGENTIAL VELOCITY.
 VRBAR IS CIRCUMFERENTIAL MEAN RADIAL VELOCITY.
 1-WVX IS VOLUMETRIC MEAN WAKE VELOCITY WITHOUT TANGENTIAL CORRECTION.
 1-WX IS VOLUMETRIC MEAN WAKE VELOCITY WITH TANGENTIAL CORRECTION.
 BBAD IS MEAN ANGLE OF ADVANCE.
 BPOS IS VARIATION BETWEEN THE MAXIMUM AND MEAN ADVANCE ANGLES (DELTA BETA PLUS).
 BNEG IS VARIATION BETWEEN THE MINIMUM AND MEAN ADVANCE ANGLES (DELTA BETA MINUS).
 THETA IS ANGLE IN DEGREES AT WHICH CORRESPONDING BPOS, OR BNEG OCCURS.

TABLE 1-3 - HARMONIC ANALYSIS OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 14

VELOCITY COMPONENT RATIOS FOR THE 52'1 BASS BOAT ON A 6.00 FEET DECK PLATEFORM
RADIUS = .456 PHASE ANGLE = 142.7

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)

HARMONIC	1	2	3	4	5	6	7	8
RADIUS = .456								
AMPLITUDE = .1470	.0584	.0017	.0445	.0203	.0042	.0230	.0026	
PHASE ANGLE = 273.5	165.0	272.3	18.0	269.3	10.2	10.2	10.2	
RADIUS = .633								
AMPLITUDE = .1568	.0596	.0247	.0430	.0109	.0226	.0161	.0052	
PHASE ANGLE = 164.1	167.8	263.0	357.6	263.7	354.9	341.9	341.9	
RADIUS = .781								
AMPLITUDE = .1554	.0438	.0520	.0318	.0124	.0280	.0020	.0225	
PHASE ANGLE = 184.2	263.5	174.2	265.4	160.8	257.8	359.5	261.9	
RADIUS = .963								
AMPLITUDE = .1627	.0428	.0435	.0342	.0139	.0249	.0068	.0206	
PHASE ANGLE = 179.2	276.1	165.0	269.0	161.1	267.1	344.4	253.0	

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)

HARMONIC	9	10	11	12	13	14	15	16
RADIUS = .456								
AMPLITUDE = .0069	.0123	.0046	.0047	.0013	.0026	.0006	.0022	
PHASE ANGLE = .4	120.8	40.2	74.9	332.1	44.2	266.5	254.1	
RADIUS = .633								
AMPLITUDE = .0157	.0077	.0041	.0109	.0079	.0050	.0043	.0022	
PHASE ANGLE = 312.2	58.2	301.3	62.2	127.6	41.3	180.9	224.3	
RADIUS = .781								
AMPLITUDE = .0116	.0148	.0024	.0016	.0019	.0030	.0066	.0095	
PHASE ANGLE = 7.1	258.8	331.9	313.1	338.2	180.5	320.7	111.4	
RADIUS = .963								
AMPLITUDE = .0110	.0096	.0160	.0097	.0122	.0023	.0086	.0073	
PHASE ANGLE = 336.1	247.1	355.5	256.1	339.5	151.4	350.8	48.3	

TABLE F-4 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 14

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 0INC 4.5KTSW014 PROPELLER DIAMETER = 6.00 FEET JA = .739									
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX,V)									
HARMONIC	1	2	3	4	5	6	7	8	
RADIUS = .312									
AMPLITUDE =	.1301	.0683	.0114	.0375	.0243	.0205	.0244	.0219	
PHASE ANGLE =	180.1	280.7	143.9	286.4	62.6	88.5	36.0	167.7	
RADIUS = .350									
AMPLITUDE =	.1354	.0689	.0083	.0349	.0222	.0131	.0239	.0165	
PHASE ANGLE =	180.9	278.4	150.0	281.6	48.7	87.8	27.7	156.2	
RADIUS = .400									
AMPLITUDE =	.1414	.0691	.0061	.0425	.0210	.0043	.0236	.0115	
PHASE ANGLE =	181.9	275.9	167.5	276.5	32.2	85.7	18.4	134.9	
RADIUS = .500									
AMPLITUDE =	.1506	.0673	.0049	.0453	.0194	.0100	.0221	.0075	
PHASE ANGLE =	183.2	272.0	195.1	269.6	10.0	267.3	5.1	79.4	
RADIUS = .600									
AMPLITUDE =	.1559	.0621	.0133	.0442	.0140	.0202	.0182	.0053	
PHASE ANGLE =	183.9	269.6	190.5	244.5	359.1	264.7	356.8	16.0	
RADIUS = .700									
AMPLITUDE =	.1554	.0508	.0349	.0354	.0227	.0259	.0077	.0135	
PHASE ANGLE =	184.6	268.2	179.6	253.0	129.8	259.2	356.5	272.7	
RADIUS = .800									
AMPLITUDE =	.1556	.0427	.0534	.0312	.0139	.0282	.0014	.0237	
PHASE ANGLE =	183.9	268.9	178.4	255.0	161.7	257.9	359.1	260.7	
RADIUS = .900									
AMPLITUDE =	.1589	.0407	.0520	.0314	.0167	.0271	.0024	.0248	
PHASE ANGLE =	181.5	272.6	181.9	255.9	162.6	261.6	341.4	256.1	
RADIUS = 1.000									
AMPLITUDE =	.1627	.428	.0438	.0342	.0139	.0249	.0068	.0206	
PHASE ANGLE =	179.2	276.1	188.0	259.6	161.1	267.1	344.4	253.0	

TABLE F-4 (Continued)

VELOCITY COMPONENT RATIOS FOR 52' BASS BOAT ONLY ON C 4.5MNTSW014									
PROPELLER DIAMETER = 6.00 FEET JA = .739									
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	=	9	.10	.11	.12	.13	.14	.15	.16
RADIUS = .312									
AMPLITUDE = .0315		.0306	.0167	.0059	.0342	.0086	.0169	.0071	
PHASE ANGLE = 66.2		63.3	60.3	51.2	319.8	206.3	341.3	96.5	
RADIUS = .350									
AMPLITUDE = .0215		.0231	.0130	.0037	.0233	.0049	.0114	.0039	
PHASE ANGLE = 80.6		72.3	67.5	52.2	319.8	203.3	340.6	99.9	
RADIUS = .400									
AMPLITUDE = .0112		.0163	.0067	.0021	.0114	.0010	.0053	.0007	
PHASE ANGLE = 62.1		51.2	41.8	32.7	320.2	173.6	337.7	141.8	
RADIUS = .500									
AMPLITUDE = .0098		.0122	.0039	.0015	.0042	.0044	.0027	.0032	
PHASE ANGLE = 325.1		44.6	42.6	32.0	132.8	39.3	178.0	257.4	
RADIUS = .600									
AMPLITUDE = .0154		.0048	.0019	.0019	.0086	.0055	.0048	.0029	
PHASE ANGLE = 310.7		63.2	22.5	82.2	131.1	39.4	176.6	243.8	
RADIUS = .700									
AMPLITUDE = .0118		.0059	.0014	.0010	.0041	.0013	.0027	.0057	
PHASE ANGLE = 341.6		272.1	315.5	71.7	3.3	95.2	284.8	125.2	
RADIUS = .800									
AMPLITUDE = .0117		.0159	.0019	.0005	.0131	.0034	.0073	.0019	
PHASE ANGLE = 9.6		257.8	334.7	290.8	337.2	183.1	323.9	108.6	
RADIUS = .900									
AMPLITUDE = .0109		.0154	.0135	.0074	.0149	.0035	.0090	.0087	
PHASE ANGLE = 1.6		253.4	347.9	264.1	336.4	179.2	338.2	85.7	
RADIUS = 1.000									
AMPLITUDE = .0110		.0096	.0160	.0097	.0122	.0023	.0086	.0073	
PHASE ANGLE = 336.1		247.1	355.5	255.1	339.5	151.4	350.8	49.3	

TABLE F-5 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 14

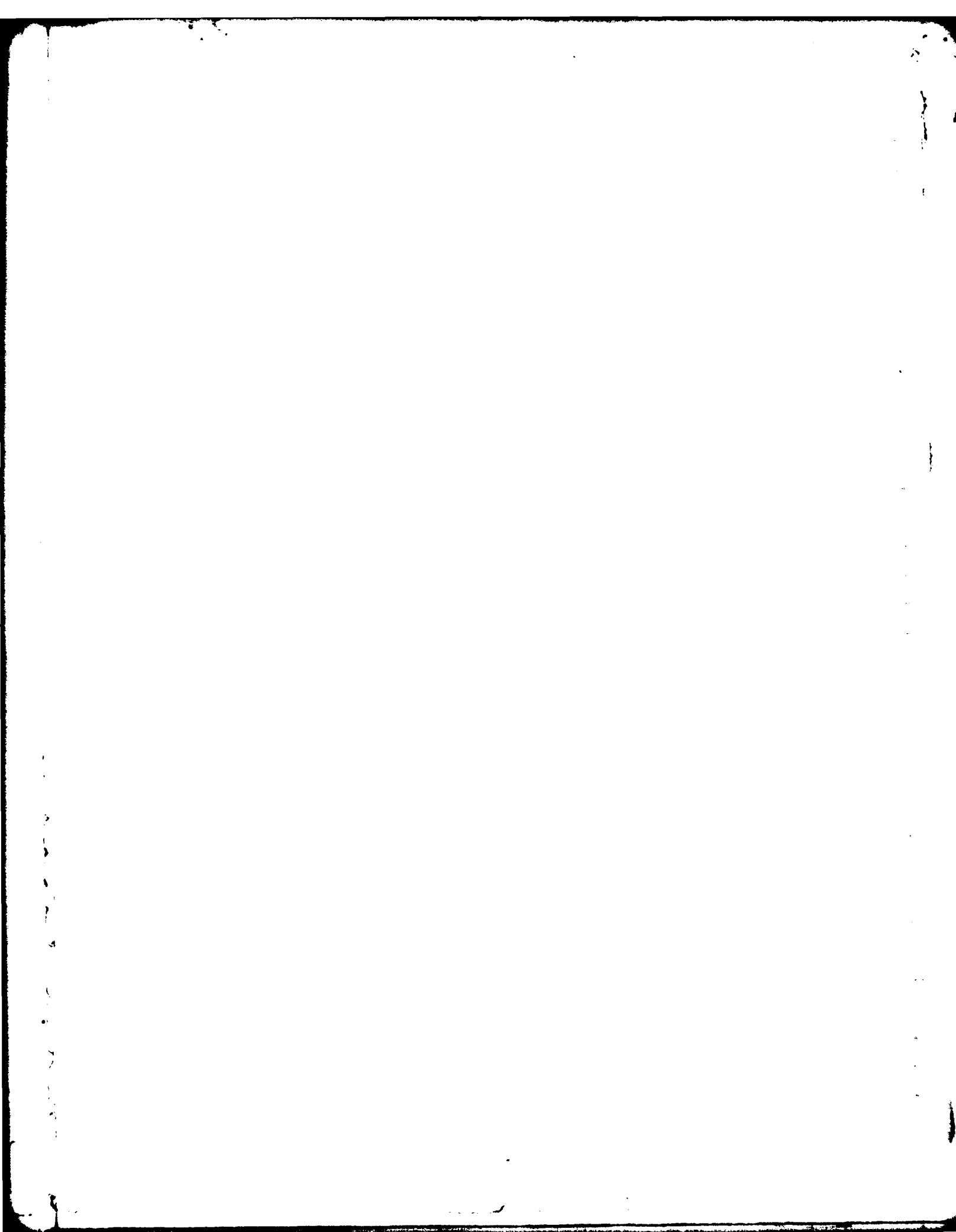
VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY ONIC 4.5XTSW014 PROPELLER DIAMETER = 6.00 FEET JA = .739									
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .456									
AMPLITUDE = .0043		.0044	.0044	.0044	.0044	.0061	.0026	.0096	.0045
PHASE ANGLE = 345.3		2.5.3	2.5.3	2.5.3	2.5.3	2.6.6	2.8.5	2.8.1	17.3
RADIUS = .633									
AMPLITUDE = .00425		.0032	.0032	.0032	.0032	.0073	.0067	.0071	.0005
PHASE ANGLE = 346.2		3.4.2	3.4.2	3.4.2	3.4.2	6.5.3	16.5.5	25.6.3	235.3
RADIUS = .781									
AMPLITUDE = .00428		.00374	.00374	.00374	.00374	.0058	.0054	.0060	.0068
PHASE ANGLE = 338.5		3.4.3	3.4.3	3.4.3	3.4.3	15.9.1	84.0	173.6	190.4
RADIUS = .963									
AMPLITUDE = .0043		.00323	.00323	.00323	.00323	.0021	.0083	.0007	.0056
PHASE ANGLE = 335.6		323.1	323.1	323.1	323.1	62.0	350.7	175.7	288.2
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .456									
AMPLITUDE = .0043		.0057	.0024	.0065	.0005	.0011	.0019	.0010	.0010
PHASE ANGLE = 278.4		18.1	23.6	338.1	163.0	192.3	69.1	126.9	
RADIUS = .633									
AMPLITUDE = .0062		.0042	.0015	.0057	.0047	.0031	.0057	.0022	
PHASE ANGLE = 240.4		3.42.5	1.93.8	3.50.2	50.8	314.9	76.8	172.5	
RADIUS = .781									
AMPLITUDE = .0028		.0049	.0047	.0010	.0052	.0003	.0035	.0034	
PHASE ANGLE = 268.6		178.7	2.5.9	1.42.1	260.1	48.1	239.7	13.9	
RADIUS = .963									
AMPLITUDE = .0057		.0049	.0030	.0029	.0048	.0038	.0070	.0026	
PHASE ANGLE = 262.4		161.8	2.1.1	1.41.9	256.2	12.5	262.5	338.6	

TABLE F-6 - HARMONIC ANALYSIS OF TANGENTIAL VELOCITY CONVERSION RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 14

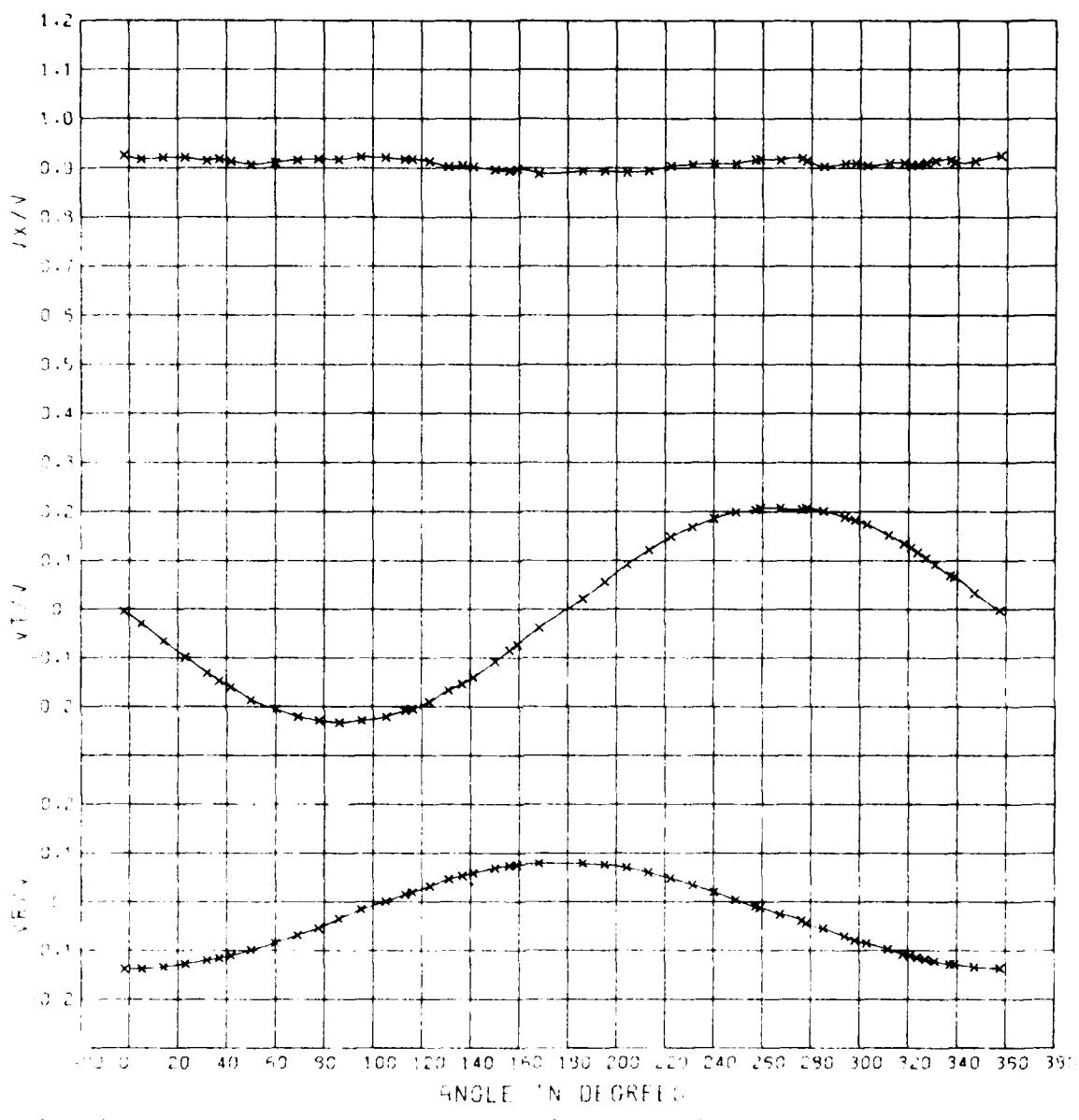
HARMONIC ANALYSES OF TANGENTIAL VELOCITY CONVERSION RATIOS (INT. V)							
	1	2	3	4	5	6	7
RADIUS = .312							
AMPLITUDE = .0612	.0087	.0017	.0113	.0133	.0074	.0083	.0090
PHASE ANGLE = 349.9	200.5	201.7	142.6	311.2	317.8	293.5	48.7
RADIUS = .350							
AMPLITUDE = .0575	.0076	.0015	.0114	.0111	.0049	.0087	.0076
PHASE ANGLE = 348.8	202.8	143.1	154.8	307.3	309.0	284.1	41.2
RADIUS = .400							
AMPLITUDE = .0533	.0060	.0028	.0119	.0086	.0025	.0093	.0060
PHASE ANGLE = 347.2	207.3	103.3	167.2	301.5	277.4	275.1	30.3
RADIUS = .500							
AMPLITUDE = .0469	.0033	.0054	.0128	.0044	.0039	.0095	.0035
PHASE ANGLE = 343.9	222.6	84.6	161.4	285.9	186.3	264.0	6.7
RADIUS = .600							
AMPLITUDE = .0431	.0026	.0017	.0120	.0011	.0063	.0080	.0009
PHASE ANGLE = 341.0	295.8	82.6	85.1	242.9	173.2	257.2	327.3
RADIUS = .700							
AMPLITUDE = .0430	.0053	.0013	.0042	.0036	.0051	.0032	.0040
PHASE ANGLE = 339.5	336.4	142.4	141.3	91.7	172.5	249.4	162.5
RADIUS = .800							
AMPLITUDE = .0426	.0078	.0057	.0052	.0055	.0061	.0005	.0071
PHASE ANGLE = 338.3	343.1	81.8	155.9	82.4	173.9	140.0	161.4
RADIUS = .900							
AMPLITUDE = .0407	.0090	.0057	.0030	.0035	.0071	.0037	.0071
PHASE ANGLE = 336.8	336.6	81.6	151.9	64.3	175.2	82.5	166.3
RADIUS = 1.000							
AMPLITUDE = .0388	.0093	.0059	.0021	.0020	.0083	.0007	.0056
PHASE ANGLE = 335.6	328.1	82.0	180.1	350.7	175.7	288.2	175.2

TABLE F-6 (Continued)

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (V _T /V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .312	=	.0095	.0081	.0062	.0034	.0178	.0099	.0130	.0074
AMPLITUDE =		.3	96.5	357.7	281.6	236.1	147.9	255.2	17.0
PHASE ANGLE =									
RADIUS = .350	=	.0068	.0062	.0043	.0040	.0119	.0070	.0081	.0048
AMPLITUDE =		348.2	76.9	2.8	310.0	235.0	150.2	255.9	21.1
PHASE ANGLE =									
RADIUS = .400	=	.0045	.0053	.0042	.0054	.0256	.0038	.0027	.0021
AMPLITUDE =		319.5	45.4	12.2	328.6	231.7	156.8	258.9	36.6
PHASE ANGLE =									
RADIUS = .500	=	.0051	.0050	.0014	.0070	.0028	.0013	.0043	.0019
AMPLITUDE =		258.3	5.1	55.5	342.5	64.6	263.2	72.9	163.2
PHASE ANGLE =									
RADIUS = .600	=	.0063	.0052	.0012	.0014	.0052	.0030	.0062	.0026
AMPLITUDE =		241.7	347.8	10.5	349.5	54.5	312.5	75.6	173.6
PHASE ANGLE =									
RADIUS = .700	=	.0039	.0012	.0023	.0024	.0021	.0012	.0012	.0012
AMPLITUDE =		250.4	211.5	213.2	213.3	239.5	210.7	116.7	36.9
PHASE ANGLE =									
RADIUS = .800	=	.0028	.0054	.0050	.0015	.0017	.0005	.0043	.0037
AMPLITUDE =		271.7	177.1	257.3	165.1	258.7	57.4	243.1	11.9
PHASE ANGLE =									
RADIUS = .900	=	.0039	.0062	.0010	.0030	.0070	.0020	.0067	.0037
AMPLITUDE =		270.5	170.1	251.0	155.8	255.8	27.6	254.3	359.3
PHASE ANGLE =									
RADIUS = 1.000	=	.0057	.0049	.0050	.0029	.0048	.0038	.0070	.0026
AMPLITUDE =		262.4	161.8	261.7	154.9	256.2	12.5	262.5	338.6
PHASE ANGLE =									

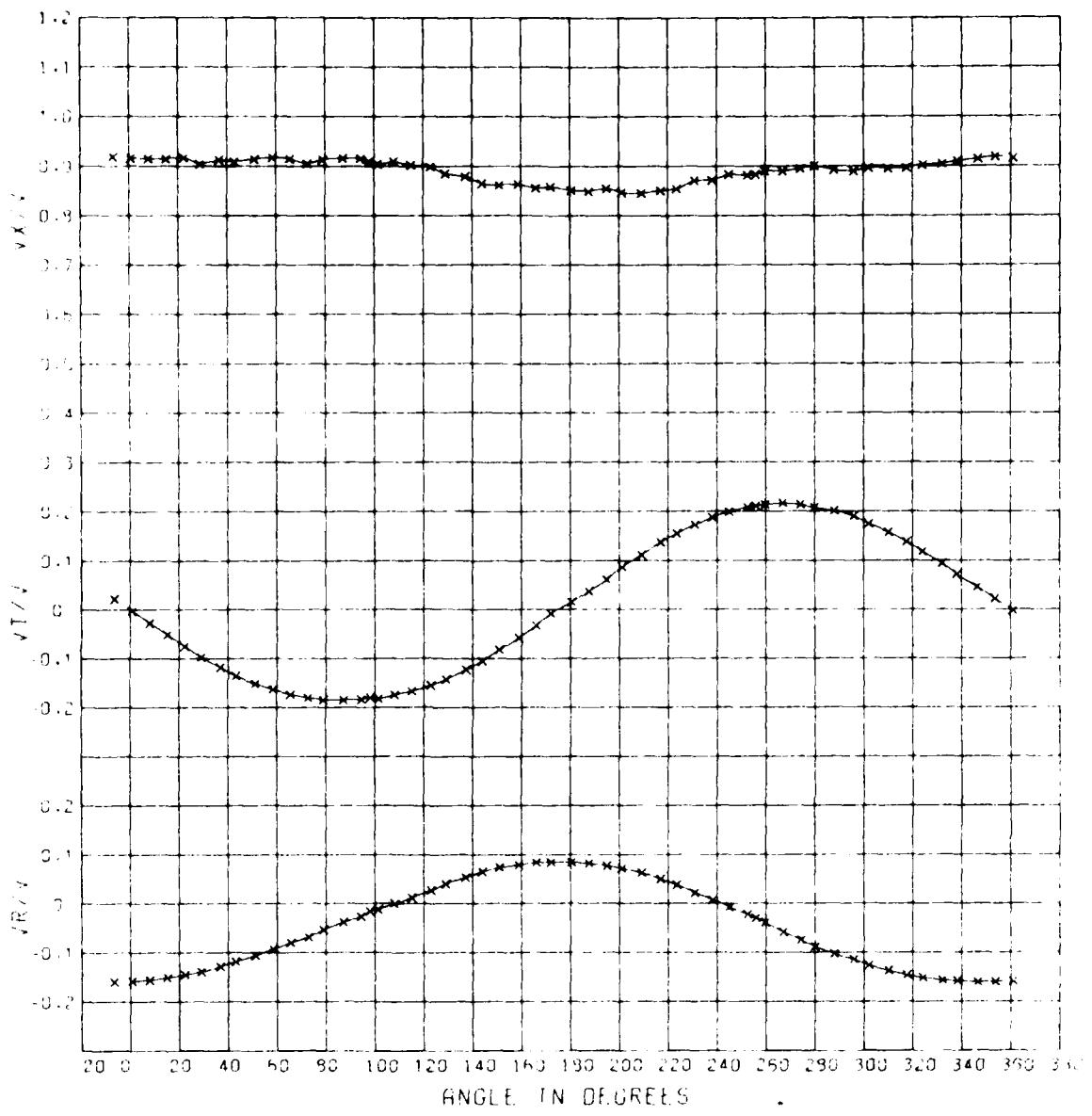


APPENDIX G
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENT 15



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC 6KTG015
0.456 RHD.

Figure G-1 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.456
for Experiment 15



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 TNC 5KT5W015
0.633 RHD.

Figure G-2 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.633
for Experiment 15

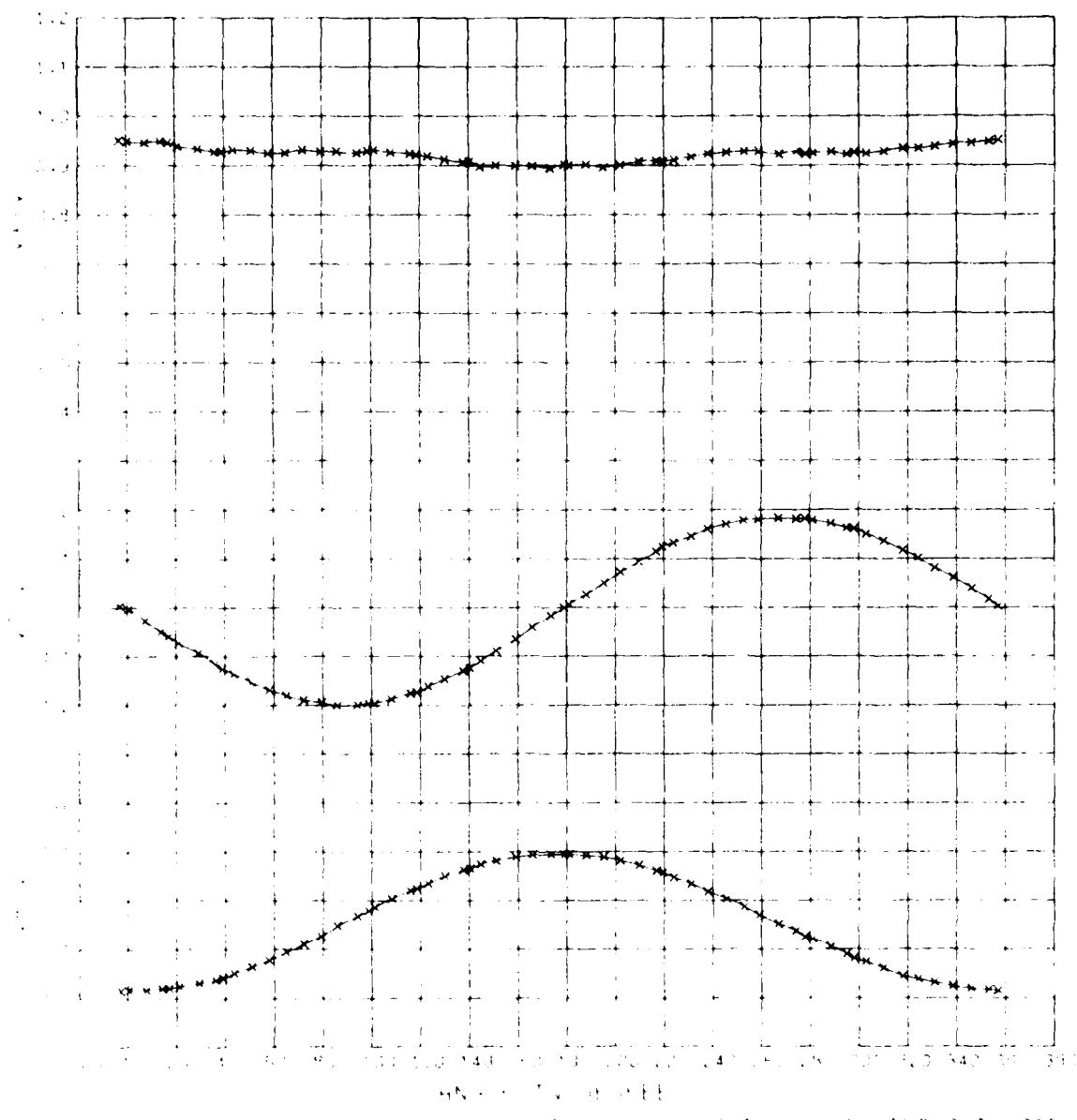
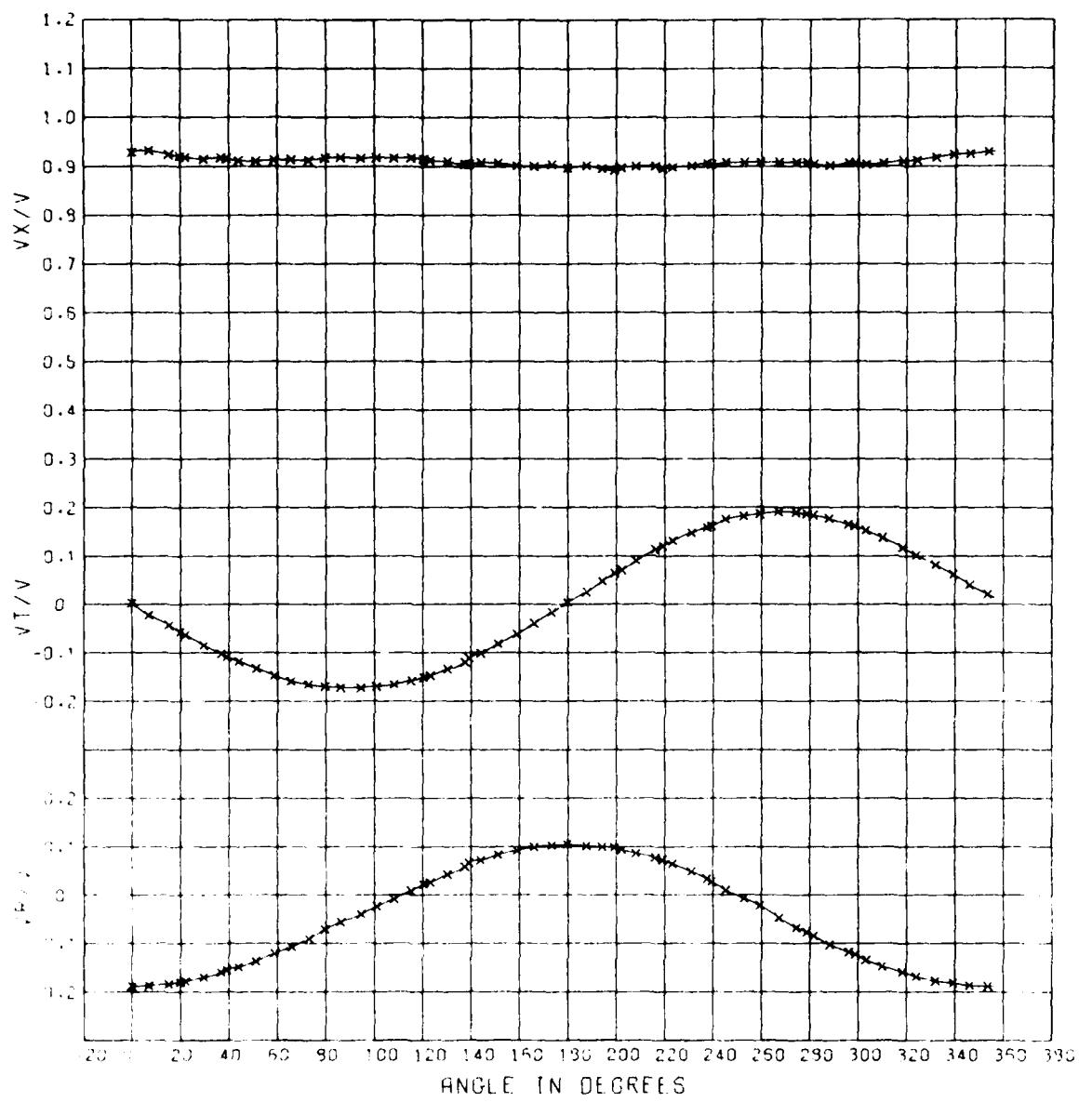


Figure G-3 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.781 for Experiment 15



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC 6KTSWG15
0.963 RAD.

Figure G-4 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.963 for Experiment 15

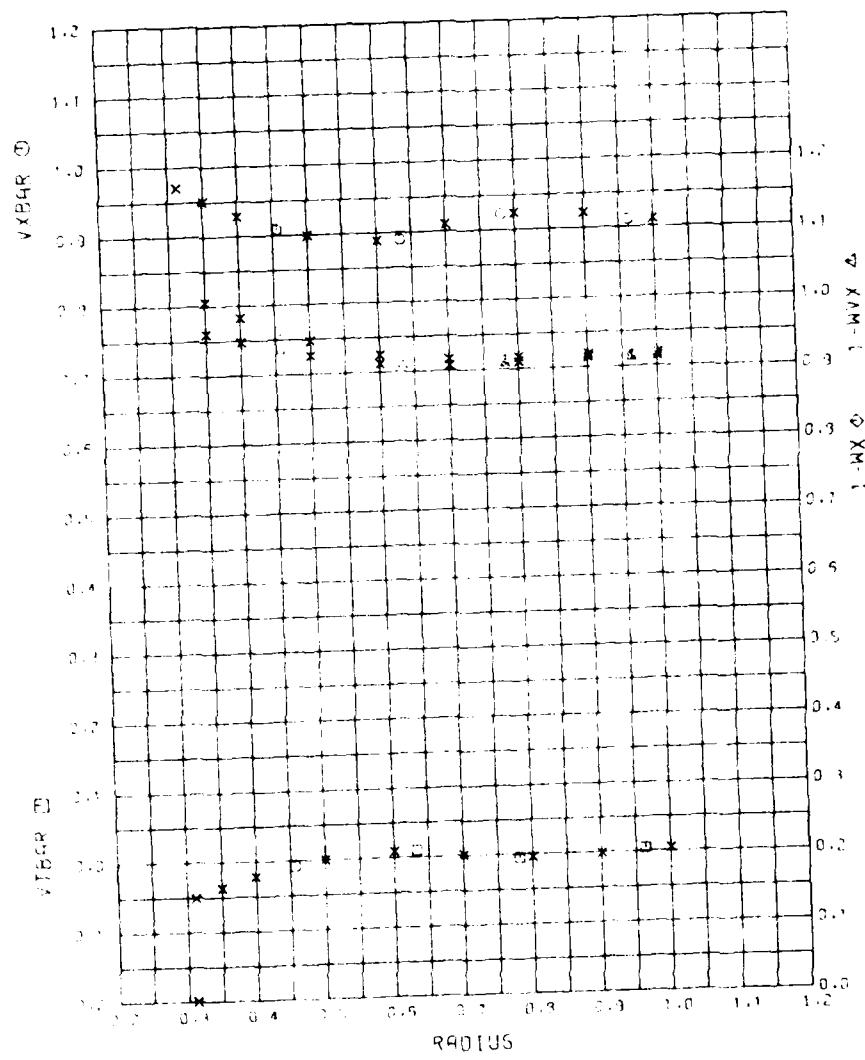


Figure G-5 - Radial Distribution of the Mean Velocity Component Ratios
for Experiment 15

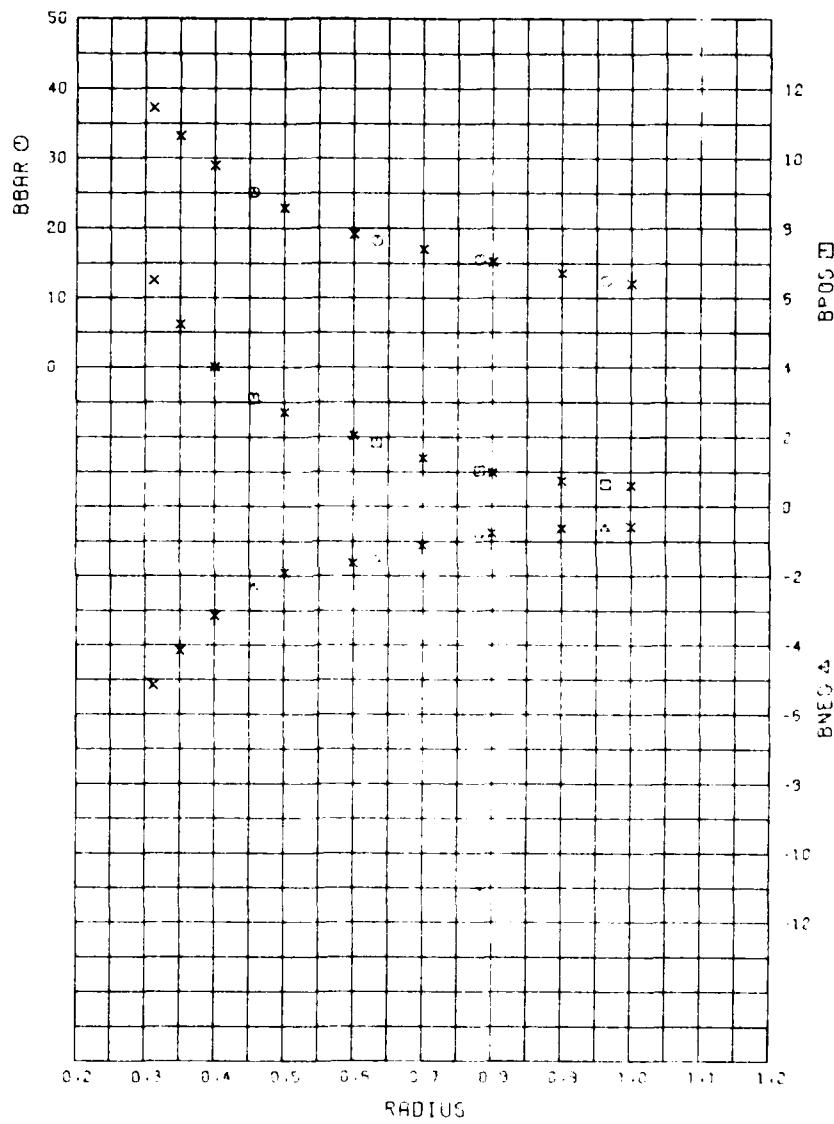


Figure G-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 15

TABLE G-1

INPUT DATA FOR HARMONIC ANALYSIS FOR R/V ATHENA
WITH BASS DYNAMOMETER BOAT, EXPERIMENT 15

RADIUS *	ANGLE	FOCUS *	ANGLE	RADIUS *	ANGLE	FOCUS *	ANGLE	RADIUS *	ANGLE	FOCUS *	ANGLE
.919	.110	.117	.115	.919	.022	.116	.010	.911	.011	.116	.003
.919	.110	.117	.116	.916	.002	.116	.000	.907	.002	.116	.000
.921	.095	.116	.116	.915	.029	.116	.016	.906	.027	.116	.022
.921	.095	.117	.117	.915	.051	.116	.040	.906	.050	.117	.037
.919	.095	.117	.118	.914	.076	.116	.065	.906	.075	.117	.063
.919	.095	.117	.119	.914	.096	.116	.085	.906	.095	.117	.083
.919	.095	.117	.120	.914	.116	.116	.105	.906	.115	.117	.090
.919	.095	.117	.121	.914	.136	.116	.125	.906	.135	.117	.105
.919	.095	.117	.122	.914	.156	.116	.145	.906	.155	.117	.125
.919	.095	.117	.123	.914	.176	.116	.165	.906	.175	.117	.145
.919	.095	.117	.124	.914	.196	.116	.185	.906	.195	.117	.165
.919	.095	.117	.125	.914	.216	.116	.205	.906	.215	.117	.185
.919	.095	.117	.126	.914	.236	.116	.225	.906	.235	.117	.205
.919	.095	.117	.127	.914	.256	.116	.245	.906	.255	.117	.225
.919	.095	.117	.128	.914	.276	.116	.265	.906	.275	.117	.245
.919	.095	.117	.129	.914	.296	.116	.285	.906	.295	.117	.265
.919	.095	.117	.130	.914	.316	.116	.305	.906	.315	.117	.285
.919	.095	.117	.131	.914	.336	.116	.325	.906	.335	.117	.305
.919	.095	.117	.132	.914	.356	.116	.345	.906	.355	.117	.325
.919	.095	.117	.133	.914	.376	.116	.365	.906	.375	.117	.345
.919	.095	.117	.134	.914	.396	.116	.385	.906	.395	.117	.365
.919	.095	.117	.135	.914	.416	.116	.405	.906	.415	.117	.385
.919	.095	.117	.136	.914	.436	.116	.425	.906	.435	.117	.405
.919	.095	.117	.137	.914	.456	.116	.445	.906	.455	.117	.425
.919	.095	.117	.138	.914	.476	.116	.465	.906	.475	.117	.445
.919	.095	.117	.139	.914	.496	.116	.485	.906	.495	.117	.465
.919	.095	.117	.140	.914	.516	.116	.505	.906	.515	.117	.485
.919	.095	.117	.141	.914	.536	.116	.525	.906	.535	.117	.505
.919	.095	.117	.142	.914	.556	.116	.545	.906	.555	.117	.525
.919	.095	.117	.143	.914	.576	.116	.565	.906	.575	.117	.545
.919	.095	.117	.144	.914	.596	.116	.585	.906	.595	.117	.565
.919	.095	.117	.145	.914	.616	.116	.605	.906	.615	.117	.585
.919	.095	.117	.146	.914	.636	.116	.625	.906	.635	.117	.605
.919	.095	.117	.147	.914	.656	.116	.645	.906	.655	.117	.625
.919	.095	.117	.148	.914	.676	.116	.665	.906	.675	.117	.645
.919	.095	.117	.149	.914	.696	.116	.685	.906	.695	.117	.665
.919	.095	.117	.150	.914	.716	.116	.705	.906	.715	.117	.685
.919	.095	.117	.151	.914	.736	.116	.725	.906	.735	.117	.705
.919	.095	.117	.152	.914	.756	.116	.745	.906	.755	.117	.725
.919	.095	.117	.153	.914	.776	.116	.765	.906	.775	.117	.745
.919	.095	.117	.154	.914	.796	.116	.785	.906	.795	.117	.765
.919	.095	.117	.155	.914	.816	.116	.805	.906	.815	.117	.785
.919	.095	.117	.156	.914	.836	.116	.825	.906	.835	.117	.805
.919	.095	.117	.157	.914	.856	.116	.845	.906	.855	.117	.825
.919	.095	.117	.158	.914	.876	.116	.865	.906	.875	.117	.845
.919	.095	.117	.159	.914	.896	.116	.885	.906	.895	.117	.865
.919	.095	.117	.160	.914	.916	.116	.905	.906	.915	.117	.885
.919	.095	.117	.161	.914	.936	.116	.925	.906	.935	.117	.905
.919	.095	.117	.162	.914	.956	.116	.945	.906	.955	.117	.925
.919	.095	.117	.163	.914	.976	.116	.965	.906	.975	.117	.945
.919	.095	.117	.164	.914	.996	.116	.985	.906	.995	.117	.965
.919	.095	.117	.165	.914	.1016	.116	.1005	.906	.1015	.117	.985
.919	.095	.117	.166	.914	.1036	.116	.1025	.906	.1035	.117	.1005
.919	.095	.117	.167	.914	.1056	.116	.1045	.906	.1055	.117	.1025
.919	.095	.117	.168	.914	.1076	.116	.1065	.906	.1075	.117	.1045
.919	.095	.117	.169	.914	.1096	.116	.1085	.906	.1095	.117	.1065
.919	.095	.117	.170	.914	.1116	.116	.1105	.906	.1115	.117	.1085
.919	.095	.117	.171	.914	.1136	.116	.1125	.906	.1135	.117	.1105
.919	.095	.117	.172	.914	.1156	.116	.1145	.906	.1155	.117	.1125
.919	.095	.117	.173	.914	.1176	.116	.1165	.906	.1175	.117	.1145
.919	.095	.117	.174	.914	.1196	.116	.1185	.906	.1195	.117	.1165
.919	.095	.117	.175	.914	.1216	.116	.1205	.906	.1215	.117	.1185
.919	.095	.117	.176	.914	.1236	.116	.1225	.906	.1235	.117	.1205
.919	.095	.117	.177	.914	.1256	.116	.1245	.906	.1255	.117	.1225
.919	.095	.117	.178	.914	.1276	.116	.1265	.906	.1275	.117	.1245
.919	.095	.117	.179	.914	.1296	.116	.1285	.906	.1295	.117	.1265
.919	.095	.117	.180	.914	.1316	.116	.1305	.906	.1315	.117	.1285
.919	.095	.117	.181	.914	.1336	.116	.1325	.906	.1335	.117	.1305
.919	.095	.117	.182	.914	.1356	.116	.1345	.906	.1355	.117	.1325
.919	.095	.117	.183	.914	.1376	.116	.1365	.906	.1375	.117	.1345
.919	.095	.117	.184	.914	.1396	.116	.1385	.906	.1395	.117	.1365
.919	.095	.117	.185	.914	.1416	.116	.1405	.906	.1415	.117	.1385
.919	.095	.117	.186	.914	.1436	.116	.1425	.906	.1435	.117	.1405
.919	.095	.117	.187	.914	.1456	.116	.1445	.906	.1455	.117	.1425
.919	.095	.117	.188	.914	.1476	.116	.1465	.906	.1475	.117	.1445
.919	.095	.117	.189	.914	.1496	.116	.1485	.906	.1495	.117	.1465
.919	.095	.117	.190	.914	.1516	.116	.1505	.906	.1515	.117	.1485
.919	.095	.117	.191	.914	.1536	.116	.1525	.906	.1535	.117	.1505
.919	.095	.117	.192	.914	.1556	.116	.1545	.906	.1555	.117	.1525
.919	.095	.117	.193	.914	.1576	.116	.1565	.906	.1575	.117	.1545
.919	.095	.117	.194	.914	.1596	.116	.1585	.906	.1595	.117	.1565
.919	.095	.117	.195	.914	.1616	.116	.1605	.906	.1615	.117	.1585
.919	.095	.117	.196	.914	.1636	.116	.1625	.906	.1635	.117	.1605
.919	.095	.117	.197	.914	.1656	.116	.1645	.906	.1655	.117	.1625
.919	.095	.117	.198	.914	.1676	.116	.1665	.906	.1675	.117	.1645
.919	.095	.117	.199	.914	.1696	.116	.1685	.906	.1695	.117	.1665
.919	.095	.117	.200	.914	.1716	.116	.1705	.906	.1715	.117	.1685
.919	.095	.117	.201	.914	.1736	.116	.1725	.906	.1735	.117	.1705
.919	.095	.117	.202	.914	.1756	.116	.1745	.906	.1755	.117	.1725
.919	.095	.117	.203	.914	.1776	.116	.1765	.906	.1775	.117	.1745
.919	.095	.117	.204	.914	.1796	.116	.1785	.906	.1795	.117	.1765
.919	.095	.117	.205	.914	.1816	.116	.1805	.906	.1815	.117	.1785
.919	.095	.117	.206	.914	.1836	.116	.1825	.906	.1835	.117	.1805
.919	.095	.117	.207	.914	.1856	.116	.1845	.906	.1855	.117	.1825
.919	.095	.117	.208	.914	.1876	.116	.1865	.906	.1875	.117	.1845
.919	.095	.117	.209	.914	.1896	.116	.1885	.906	.1895	.117	.1865
.919	.095	.117	.210	.914	.1916	.116	.1905	.906	.1915	.117	.1885
.919	.095	.117	.211	.914	.1936	.116	.1925	.906	.1935	.117	.1905
.919	.095	.117	.212	.914	.1956	.116	.1945	.906	.1955	.117	.1925
.919	.095	.117	.213	.914	.1976	.116	.1965	.906	.1975	.117	.1945
.919	.095	.117	.214	.914	.1996	.116	.1985	.906	.1995	.117	.1965
.919	.095	.117	.215	.914	.2016	.116	.2005	.906	.2015	.117	.1985
.919	.095	.117	.216	.914	.2036	.116	.2025	.906	.2035	.117	.2005
.919	.095	.117	.217	.914	.2056	.116	.2045	.906	.2055	.117	.2025
.919	.095	.117	.218	.914	.2076	.116	.2065	.906	.2075	.117	.2045
.919	.095	.117	.219	.914	.2096	.11					

TABLE G-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 15

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC 6KTSW015
PROPELLER DIAMETER = 6.00 FEET

RADIUS = .456	.633	.781	.563	.312	.350	.400	.500	.600	.700	.800	.900	1.000
VXBAR = .909	.890	.923	.911	.971	.951	.928	.899	.889	.910	.924	.922	.911
VTBAR = -.008	.010	-.004	.005	-.051	-.037	-.022	-.000	.009	.001	-.004	-.001	.005
VRBAR = -.028	-.043	-.047	-.047	-.008	-.014	-.022	-.033	-.041	-.045	-.047	-.047	-.047
1-WVX = .934	.909	.908	.912	0.000	.960	.947	.926	.912	.907	.910	.914	.914
1-WX = .963	.921	.914	.917	0.000	1.006	.982	.947	.925	.916	.917	.919	.919
BBAR = 25.21	18.24	15.55	2.52	37.26	33.22	28.93	22.91	19.14	16.99	15.22	13.54	12.07
BBR5 = 3.11	1.85	1.03	.65	.65	.5.51	5.23	4.01	2.71	2.04	1.39	.98	.61
THETA = 95.00	90.00	100.00	92.00	100.00	100.00	100.00	92.50	90.00	85.00	102.50	102.50	85.00
BNEG = -2.34	-1.53	-.8C	-.62	-.62	-.4.16	-.3.15	-.1.91	-.1.64	-.1.12	-.76	-.63	-.58
THETA = 285.00	222.50	267.50	287.50	282.50	282.50	285.00	250.00	222.50	220.00	267.50	280.00	287.50

149

VXBAR IS CIRCUMFERNCE, MEAN CIRCUMFERENTIAL VELOCITY.
VTBAR IS CIRCUMFERNCE, MEAN TANGENTIAL VELOCITY.
VRBAR IS CIRCUMFERNCE, MEAN TOTAL VELOCITY.
1-WVX IS CIRCUMFERNCE, MEAN ADVANCE ANGLE WITHOUT TANGENTIAL CORRECTION.
1-WX IS CIRCUMFERNCE, MEAN ADVANCE ANGLE WITH TANGENTIAL CORRECTION.
BBAR IS MEAN ANGLE OF ADVANCE.
BBR5 IS VARIATION BETWEEN THE MAXIMUM AND MEAN ADVANCE ANGLES (DELTA BETA PLUS).
BNEG IS VARIATION BETWEEN THE MINIMUM AND MEAN ADVANCE ANGLES (DELTA BETA MINUS).
THETA IS ANGLE IN DEGREES AT WHICH CORRESPONDING BPOS OR BNEG OCCURS.

TABLE G-3 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 15

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY IN GTSW015
PROPELLER DIAMETER = 6.00 FEET
 $JA = .739$

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .456	=	.0099	.0059	.0053	.0027	.0010	.0008	.0007	.0006
AMPLITUDE =			274.9	87.3	78.8	291.9	305.3	351.0	82.8
PHASE ANGLE =		73.0							
RADIUS = .633	=	.0304	.0102	.0048	.0040	.0017	.0022	.0004	.0009
AMPLITUDE =			259.3	83.5	102.6	237.0	111.8	280.8	21.3
PHASE ANGLE =		68.2							
RADIUS = .781	=	.0187	.0030	.0071	.0029	.0006	.0014	.0006	.0003
AMPLITUDE =			283.9	105.6	98.7	279.3	88.9	12.8	330.7
PHASE ANGLE =		91.4							
RADIUS = .963	=	.0103	.0012	.0051	.0034	.0001	.0004	.0007	.0002
AMPLITUDE =			147.8	94.7	107.0	159.4	102.5	68.0	175.8
PHASE ANGLE =		62.8							
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .456	=	.0019	.0007	.0001	.0005	.0007	.0007	.0007	.0006
AMPLITUDE =			396.1	73.2	46.5	146.4	205.6	151.4	81.7
PHASE ANGLE =		180.6							
RADIUS = .633	=	.0008.	.0020	.0009	.0003	.0010	.0004	.0011	.0009
AMPLITUDE =			261.1	195.5	149.3	60.4	239.8	211.8	164.1
PHASE ANGLE =		78.3							
RADIUS = .781	=	.0006	.0004	.0010	.0007	.0012	.0007	.0006	.0005
AMPLITUDE =			75.0	270.7	294.0	211.0	72.1	172.7	34.0
PHASE ANGLE =		27.5							
RADIUS = .963	=	.0003	.0007	.0004	.0012	.0005	.0005	.0004	.0006
AMPLITUDE =			40.4	311.8	77.8	315.4	324.4	286.7	293.5
PHASE ANGLE =		70.7							

TABLE G-4 - HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 15

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX/V)							
HARMONIC	=	1	2	3	4	5	6
RADIUS = .312							
AMPLITUDE = .0372		.0353	.0301	.0233	.0035	.0064	.0024
PHASE ANGLE = 233.7		47.7	104.2	344.0	13.4	300.8	20.8
RADIUS = .350							
AMPLITUDE = .0223		.0258	.0251	.0243	.0025	.0046	.0019
PHASE ANGLE = 231.6		33.1	152.2	10.1	6.0	300.8	17.0
RADIUS = .400							
AMPLITUDE = .0059		.0031	.0021	.0014	.0014	.0026	.0012
PHASE ANGLE = 212.0		325.5	53.2	43.6	345.0	301.2	8.8
RADIUS = .500							
AMPLITUDE = .0197		.0163	.0163	.0162	.0012	.0012	.0008
PHASE ANGLE = 67.1		21.4	21.4	21.4	21.4	104.4	129.7
RADIUS = .600							
AMPLITUDE = .0295		.0285	.0285	.0285	.0017	.0019	.0005
PHASE ANGLE = 67.0		259.5	76.4	101.3	238.4	112.9	326.7
RADIUS = .700							
AMPLITUDE = .0241		.0254	.0214	.0033	.0011	.0018	.0004
PHASE ANGLE = 86.3		257.6	44.7	100.0	251.8	100.5	341.7
RADIUS = .800							
AMPLITUDE = .0177		.0024	.0072	.0018	.0005	.0013	.0007
PHASE ANGLE = 93.0		264.3	104.0	98.8	266.8	86.8	17.6
RADIUS = .900							
AMPLITUDE = .0122		.0002	.0004	.0030	.0002	.0008	.0007
PHASE ANGLE = 87.8		16.2	103.2	102.9	320.5	82.6	43.6
RADIUS = 1.000							
AMPLITUDE = .0053		.0012	.0053	.0034	.0001	.0024	.0007
PHASE ANGLE = 147.6		64.7	127.0	129.4	102.5	68.0	175.6

TABLE G-4 (Continued)

HARMONIC ANALYSIS OF LONGITUDINAL VELOCITY COMPONENT RATIOS (Vx/V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .312									
AMPLITUDE = .0052		.0060	.0036	.0039	.0043	.0013	.0025	.0035	
PHASE ANGLE = 201.8		63.0	33.5	355.9	207.7	141.0	84.0	34.5	
RADIUS = .350									
AMPLITUDE = .0041		.0042	.0027	.0014	.0030	.0010	.0018	.0025	
PHASE ANGLE = 198.5		59.9	38.4	2.2	203.7	155.6	90.8	38.0	
RADIUS = .400									
AMPLITUDE = .0029		.0021	.0018	.0008	.0016	.0008	.0011	.0014	
PHASE ANGLE = 192.3		50.4	48.7	15.9	192.5	180.2	108.5	47.3	
RADIUS = .500									
AMPLITUDE = .0012		.0011	.0001	.0004	.0007	.0007	.0008	.0005	
PHASE ANGLE = 163.9		216.2	112.7	82.1	99.0	219.7	184.9	142.3	
RADIUS = .600									
AMPLITUDE = .0008		.0020	.0001	.0004	.0011	.0005	.0011	.0009	
PHASE ANGLE = 95.5		263.0	183.4	135.1	60.9	235.9	210.4	182.0	
RADIUS = .700									
AMPLITUDE = .0007		.0006	.0001	.0005	.0005	.0003	.0008	.0002	
PHASE ANGLE = 50.8		260.1	239.3	276.6	179.4	89.1	192.1	117.0	
RADIUS = .800									
AMPLITUDE = .0006		.0006	.0011	.0007	.0013	.0007	.0005	.0006	
PHASE ANGLE = 24.7		74.3	275.4	298.0	213.5	69.5	170.0	28.0	
RADIUS = .900									
AMPLITUDE = .0004		.0009	.0010	.0004	.0009	.0005	.0002	.0006	
PHASE ANGLE = 30.2		63.8	295.2	26.0	231.5	38.1	204.6	348.0	
RADIUS = 1.000									
AMPLITUDE = .0003		.0007	.0008	.0012	.0005	.0005	.0004	.0006	
PHASE ANGLE = 70.7		40.4	314.8	77.8	315.4	324.4	286.7	293.5	

TABLE G-5 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 15

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY INC 6KTSW015 PROPELLER DIAMETER = 6.00 FEET JA = .739									
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .456									
AMPLITUDE =	.2203	.0033	.0018	.0004	.0019	.0006	.0008	.0005	
PHASE ANGLE =	182.2	103.0	32.3	291.2	19.6	169.3	41.8	201.6	
RADIUS = .633									
AMPLITUDE =	.2005	.0040	.0005	.0012	.0004	.0008	.0003		
PHASE ANGLE =	182.3	260.2	45.0	14.8	12.7	153.7	14.2	129.4	
RADIUS = .781									
AMPLITUDE =	.1899	.0039	.0020	.0002	.0008	.0005	.0003	.0004	
PHASE ANGLE =	181.3	71.1	12.6	257.9	31.9	114.6	356.4	162.0	
RADIUS = .963									
AMPLITUDE =	.1799	.0041	.0017	.0008	.0003	.0004	.0002	.0002	
PHASE ANGLE =	180.7	310.9	15.4	86.0	43.6	201.3	81.1	105.2	
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .456									
AMPLITUDE =	.0007	.0004	.0003	.0005	.0002	.0002	.0001	.0003	
PHASE ANGLE =	25.5	166.3	49.5	302.6	312.9	28.0	298.5	153.0	
RADIUS = .633									
AMPLITUDE =	.0006	.0004	.0003	.0007	.0003	.0003	.0003	.0005	
PHASE ANGLE =	334.6	180.5	52.8	149.8	273.2	224.0	344.0	137.1	
RADIUS = .781									
AMPLITUDE =	.0002	.0002	.0001	.0022	.0003	.0002	.0006	.0002	
PHASE ANGLE =	51.4	99.8	250.3	337.5	110.4	79.8	354.8	287.0	
RADIUS = .963									
AMPLITUDE =	.0001	.0005	.0002	.0004	.0006	.0003	.0002	.0002	
PHASE ANGLE =	256.3	59.1	270.8	145.5	94.3	179.7	51.4	134.5	

TABLE G-6 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 15

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY IN GKT SW015
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)

HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .350		.2422	.0223	.0028	.0045	.0027	.0038	.0010	.0016
AMPLITUDE =		181.3	96.6	10.3	292.1	31.2	164.7	91.9	220.7
PHASE ANGLE =									
RADIUS = .400		.2359	.0162	.0021	.0032	.0025	.0027	.0009	.0013
AMPLITUDE =		181.6	97.2	13.1	292.1	28.1	166.8	77.3	218.3
PHASE ANGLE =									
RADIUS = .500		.2282	.0093	.0014	.0017	.0022	.0007	.0008	.0009
AMPLITUDE =		181.9	98.6	19.1	292.1	23.9	168.7	58.7	213.1
PHASE ANGLE =									
RADIUS = .600		.2146	.0004	.0005	.0003	.0017	.0006	.0009	.0004
AMPLITUDE =		182.3	210.1	48.9	114.9	16.6	168.3	32.1	184.6
PHASE ANGLE =									
RADIUS = .700		.2036	.0039	.0005	.0012	.0013	.0005	.0008	.0003
AMPLITUDE =		182.4	277.2	61.1	114.2	12.6	159.4	17.6	135.3
PHASE ANGLE =									
RADIUS = .800		.1954	.0013	.0014	.0003	.0010	.0005	.0006	.0004
AMPLITUDE =		181.8	47.7	18.6	134.8	21.6	125.4	5.6	153.6
PHASE ANGLE =									
RADIUS = .900		.1887	.0041	.0021	.0003	.0007	.0004	.0002	.0004
AMPLITUDE =		181.2	70.2	12.0	266.4	34.1	114.9	355.8	162.1
PHASE ANGLE =									
RADIUS = 1.000		.1830	.0024	.0021	.0001	.0005	.0003	.0001	.0003
AMPLITUDE =		180.8	31.6	10.3	53.1	43.1	147.0	45.8	147.9
PHASE ANGLE =									

TABLE G-6 (Continued)

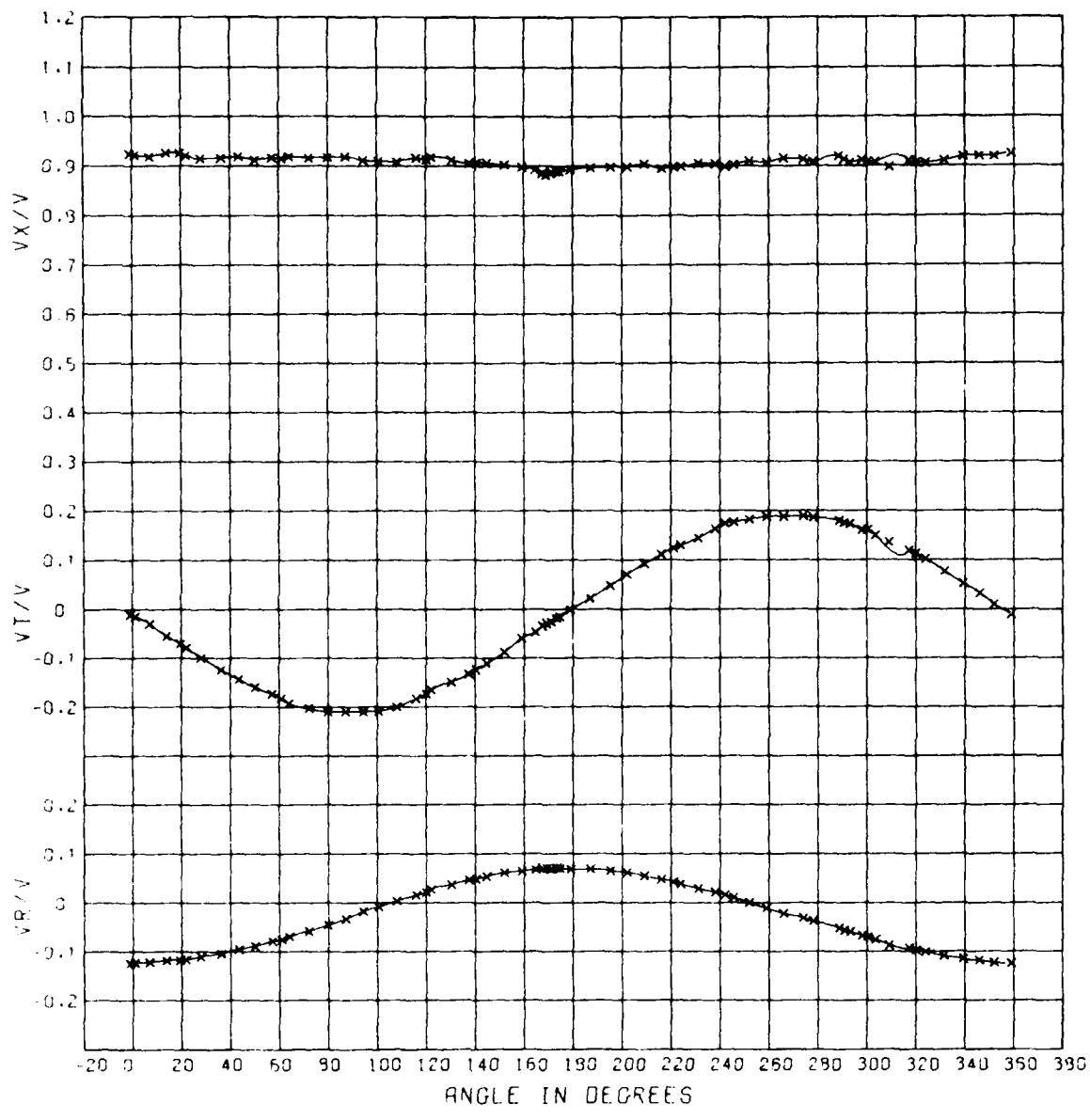
VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC GRITS AND 015
PROPELLER DIAMETER = 6.00 FEET

$\Delta A = .739$

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)

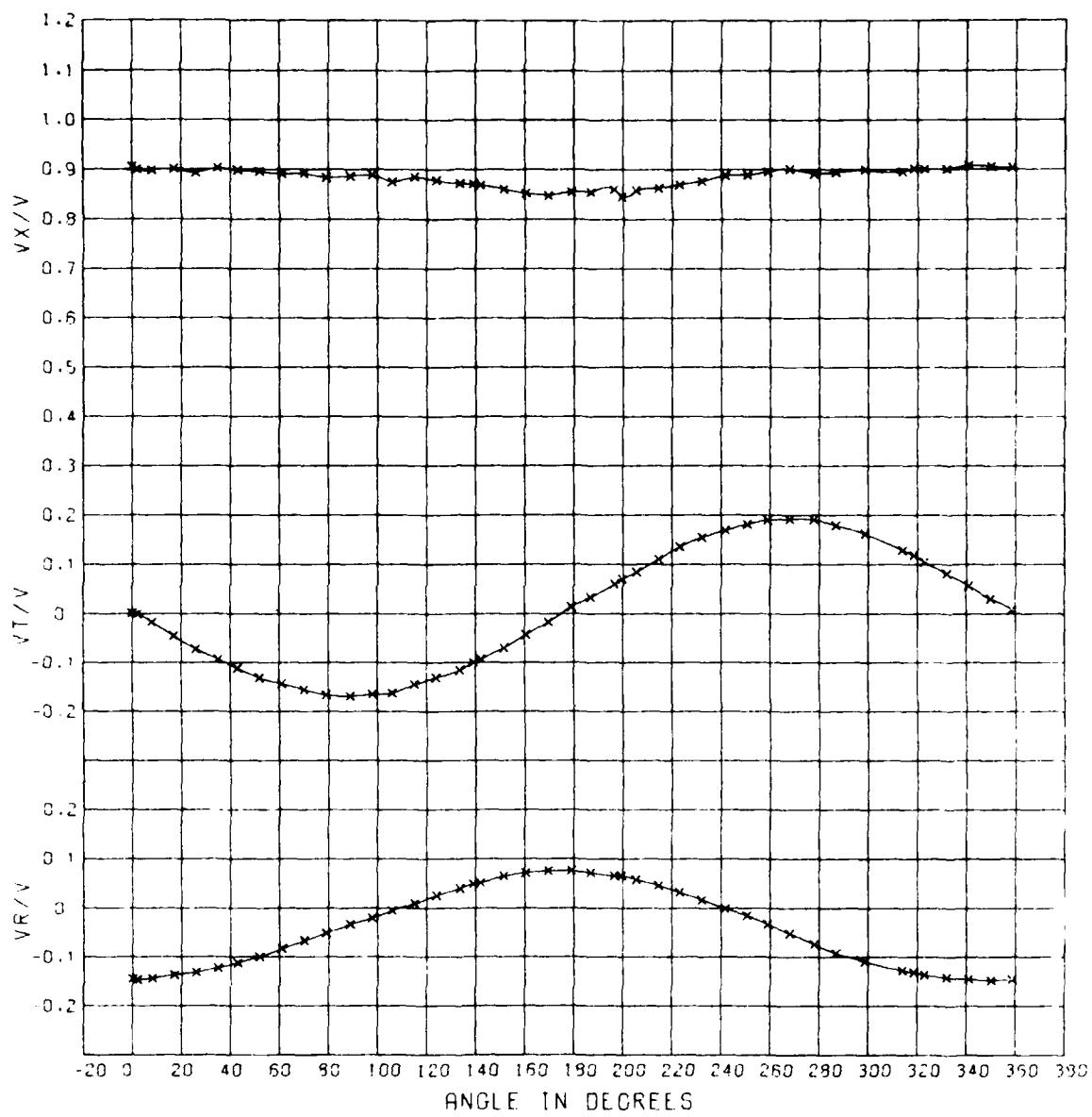
HARMONIC	*	9	10	11	12	13	14	15	16
RADIUS =	.312								
AMPLITUDE =	.0016	.0005	.0001	.0029	.0006	.0014	.0002	.0007	
PHASE ANGLE =	80.3	68.4	284.9	319.5	61.5	41.9	227.9	294.5	
RADIUS =	.350								
AMPLITUDE =	.0012	.0004	.0001	.0021	.0004	.0010	.0001	.0004	
PHASE ANGLE =	71.3	110.3	11.2	318.3	49.0	40.7	241.4	286.4	
RADIUS =	.400								
AMPLITUDE =	.0009	.0004	.0002	.0012	.0002	.0006	.0001	.0001	
PHASE ANGLE =	53.4	142.8	42.5	315.1	9.8	37.8	266.7	235.2	
RADIUS =	.500								
AMPLITUDE =	.0007	.0005	.0003	.0002	.0003	.0001	.0002	.0004	
PHASE ANGLE =	4.3	175.6	51.7	214.1	293.8	307.7	317.3	142.4	
RADIUS =	.600								
AMPLITUDE =	.0007	.0005	.0003	.0006	.0003	.0003	.0003	.0005	
PHASE ANGLE =	338.0	181.9	53.1	151.9	277.3	227.9	339.8	137.0	
RADIUS =	.700								
AMPLITUDE =	.0003	.0003	.0001	.0002	.0001	.0000	.0005	.0001	
PHASE ANGLE =	356.2	148.0	54.4	145.5	181.8	102.8	349.2	170.5	
RADIUS =	.800								
AMPLITUDE =	.0002	.0002	.0002	.0002	.0003	.0002	.0006	.0002	
PHASE ANGLE =	64.3	92.2	251.4	336.5	108.3	85.2	356.6	269.9	
RADIUS =	.900								
AMPLITUDE =	.0001	.0002	.0001	.0001	.0004	.0003	.0004	.0001	
PHASE ANGLE =	112.9	65.4	262.2	346.0	100.4	148.9	14.3	275.2	
RADIUS = 1.000									
AMPLITUDE =	.0001	.0001	.0002	.0004	.0006	.0003	.0003	.0002	
PHASE ANGLE =	256.3	59.1	275.2	145.5	94.3	179.7	51.4	134.5	

APPENDIX H
VELOCITY COMPONENT RATIOS AND HARMONIC ANALYSIS
FOR EXPERIMENT 16



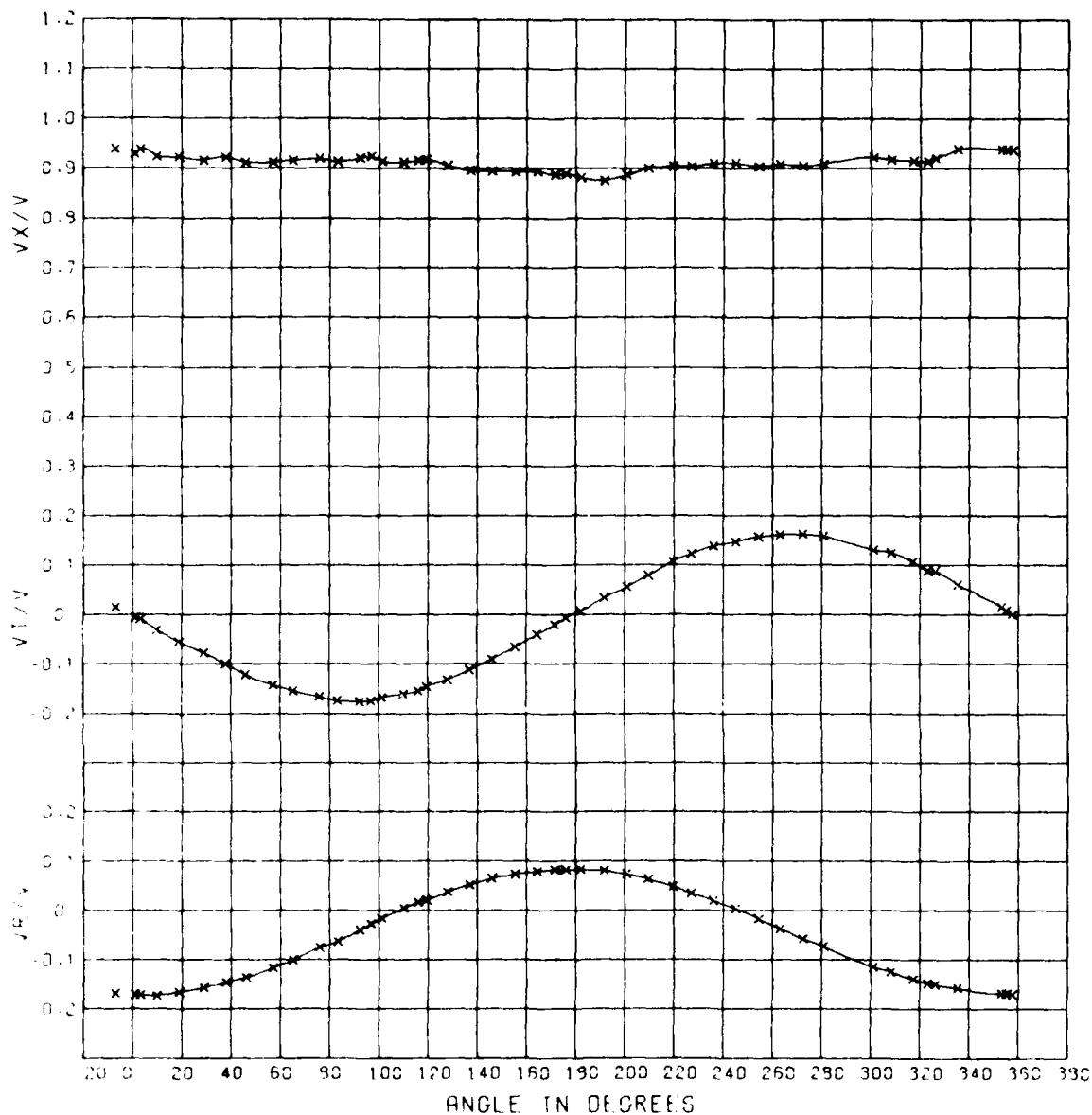
VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC 3KTSW016
0.456 RAD.

Figure H-1 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.456
for Experiment 16



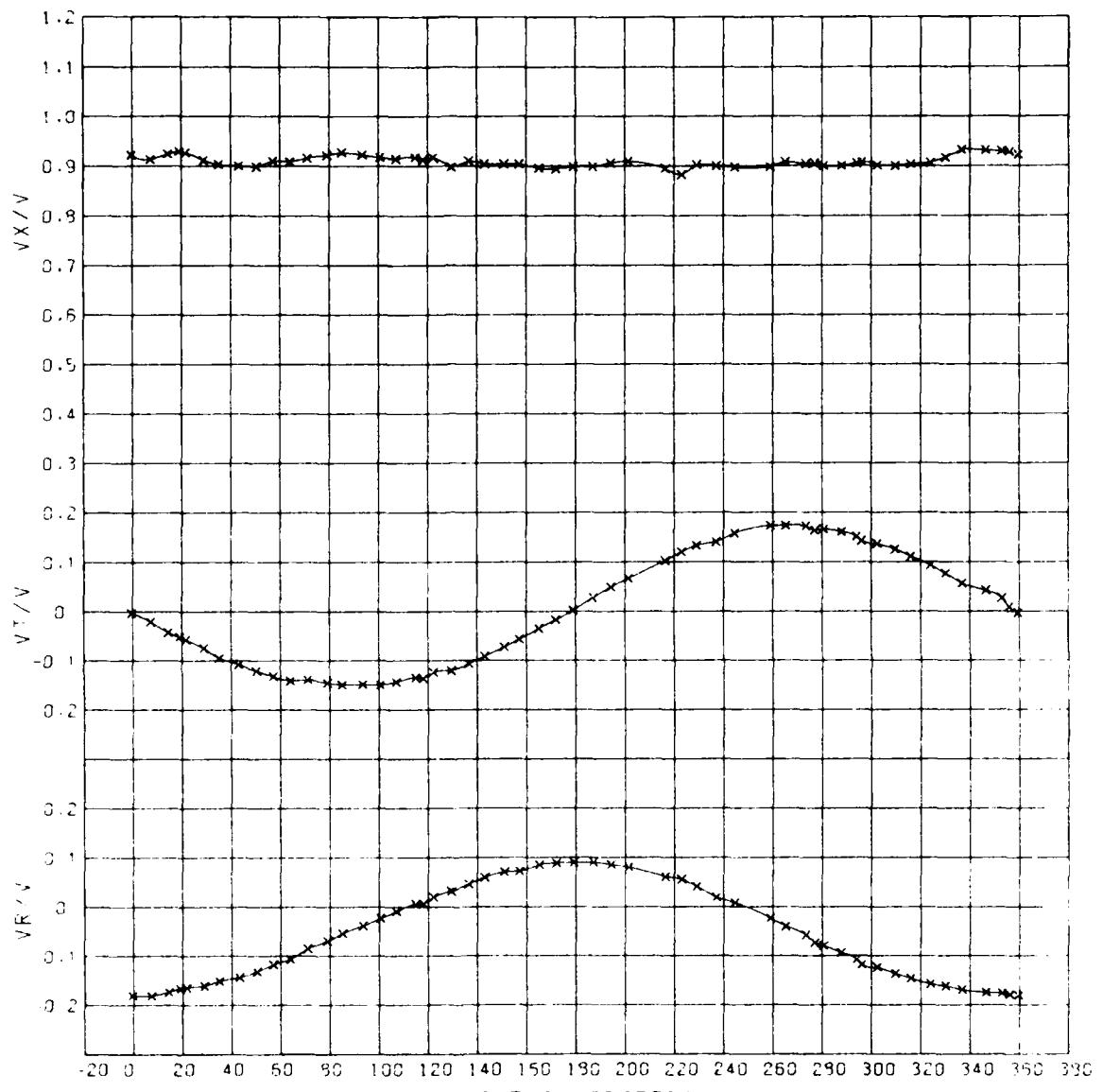
VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC 3KTSW016
0.633 RAD.

Figure H-2 - Circumferential Distribution of the Longitudinal, Tangential, and Radial Velocity Component Ratios - Radius Ratio = 0.633 for Experiment 16



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC 3KTSW015
0.781 RAD.

Figure H-3 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.781
for Experiment 16



VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC 3KTSW016
0.963 RAD.

Figure H-4 - Circumferential Distribution of the Longitudinal, Tangential,
and Radial Velocity Component Ratios - Radius Ratio = 0.963
for Experiment 16

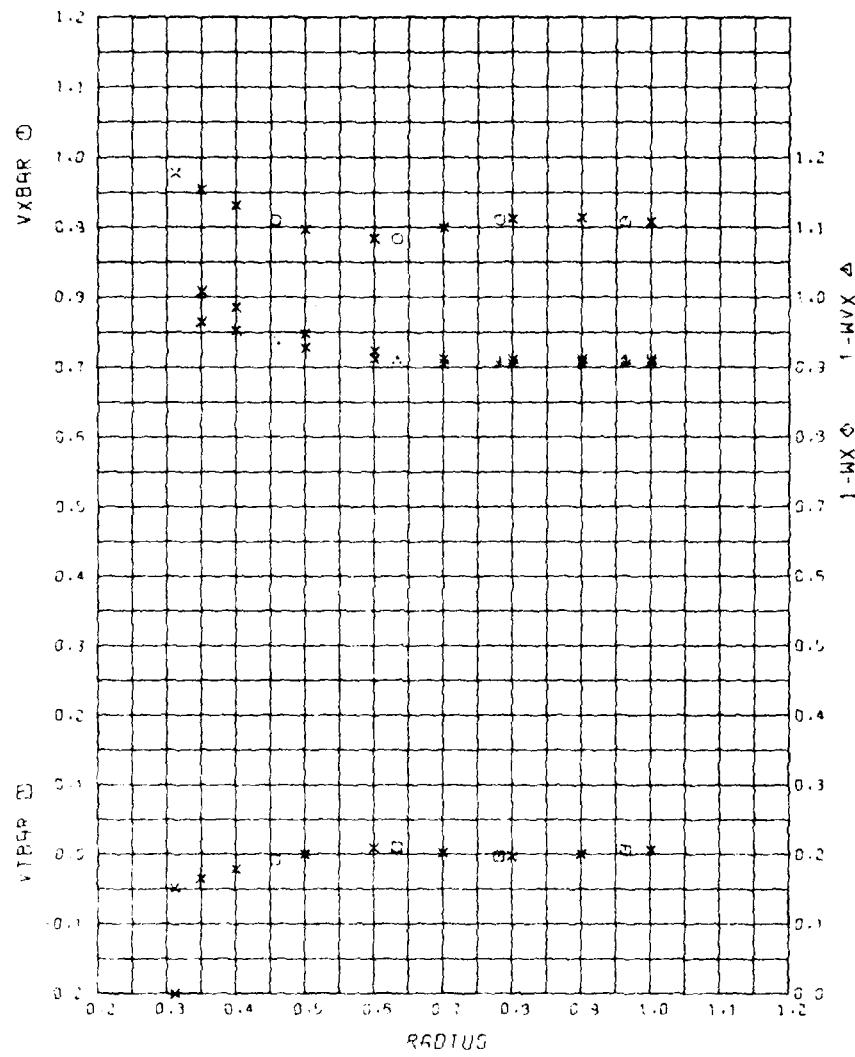


Figure H-5 - Radial Distribution of the Mean Velocity Component Ratios
for Experiment 16

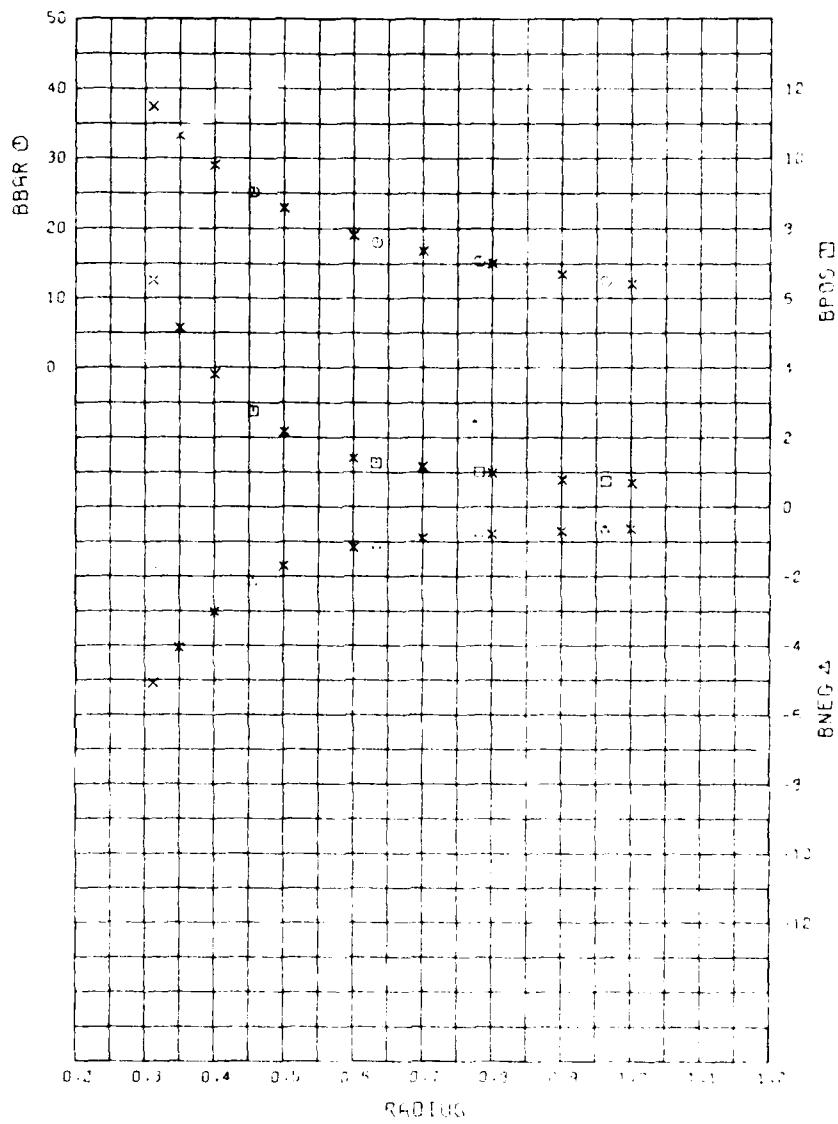


Figure II-6 - Radial Distribution of the Mean Advance Angle and Advance Angle Variations for Experiment 16

TABLE H-1

INPUT DATA FOR HARMONIC ANALYSIS FOR R/V ATHENA
WITH BASS DYNAMOMETER BOAT, EXPERIMENT 16

ANGLE	RADIUS *	VX/V	VT/V	WZ/V	ANGLE	VX/V	VT/V	WZ/V	ANGLE	RADIUS *	VX/V	VT/V	WZ/V	ANGLE	RADIUS *	VX/V	VT/V	WZ/V
-1.0	.925	-.811	-.125	.125	-1.0	.905	-.081	.135	-1.0	.930	-.035	.159	-.10	.926	-.002	.177	-.10	.905
.0	.923	-.815	-.123	.123	.0	.935	-.000	.135	.0	.928	-.006	.172	0.0	.921	-.006	.183	0.0	.921
.1	.920	-.817	-.121	.121	.1	.930	-.051	.131	.1	.931	-.010	.171	7.3	.913	-.021	.181	7.3	.913
.2	.927	-.805	-.118	.118	.2	.935	-.046	.130	.2	.937	-.010	.171	14.6	.913	-.024	.183	14.6	.913
.3	.926	-.807	-.117	.117	.3	.930	-.071	.121	.3	.931	-.022	.173	21.9	.929	-.031	.184	21.9	.929
.4	.920	-.817	-.116	.116	.4	.932	-.093	.122	.4	.932	-.030	.170	29.1	.931	-.037	.186	29.1	.931
.5	.925	-.819	-.115	.115	.5	.935	-.112	.112	.5	.927	-.100	.157	35.0	.931	-.059	.190	35.0	.931
.6	.928	-.816	-.114	.114	.6	.930	-.131	.093	.6	.931	-.122	.136	41.1	.931	-.101	.193	41.1	.931
.7	.921	-.805	-.113	.113	.7	.932	-.142	.083	.7	.937	-.137	.131	47.3	.931	-.142	.194	47.3	.931
.8	.917	-.816	-.112	.112	.8	.935	-.152	.073	.8	.931	-.157	.131	53.5	.931	-.152	.195	53.5	.931
.9	.917	-.817	-.111	.111	.9	.930	-.163	.063	.9	.931	-.167	.131	59.7	.931	-.158	.196	59.7	.931
.10	.916	-.818	-.110	.110	.10	.935	-.180	.050	.10	.931	-.176	.136	65.9	.931	-.159	.196	65.9	.931
.11	.919	-.805	-.109	.109	.11	.930	-.185	.045	.11	.931	-.185	.136	72.1	.936	-.138	.196	72.1	.936
.12	.920	-.818	-.108	.108	.12	.935	-.185	.045	.12	.926	-.176	.137	78.3	.927	-.135	.196	78.3	.927
.13	.918	-.818	-.107	.107	.13	.930	-.185	.045	.13	.930	-.175	.137	84.5	.926	-.134	.196	84.5	.926
.14	.919	-.819	-.106	.106	.14	.935	-.185	.045	.14	.931	-.185	.137	90.7	.927	-.134	.196	90.7	.927
.15	.911	-.816	-.105	.105	.15	.930	-.185	.045	.15	.931	-.195	.137	96.9	.913	-.135	.197	96.9	.913
.16	.917	-.817	-.104	.104	.16	.935	-.185	.045	.16	.931	-.205	.137	103.1	.913	-.135	.197	103.1	.913
.17	.916	-.818	-.103	.103	.17	.930	-.185	.045	.17	.931	-.215	.137	109.3	.913	-.135	.197	109.3	.913
.18	.915	-.819	-.102	.102	.18	.935	-.185	.045	.18	.931	-.225	.137	115.5	.913	-.135	.197	115.5	.913
.19	.912	-.818	-.101	.101	.19	.930	-.185	.045	.19	.931	-.235	.137	121.7	.913	-.135	.197	121.7	.913
.20	.909	-.819	-.100	.100	.20	.935	-.185	.045	.20	.931	-.245	.137	127.9	.913	-.135	.197	127.9	.913
.21	.916	-.818	-.99	.99	.21	.930	-.185	.045	.21	.931	-.255	.137	134.1	.913	-.135	.197	134.1	.913
.22	.915	-.819	-.98	.98	.22	.935	-.185	.045	.22	.931	-.265	.137	140.3	.913	-.135	.197	140.3	.913
.23	.913	-.818	-.97	.97	.23	.930	-.185	.045	.23	.931	-.275	.137	146.5	.913	-.135	.197	146.5	.913
.24	.912	-.819	-.96	.96	.24	.935	-.185	.045	.24	.931	-.285	.137	152.7	.913	-.135	.197	152.7	.913
.25	.911	-.818	-.95	.95	.25	.930	-.185	.045	.25	.931	-.295	.137	158.9	.913	-.135	.197	158.9	.913
.26	.910	-.819	-.94	.94	.26	.935	-.185	.045	.26	.931	-.305	.137	165.1	.913	-.135	.197	165.1	.913
.27	.909	-.818	-.93	.93	.27	.930	-.185	.045	.27	.931	-.315	.137	171.3	.913	-.135	.197	171.3	.913
.28	.908	-.819	-.92	.92	.28	.935	-.185	.045	.28	.931	-.325	.137	177.5	.913	-.135	.197	177.5	.913
.29	.907	-.818	-.91	.91	.29	.930	-.185	.045	.29	.931	-.335	.137	183.7	.913	-.135	.197	183.7	.913
.30	.906	-.819	-.90	.90	.30	.935	-.185	.045	.30	.931	-.345	.137	189.9	.913	-.135	.197	189.9	.913
.31	.905	-.818	-.89	.89	.31	.930	-.185	.045	.31	.931	-.355	.137	196.1	.913	-.135	.197	196.1	.913
.32	.904	-.819	-.88	.88	.32	.935	-.185	.045	.32	.931	-.365	.137	202.3	.913	-.135	.197	202.3	.913
.33	.903	-.818	-.87	.87	.33	.930	-.185	.045	.33	.931	-.375	.137	208.5	.913	-.135	.197	208.5	.913
.34	.902	-.819	-.86	.86	.34	.935	-.185	.045	.34	.931	-.385	.137	214.7	.913	-.135	.197	214.7	.913
.35	.901	-.818	-.85	.85	.35	.930	-.185	.045	.35	.931	-.395	.137	220.9	.913	-.135	.197	220.9	.913
.36	.900	-.819	-.84	.84	.36	.935	-.185	.045	.36	.931	-.405	.137	227.1	.913	-.135	.197	227.1	.913
.37	.899	-.818	-.83	.83	.37	.930	-.185	.045	.37	.931	-.415	.137	233.3	.913	-.135	.197	233.3	.913
.38	.898	-.819	-.82	.82	.38	.935	-.185	.045	.38	.931	-.425	.137	239.5	.913	-.135	.197	239.5	.913
.39	.897	-.818	-.81	.81	.39	.930	-.185	.045	.39	.931	-.435	.137	245.7	.913	-.135	.197	245.7	.913
.40	.896	-.819	-.80	.80	.40	.935	-.185	.045	.40	.931	-.445	.137	251.9	.913	-.135	.197	251.9	.913
.41	.895	-.818	-.79	.79	.41	.930	-.185	.045	.41	.931	-.455	.137	258.1	.913	-.135	.197	258.1	.913
.42	.894	-.819	-.78	.78	.42	.935	-.185	.045	.42	.931	-.465	.137	264.3	.913	-.135	.197	264.3	.913
.43	.893	-.818	-.77	.77	.43	.930	-.185	.045	.43	.931	-.475	.137	270.5	.913	-.135	.197	270.5	.913
.44	.892	-.819	-.76	.76	.44	.935	-.185	.045	.44	.931	-.485	.137	276.7	.913	-.135	.197	276.7	.913
.45	.891	-.818	-.75	.75	.45	.930	-.185	.045	.45	.931	-.495	.137	282.9	.913	-.135	.197	282.9	.913
.46	.890	-.819	-.74	.74	.46	.935	-.185	.045	.46	.931	-.505	.137	289.1	.913	-.135	.197	289.1	.913
.47	.889	-.818	-.73	.73	.47	.930	-.185	.045	.47	.931	-.515	.137	295.3	.913	-.135	.197	295.3	.913
.48	.888	-.819	-.72	.72	.48	.935	-.185	.045	.48	.931	-.525	.137	301.5	.913	-.135	.197	301.5	.913
.49	.887	-.818	-.71	.71	.49	.930	-.185	.045	.49	.931	-.535	.137	307.7	.913	-.135	.197	307.7	.913
.50	.886	-.819	-.70	.70	.50	.935	-.185	.045	.50	.931	-.545	.137	313.9	.913	-.135	.197	313.9	.913
.51	.885	-.818	-.69	.69	.51	.930	-.185	.045	.51	.931	-.555	.137	319.1	.913	-.135	.197	319.1	.913
.52	.884	-.819	-.68	.68	.52	.935	-.185	.045	.52	.931	-.565	.137	325.3	.913	-.135	.197	325.3	.913
.53	.883	-.818	-.67	.67	.53	.930	-.185	.045	.53	.931	-.575	.137	331.5	.913	-.135	.197	331.5	.913
.54	.882	-.819	-.66	.66	.54	.935	-.185	.045	.54	.931	-.585	.137	337.7	.913	-.135	.197	337.7	.913
.55	.881	-.818	-.65	.65	.55	.930	-.185	.045	.55	.931	-.595	.137	343.9	.913	-.135	.197	343.9	.913
.56	.880	-.819	-.64	.64	.56	.935	-.185	.045	.56	.931	-.605	.137	350.1	.913	-.135	.197	350.1	.913
.57	.879	-.818	-.63	.63	.57	.930	-.185	.045	.57	.931	-.615	.137	356.3	.913	-.135	.197	356.3	.913
.58	.878	-.819	-.62	.62	.58	.935	-.185	.045	.58	.931	-.625	.137	362.5	.913	-.135	.197	362.5	.913
.59	.877	-.818	-.61	.61	.59	.930	-.185	.045	.59	.931	-.635	.137	368.7	.913	-.135	.197	368.7	.913
.60	.876	-.819	-.60	.60	.60	.935	-.185	.045	.60	.931	-.645	.137	374.9	.913	-.135	.197	374.9	.913
.61	.875	-.818	-.59	.59	.61	.930	-.185	.045	.61	.931	-.655	.137	381.1	.913	-.135	.197	381.1	.913
.62	.874	-.819	-.58	.58	.62	.935	-.185	.045	.62	.931	-.665	.137	387.3	.913	-.135	.197	387.3	.913
.63	.873	-.818	-.57	.57	.63	.930	-.185	.045	.63	.931	-.675	.137	393.5	.913	-.135	.197	393.5	.913
.64	.872	-.819	-.56	.56	.64	.935	-.185	.045	.64	.931	-.685	.137	409.7	.913	-.135	.197	409.7	.913
.65	.871	-.818	-.55	.55	.65</													

TABLE H-2 - LISTING OF THE MEAN VELOCITY COMPONENT RATIOS, THE MEAN ADVANCE ANGLES AND OTHER DERIVED QUANTITIES AT THE EXPERIMENTAL AND INTERPOLATED RADII FOR EXPERIMENT 16

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY 10 INC 3KTSW016
PROPELLER DIAMETER = 6.00 FEET JA = .739

RADIUS = .456	.633	.781	.763	.312	.350	.400	.500	.600	.700	.800	.900	1.000
VBAR = .910	.834	.911	.608	.577	.955	.931	.897	.884	.899	.912	.913	.908
VBAR = -.038	.010	-.003	.206	-.048	-.035	-.021	-.000	.009	.002	-.003	-.000	.006
VBAR = -.026	-.041	-.046	-.247	-.008	-.013	-.020	-.031	-.039	-.044	-.046	-.047	-.047
1-WX = .37	.903	.905	.005	0.000	.965	.952	.928	.912	.905	.905	.907	.908
1-WX = -.64	.918	.909	.910	0.000	1.009	.935	.745	.923	.712	.911	.912	.912
BBAR = 25.22	18.12	15.34	12.49	37.38	33.31	28.13	22.14	19.05	16.80	15.02	13.42	12.04
BPOS = 2.76	1.27	1.02	.74	6.52	5.16	3.31	2.57	1.40	1.16	.98	.78	.70
THETA = 85.00	95.00	95.00	85.00	80.50	80.00	82.50	91.50	92.50	95.00	95.00	95.00	85.00
SIGS = -2.18	-1.13	-1.79	-5.65	-5.07	-4.06	-3.52	-1.79	-1.18	-0.90	.77	.59	.63
THETA = 242.50	260.00	255.00	222.50	250.00	242.50	242.50	242.50	242.50	200.00	200.00	255.00	222.50

- 15 CIRCUMFERENTIAL MEAN TANGENTIAL VELOCITY.
- 15 CIRCUMFERENTIAL MEAN RADIAL VELOCITY.
- 15 CIRCUMFERENTIAL MEAN TOTAL VELOCITY.
- 15 CIRCUMFERENTIAL MEAN VARIATION WITHOUT TANGENTIAL CORRECTION.
- 15 CIRCUMFERENTIAL MEAN VARIATION WITH TANGENTIAL CORRECTION.
- 15 MEAN ANGLE OF ADVANCE.
- 15 MEAN ANGLE OF ADVANCE AND MEAN SINE BETA PLUS).
- 15 MEAN ANGLE OF ADVANCE AND MEAN SINE BETA MINUS).
- 15 VARIATION BETWEEN THE MAXIMUM AND MEAN SINE BETA PLUS).
- 15 VARIATION BETWEEN THE MAXIMUM AND MEAN SINE BETA MINUS).
- 15 ANGLE IN DEGREES AT WHICH CORRESPONDING RATIO IS EQUAL.

TABLE 6-3

HARMONIC ANALYSIS OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 16

*E-SOCETY LONGITUDINAL RATIO = .00155271 BASS BOAT ONLY 10 INC 341SWC16
PROPELLER DIAMETER = 6.00 FEET JA = .739

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX.V)

HARMONIC	1	2	3	4	5	6	7	8
RADIUS = .456	.0032	.0032	.0032	.0016	.0029	.0017	.0004	.0002
AMPLITUDE = 74.2	264.9	71.7	21.0	122.4	9.5	200.2	170.6	
PHASE ANGLE =								
RADIUS = .633								
AMPLITUDE = 98.3	.0220	.0263	.0045	.0010	.0025	.0005	.0015	.0008
PHASE ANGLE =	267.2	74.0	130.6	209.8	69.4	192.2	92.4	
RADIUS = .781								
AMPLITUDE = 88.2	.0176	.0032	.0077	.0014	.0023	.0037	.0006	.0033
PHASE ANGLE =	223.0	118.8	168.2	65.6	165.2	210.1	211.8	
RADIUS = .963								
AMPLITUDE = 53.9	.0102	.0029	.0005	.0056	.0021	.0025	.0024	.0032
PHASE ANGLE =	157.1	134.8	90.4	126.6	291.4	217.6	271.8	
HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX.V)								
HARMONIC = 9	10	11	12	13	14	15	16	
RADIUS = .456								
AMPLITUDE = 145.2	.0012	.0014	.0014	.0005	.0018	.0010	.0012	.0012
PHASE ANGLE =	234.6	236.8	323.8	306.9	60.0	164.3	139.2	
RADIUS = .633								
AMPLITUDE = 224.9	.0011	.0010	.0015	.0009	.0014	.0018	.0010	.0004
PHASE ANGLE =	356.5	160.9	168.4	255.2	272.2	98.8	337.1	
RADIUS = .781								
AMPLITUDE = 337.3	.0008	.0004	.0010	.0019	.0015	.0003	.0010	.0002
PHASE ANGLE =	282.3	1.3	48.6	299.9	241.2	86.9	28.1	
RADIUS = .963								
AMPLITUDE = 206.5	.0016	.0033	.0012	.0025	.0008	.0001	.0011	.0008
PHASE ANGLE =	269.1	202.4	152.3	251.6	12.8	179.7	77.3	

TABLE R-4 - HARMONIC ANALYSIS OF LONGITUDINAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 16

HARMONIC ANALYSES OF LONGITUDINAL VELOCITY COMPONENT RATIOS (VX V)									
HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .312		.0256	.0251	.0253	.0257	.0118	.0007	.0024	.0049
APP. = .05									
PHASE ANG. =		322.5	325.3	327.2	330.3	78.1	42.3	4.2	227.8
RADIUS = .350		.0132	.0038	.0034	.0034	.0037	.0011	.0015	.0032
APP. = .05									
PHASE ANG. =		335.4	335.4	335.6	335.6	82.8	20.2	3.0	225.9
RADIUS = .400		.0077	.0027	.0024	.0024	.0030	.0015	.0015	.0016
APP. = .05									
PHASE ANG. =		233.1	233.1	233.3	233.3	93.6	11.9	356.4	225.3
RADIUS = .500		.0148	.0050	.0049	.0049	.0057	.0016	.0009	.0005
APP. = .05									
PHASE ANG. =		63.8	63.8	64.2	64.2	155.3	10.1	192.9	74.5
RADIUS = .600		.0212	.0094	.0093	.0093	.0097	.0027	.0016	.0010
APP. = .05									
PHASE ANG. =		47.9	47.9	48.7	48.7	152.3	29.6	191.6	74.0
RADIUS = .700		.0203	.0043	.0041	.0041	.0047	.0026	.0019	.0012
APP. = .05									
PHASE ANG. =		34.4	34.4	35.7	35.7	168.0	156.3	124.4	425.3
RADIUS = .800		.0168	.0029	.0029	.0029	.0025	.0027	.0007	.0005
APP. = .05									
PHASE ANG. =		66.3	221.6	121.0	135.5	65.7	167.3	214.0	213.0
RADIUS = .900		.0126	.0027	.0026	.0026	.0024	.0019	.0014	.0003
APP. = .05									
PHASE ANG. =		71.5	176.8	129.5	132.5	83.7	201.6	219.6	234.7
RADIUS = .950		.0102	.0029	.0025	.0024	.0021	.0025	.0024	.0023
APP. = .05									
PHASE ANG. =		53.2	157.1	104.8	105.4	121.6	211.4	217.6	217.8

TABLE H-4 (Continued)

VELOCITY COMPONENT RATIOS FOR TUNNEL 527: BASS BOAT ONLY INC 3KTSW016									
PROJECTOR DIAMETER = 6.00 FEET JA = .739									
HARMONIC ANALYSES OF CONSTITUTION VELOCITY COMPONENT RATIOS (VX.V)									
HARMONIC	=	9	10	11	12	13	14	15	16
RADIUS = .312	=	.0033	.0038	.0033	.0021	.0048	.0066	.0026	.0041
AMPLITUDE = 86.9	=	256.3	272.3	312.6	340.9	82.0	197.0	141.2	
PHASE ANGLE =									
RADIUS = .350	=	.0025	.0030	.0027	.0016	.0038	.0048	.0021	.0032
AMPLITUDE = 95.2	=	262.3	265.6	312.2	335.6	80.4	191.8	141.1	
PHASE ANGLE =									
RADIUS = .400	=	.0017	.0021	.0020	.0010	.0027	.0027	.0016	.0022
AMPLITUDE = 112.8	=	274.0	254.0	313.2	325.6	76.5	181.7	140.6	
PHASE ANGLE =									
RADIUS = .500	=	.0011	.0012	.0011	.0005	.0035	.0035	.0010	.0006
AMPLITUDE = 173.7	=	315.4	220.5	5.4	287.5	322.8	145.8	135.5	
PHASE ANGLE =									
RADIUS = .600	=	.0011	.0011	.0006	.0007	.0014	.0017	.0010	.0003
AMPLITUDE = 214.9	=	214.9	141.8	69.5	257.0	274.6	106.6	106.6	
PHASE ANGLE =									
RADIUS = .700	=	.0006	.0005	.0015	.0014	.0010	.0011	.0003	
AMPLITUDE = 302.9	=	2.3	2.3	45.1	284.5	265.3	86.5	344.3	
PHASE ANGLE =									
RADIUS = .800	=	.0008	.0006	.0011	.0013	.0015	.0002	.0009	.0002
AMPLITUDE = 337.2	=	271.9	359.0	52.2	301.0	227.4	89.6	41.3	
PHASE ANGLE =									
RADIUS = .900	=	.0005	.0020	.0012	.0015	.0011	.0001	.0007	.0005
AMPLITUDE = 252.0	=	266.3	331.1	109.5	290.6	114.7	137.4	73.3	
PHASE ANGLE =									
RADIUS = 1.000	=	.0016	.0033	.0012	.0026	.0008	.0001	.0011	.0008
AMPLITUDE = 206.5	=	269.1	298.4	152.3	251.6	12.8	179.7	77.3	
PHASE ANGLE =									

TABLE 4-5 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE EXPERIMENTAL RADII FOR EXPERIMENT 16

VELOCITY COMPONENT RATIOS FOR MODEL 5271 BASS BOAT ONLY IN C 3KTSWC16 PROPELLER DIAMETER = 6.00 FEET JA = .739							
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)							
HARMONIC	1	2	3	4	5	6	7
RADIUS = .456							
AMPLITUDE =	.1958	.0023	.0059	.0001	.0006	.0010	.0014
PHASE ANGLE =	182.2	77.3	4.2	184.6	135.0	200.4	285.2
RADIUS = .633							
AMPLITUDE =	.1761	.0026	.0034	.0005	.0010	.0012	.0005
PHASE ANGLE =	181.9	301.3	7.9	103.0	98.9	109.4	344.0
RADIUS = .781							
AMPLITUDE =	.1654	.0023	.0027	.0011	.0005	.0012	.0006
PHASE ANGLE =	181.0	61.6	12.3	235.4	306.7	166.4	330.8
RADIUS = .963							
AMPLITUDE =	.1607	.0045	.0010	.0023	.0002	.0002	.0011
PHASE ANGLE =	181.6	291.7	107.0	100.8	176.4	342.8	98.1
HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)							
HARMONIC	8	9	10	11	12	13	14
RADIUS = .456							
AMPLITUDE =	.0027	.0008	.0039	.0012	.0009	.0008	.0010
PHASE ANGLE =	15.5	352.0	138.5	167.7	208.4	272.7	309.1
RADIUS = .633							
AMPLITUDE =	.0003	.0004	.0004	.0004	.0005	.0001	.0004
PHASE ANGLE =	161.6	35.1	59.4	55.8	346.0	215.4	232.0
RADIUS = .781							
AMPLITUDE =	.0010	.0004	.0003	.0005	.0003	.0002	.0005
PHASE ANGLE =	169.9	158.7	17.7	337.7	23.5	83.1	11.3
RADIUS = .963							
AMPLITUDE =	.0012	.0003	.0013	.0013	.0007	.0003	.0002
PHASE ANGLE =	162.5	162.1	162.1	243.2	197.7	53.4	356.6

TABLE H-6 - HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS AT THE INTERPOLATED RADII FOR EXPERIMENT 16

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)									
HARMONIC	=	1	2	3	4	5	6	7	8
RADIUS = .312									
AMPLITUDE = .2173		.0170	.0010	.0022	.0012	.0031	.0026	.0043	
PHASE ANGLE = 182.0		90.2	10.8	255.2	268.1	252.5	240.5	280.7	
RADIUS = .350									
AMPLITUDE = .2111		.0126	.0010	.0015	.0007	.0022	.0020	.0034	
PHASE ANGLE = 182.1		89.2	10.4	255.3	261.4	248.2	246.6	281.6	
RADIUS = .400									
AMPLITUDE = .2036		.0076	.0059	.0007	.0003	.0013	.0014	.0024	
PHASE ANGLE = 182.2		65.6	9.8	251.7	230.4	236.9	259.9	283.4	
RADIUS = .500									
AMPLITUDE = .1902		.0012	.0051	.0003	.0005	.0006	.0009	.0008	
PHASE ANGLE = 182.2		33.0	8.7	28.7	116.3	150.4	309.3	293.5	
RADIUS = .600									
AMPLITUDE = .1792		.0025	.0038	.0005	.0006	.0010	.0011	.0003	
PHASE ANGLE = 182.0		300.4	7.9	96.4	103.1	112.2	340.8	73.4	
RADIUS = .700									
AMPLITUDE = .1705		.0019	.0033	.0007	.0002	.0006	.0013	.0006	
PHASE ANGLE = 181.4		41.6	7.6	237.6	344.5	126.6	335.5	91.3	
RADIUS = .800									
AMPLITUDE = .1645		.0032	.0025	.0010	.0005	.0002	.0011	.0006	
PHASE ANGLE = 181.0		60.9	11.7	235.0	304.1	183.6	330.3	113.8	
RADIUS = .900									
AMPLITUDE = .1613		.0016	.0012	.0008	.0003	.0003	.0005	.0007	
PHASE ANGLE = 181.1		357.1	37.2	136.5	284.3	313.1	335.2	165.4	
RADIUS = 1.000									
AMPLITUDE = .1607		.0045	.0010	.0023	.0002	.0005	.0002	.0011	
PHASE ANGLE = 181.6		291.7	107.0	100.8	176.4	342.8	98.1	192.2	

TABLE H-6 (Continued)

HARMONIC ANALYSES OF TANGENTIAL VELOCITY COMPONENT RATIOS (VT/V)						
HARMONIC	=	9	10	11	12	13
RADIUS = .312						
AMPLITUDE = .0068		.0010	.0022	.0022	.0041	.0016
PHASE ANGLE = 15.1		321.1	146.6	117.0	185.7	314.9
RADIUS = .350						
AMPLITUDE = .0055		.0010	.0018	.0019	.0031	.0013
PHASE ANGLE = 15.1		329.5	147.2	115.2	188.1	306.1
RADIUS = .400						
AMPLITUDE = .0041		.0009	.0014	.0016	.0019	.0010
PHASE ANGLE = 15.1		340.4	147.9	112.3	193.5	291.7
RADIUS = .500						
AMPLITUDE = .0017		.0007	.0006	.0010	.0005	.0007
PHASE ANGLE = 16.4		.8	148.5	102.2	247.9	257.2
RADIUS = .600						
AMPLITUDE = .0002		.0004	.0031	.0005	.0008	.0005
PHASE ANGLE = 64.8		23.5	130.2	74.8	339.2	225.7
RADIUS = .700						
AMPLITUDE = .0007		.0002	.0003	.0005	.0007	.0001
PHASE ANGLE = 169.4		130.8	18.9	10.1	3.9	123.7
RADIUS = .800						
AMPLITUDE = .0010		.0005	.0002	.0006	.0005	.0004
PHASE ANGLE = 169.6		159.3	18.5	329.2	27.4	84.7
RADIUS = .900						
AMPLITUDE = .0012		.0003	.0005	.0008	.0001	.0003
PHASE ANGLE = 166.3		141.3	191.4	271.4	42.2	150.0
RADIUS = 1.000						
AMPLITUDE = .0012		.0003	.0013	.0002	.0007	.0003
PHASE ANGLE = 162.5		66.1	192.6	243.2	231.5	197.7

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